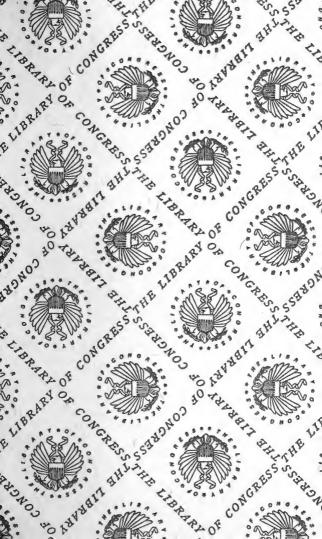
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HANDY

MECHANICAL POCKET COMPANION

FOR THE

Engineer, Business Man & Mechanic.

CONTAINING

TABLE OF METALS, STRENGTH OF MATERIALS, WAGES, BOARD
MEASURE, SCANTLING MEASURE, CUTTING SCREWS BY
LATHE, HORSE-POWER OF SHAFTING, BELTING,
CIRCUMFERENCES, AREAS, SQUARES, CUBES,

SQUARE ROOT, CUBE ROOT ETC. ETC. CONGRESS

COMPILED BY WASHINGTON

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PREFACE.

This little collation of authorities and culling of condensed and useful tables, rules, etc., is designed to meet a growing demand for something more practical and concise for the use of Mechanics, in all the different departments of Mechanical industries.

It has been arranged with great care, selected from the best authorities, just the right thing and an endeavor made to put them in the right place.

This volume gives more practical and less theoretical knowledge than can be found in any other book yet offered to the practical Mechanic, and at a price within the reach of all.

The idea has been to have this book published in such a shape that it can be carried in a pocket so that it may be referred to at any time.

A. W. H.



THE CHEMICAL KINGDOM.

NAME, WHEN DISCOVERED, BY WHOM, SYMBOLS, COLOR AND SPECIFIC GRAVITY.

Name.	Dis- cov.	By whom.	Sy- m.	Color.	Sp'c. G'ty.
Aluminum.	1808	Davy.	Al	White	2.60
Antimony.	1460	Basil-Valentine	Sb	Bluish White	6.70
Arsenic.	1733	Brandt.	As	Gray	5.88
Barium.	1808	Davy.	Ba	Dark Gray	1.50
Bismuth.	1529	Agricola.	Bi	Yellow'h W'te	9.80
Boran.	1808	Davy.	В	White	2.00
Bromine.	1826	Balard.	Br	Brownish R'd	2.97
Cadmium.	1817	Stromeyer.	Cd	White	8.60
Cæsium.	1860	Bunsen.	Cs	Blue	1.50
Calcium.		Davy.	Ca	White	3.52
Carbon.		Ancients.	C	Black	
Cerium.	1803	Berzelius.	Ce	Gray White	
Chlorine.		Scheele.	Cl	Greenish	2.49
Chromium.		Vanquelin.		Grayish W'te	6.00
Cobalt.	1733	Brandt.		Gray White	8.90
Columbium.	1801	Hatchett.	Cb	Iron Gray	5.50
Copper.		Ancients.	Cu	Red	8.90
Didymium.	1841		D	1	
Erbium.	1841		E	White	
Fluorine.	1		F	Colorless	1.29
Gallium.	1875	Lecog.	9	COTOTICOS	1.20
Gold.	10.0	Ancients.	in	Yellow	19.26
Glucinum.	1828	Wohler.	G	White	10.20
Hydrogen.		Cavendish.	H	Colorless	.07
Indium.		Reichter.	In	Bluish	7.42
Iodine.		Courtois.	T	Grayish Bla'k	
Iridium.	1803		Īr	White	18.68
Iron.	1000	Ancients.		Bluish Gray	7.90
	1841	Mosander.		Red	1.00
Lead.	1041	Ancients.		Blue	11.44
Lithium.	1817	Bunsen.	it."	White	.59
Magnesium.		Davy.		Silver White	3.70
Manganese.		Gahn.	Mr	Gray White	8.00
Mercury.		Ancients.		White	13.60
mercury.	1	Aucients.	Hig	и ште	110.00

CHEMICAL KINGDOM. (Continued.)

Name.	Dis-		Sy- m.	Color,	S. G.
Molybdenum.	1782	Hjelm.		Gray	8.60
Nickel.		Cronstedt.	Ni	White	8.80
Nitrogen.	1772	Rutheford.	N	Colorless	.97
Osmium.	1803	Tennant.	Os	Bluish Black	10.00
Oxygen.	1774	Priestley.	О	Colorless	1.11
Palladium.		Wallaston.	Pd	Bluish Wh'te	11.80
Phosphorus.	1669	Brandt.	P	Yellow	2,00
Platinum.	1741	Wood.	Pt	Bluish Wh'te	21.50
Potassium	1807	Davv.	K	Gray White	.87
Rhodium.	1803	Wallaston.	Ro	Grayish W'te	10.60
Rubidium.		Bunsen.		Red	
Ruthenium.	1847	Claus.	Ru	White	
Selenium.		Berzelius.	Se	Dark Brown	4.32
Silicon.	1824	Berzelius.		Brown	
Silver.		Ancients.		White	10.50
Sodium.	1808	Davy.	Na	Gray White	.97
Strontium.		Davy.	Sr	Grav	2.50
Sulphur.		Ancients.	S	Yellow	1.99
Tantalum.	11802	Ekeberg.	Ta		
Tellurium.		Klaproth.	Te	Bluish Wh'te	6.20
Thallium.		Crookes.	TI	Green	
Thorium.		Berzelius.	Th	White	
Tin.	1-0-0	Ancients.		White	7.30
Titanium.	1789	Gregor.		Red	5.30
Tungsten.		De Layurt.		Brown'h B'k	
Uranium.	1789	Klaproth		Gray	8.00
Vanadium.	1830	Sefstrom.	V	White	
Yttrium.	1828	Wohler.	Ÿ	White	
Zinc.		Paracelsus.		Bluish Wh'te	7.00
Zirconium.		Berzelius.		White	1.0

METAL BORING AND TURNING.

Boring Cast-Iron—Divide 25 by the diameter of the cylinder in inches for the revolutions per minute.

- " Wrought-Iron—The speed is one fifth greater than for cast-iron.
- "Brass—The speed is one half that, for cast-iron. Turning Cast-Iron—The speed is twice that of boring.
 - "Wrought-Iron—The speed is one fifth greater than that for east-iron.
 - Brass—The speed is twice that of boring.

Verticle Boring—The speed may be twice that of horizontal boring.

The feed depends upon the stability of the machine and depth of cut.

IRON TURNING and BORING by means of the SLIDE REST.

						-	-
Diameter in Inches.	Revolution of Spindle per Minute.	Diameter in Inches.	Revolution of Spindle per Minute.	Diameter in Inches.	Revolution of Boring bar per Minute.	Diameter in Inches.	Revolution of Boring bar per Minute.
1 2 3 4 5 6 7 8 9 10 15 20	50. 25. 16.67 12.50 10. 8.32 7.15 6.25 5.55 5.55	25 30 35 40 45 50 60 70 80 90 100	2. 1.667 1.430 1.250 1.120 1. .834 .716 .626 .554 .500	1 2 3 4 5 6 7 8 9 10 15 20	25. 12.500 8.330 6.250 5. 4.160 3.570 3.125 2.770 2.500 1.660 1.250	25 30 35 40 45 50 60 70 80 90 100	1. .833 .714 .425 .566 .500 .417 .358 .313 .278 .250

Velocities of Wood-working Machinery in Feet or Revolutions per Minute.

Circular Saws, at periphery, 6000 to 7000 feet.

Band Saws, 2500 feet.

Gang Saws, 20 inch stroke, 120 strokes, per minute. Scroll Saws, 300 strokes, per minute.

Planing machine cutters at periphery, 4000 to 6000 feet.

Work under planing machine, 1-20 of an inch for each cut.

Molding-machine cutters, 3500 to 4000 feet.

Squaring-up-machine cutters, 7000 to 8000 feet.

Wood-Carving drills, 5000 revolutions.

Machine augers, 11/2 inch in diameter, 900 revolutions.

Machine augers, 34 inch in diameter, 1200 revolutions,

Gang Saws require for 45 superficial feet of pine per hour, one Horse Power.

Circular Saws require for 75 superficial feet of pine per hour, one Horse Power.

In oak or hard wood, 34 ths of the above quantity require one Horse Power.

Table to calculate the Pitch of a Toothed Wheel when the radius and number of teeth are given; and the Radius, when the Pitch and number of teeth are given, from 10 to 159 teeth.

No.	Radi-	No	Radi-	No	Radi-	No	Radi-	No	Radi-
T'h		T'h		T'h		T'h	us.	T'h	
	us.					-			us.
10	1.618	40	6.373	70	11.144	100	15.918	130	20.692
11	1.774	41	6.532	71	11.303	101	16.077	131	20.851
12	1.932	42	6.691	72	11.463	102	16.236	132	21.010
13	2.089	43	6.850	73	11.622	103	16.395	133	21.169
14	2.247	44	7.009	74	11.781	104	16.554	134	21.328
15	2.405	45	7.168	75	11.940	105	16.713	135	21.488
16	2.563	46	7.327	76	12.099	106	16.873	-136	21.647
17	2.721	47	7.486	77	12.258	107	17.032	137	21.806
18	2.869	48	7.645	78	12.417	108	17.191	138	21.965
19	3.038	49	7.804	79	12.576	109	17.350	139	22.124
20	3.196	50	7.963	80	12.735	110	17.509	140	22.283
21	3.355	51	8.122	81	12.895	111	17.668	141	22.442
22	3.513	52	8.281	82	13.054	112	17.827	142	22.602
23	3.672	53	8.440	83	13.213	113	17.987	143	22.761
24	3.830	54	8.599	84	13.370	114	18.146	144	22.920
25	3.989	55	8.758	85	13.531	115	18.305	145	23.079
26	4.148	56	8.917	86	13.690	116	18.464	146	23.238
27	4.307	57	9.076	87	13.849	117	18.623	147	23.397
28	4.465	58	9.235	88	14.008	118	18.782	148	23.556
29	4.624	59	9.394	89	14.168	119	18.941	149	23.716
30	4.788	60	9.553	90	14.327	120	19.101	150	23.874
31	4.942	61	9.712	91	14.486	121	19.260	151	24.034
32	5.101	62	9.872	92	14.645	122	19.419	152	24.193
33	5.260	63	10.031	93	14.804	123	19.578	153	24.352
34	5.419	64	10.190	94	14.963	124	19.737	154	24.511
35	5.578	65	10.349	95	15.122	125	19.896	155	24.620
36	5.737	66	10.508	96	15.281	126	20.055	156	24.830
37	5.896	67	10.667	97	15.440	127	20.214	157	24.989
38	6.055	68	10.826	98	15.600	128	20.374	158	25.148
39	6.214	69	10.985	99	15.759	129	20.533	159	25.307

Rule 1-Divide the required radius by the radius opposite the given number of teeth in the table; the quotient will be the required pitch of the wheel.

Example-To find the Pitch of a wheel whose radius is 43 inches, that shall contain 90 teeth. Required radius 43+14.327=3 inch pitch.

Rule 2-Multiply the radius opposite the given number of teeth by the pitch required; the product will be the required radius of the wheel.

Example-To find the radius of a wheel that shall contain 48 teeth of 21/2 inch pitch.

In the table, radius $7.645 \times 2.5 = 19\frac{1}{10}$ inches nearly.

PROPORTION SCALES FOR GEARING.

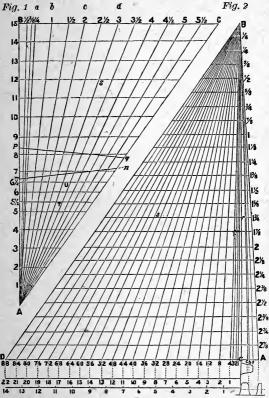


Figure 1 contains the proportions, in which the pitch is supposed to be divided into 15 equal parts.

The construction of this scale is very simple. Thus let A. B. be divided into 15 equal parts, and draw B. C. per-

pendicular to it; and again divide B. C. into a determinate number of parts from B. actual measures of the pitches for which the scale is intended to be used; that is, B a=1/2 inch; B b=1 inch; B c=2 inches, and so on, and join a and A, b and A, c and A, and so on. To complete the scale, draw 15 parallels to BC from the points numbered in the line A B, numbering their intersections (if thought proper) with the line A C in the same order; and also the two parallels T and U, (which are full lines in diagram,) equidistant from the parallels on each side of them.

The scale is thus ready for use, and its principle is self-To get from it the several proportions for a given pitch, say 3 inches=Bd, let the compasses be extended from the intersection of the parallel marked T, with the line A B, to the point where it intersects the line A d; this will be the part of the tooth from the pitch line to the point, and equivalent to $5\frac{1}{2}$ parts of the pitch, (viz. of Bd;) similarly the compasses being extended from the intersection of the parallel U, with the line A B, to its point of intersection of the line A d, will give the part of the length of the tooth from the pitch line to the root, and equivalent to 61 parts of the pitch. For the whole length of the tooth (if wanted in one measurement) set the compasses to the point where the parallel marked 12 meets the line A B, and extend to its point of intersection of the line A d at s, the length is 12 parts of the pitch B d; the working depth is in like manner found from the parallel marked 11; the thickness from that marked 7; and the width of space from that marked 8. The proportions for any other given pitch comprised in the scale are found in precisely the same way, and if the scale be well constructed they may be measured off with the utmost accuracy. To save confusion it is, however, better in practice to insert in the diagram only those parallels, namely, T. U. 12, 11 8. 7, which are required; the others are not requisite, and by inattention may lead to error.

The description of the scale as here given supposes that lateral clearance is constantly $_{15}^{\rm to}$ of the pitch; but as it is commonly desired that this should vary slightly with the pitch relatively increasing as pitch decreases, two other lines, m n and p q, have been introduced into the scale, to enable such modification to be adopted, should it be required. These lines are drawn at such angles as to give a clearance at 6 inches pitch of 1–18th, which is increased at $\frac{3}{4}$ inch pitch to $\frac{1}{100}$. From these lines the thickness and space are to be taken, instead of using the lines marked 7 and 8, setting the compasses in the points of intersection with the pitch lines, and extending perpendicularly to the time A B; in other words, the shortest distance from the point of intersection with the pitch line to the line A B; is the required measure of the space when the line p q is taken, and of

the thickness of tooth when the line m n is taken.

Figure 2 is more complete than the one described, and when well constructed insures, with moderate care, a degree of accuracy and uniformity. in the construction of the various sizes of wheels for which it is employed, that can hardly be otherwise attained. The principle of its construction is in effect the same as that described, but its use is more extended; the diameter of the wheel being found from it simultaneously with the length and thickness of tooth, width of space, and clearances. The scale is adapted to wheels of all the pitches, from 1/2 inch up to 3 inches.

The mode of construction is this: having drawn the line A D of any convenient length, raise the perpendicular C B to it, also of any convenient length. On the line A D lay off the greatest pitch off the scale from C to A; then from C towards D lay of seven times the pitch once or twice. according to the sizes of wheels of which the scale is intended to be applied. In the scale given, double of seven times the pitch is laid off, namely. 42 inches; then each of these great divisions being subdivided into 11 equal parts, one of these parts will be equal to four teeth upon the radius of the wheel, so that the whole line CD will be divided into 88 radial pitches. Next on the line C B set off the pitches which may be required in the scale, and through these points draw the 24 parallels to A D. terminating in the lines A B and D B. Then each parallel measured from the line B C to its point of termination in B D, is the radius of a wheel of 88 teeth of the particular pitch marked against it on the line A B. They also express the radii of wheels having less than 88 teeth when measured only to the corresponding point in the line joining B, and the divisional on C D, against which the number of teeth is marked. Thus the radius of a wheel of 52 teeth and 1% pitch, is $r = 15\sqrt{n}$ inches very nearly.

The scale may also be used when the number of teeth exceeds 88; for example, to find the radius of a wheel having 100 teeth. Thus having found the radius answering to 88 teeth, upon the same parallel take off the measure answering to the difference 100-88=12 teeth; and the two measurements are the same parallel take off the measure answering to the difference 100-88=12 teeth; and the two measurements are the same parallel take of the measurements.

sures together will be the radius required.

To adapt the scale to odd numbers of teeth, the first division on the right of C is divided into single radial pitches, so that the radius of any wheel may be measured off without having recourse to calculation of any kind. Thus, for example, if the wheel is intended to contain 50 teeth, the compasses being extended from 52 to the intersection of the parallel answering to the particular pitch to where it meets the line joining Q and B, will give the radius required, that is, a radius answering to 52-2=50 teeth; and any other number of teeth when not marked against the base may be found in the same way.

For the proportions of the teeth, set off $C = \frac{7}{10}$ of the pitch, then will $A = \frac{3}{10}$ of the pitch, which corresponds to

the depth from the point of the tooth to the pitch line. Again, set off C $b = \frac{1}{15}$ th of the 3 inch pitch, and $\frac{1}{15}$ on the parallel against the 1 inch pitch, this will be the thickness of the tooth, allowing from a fifteenth for clearance on the largest pitch, to a tenth on those from % inch and under; and A b will be the width of space, including the Lines being drawn from those points to B comclearance.

plete the diagram. To use the scale, lay off the addendum of the tooth; that is, length beyond the pitch line, equal to A $a=\frac{3}{10}$ pitch, and the same length marked off within the pitch line will give the whole working depth of the tooth, namely, & pitch. Then with the measure $C a = \frac{7}{10}$ pitch in the compasses. mark off the whole length of the tooth, and this will allow at the bottom for clearance. Again, set off the thickness of tooth=Cb, and the space=Ab which will contain the clearance for the particular pitch, varying from 15 to ful-

ly $\frac{1}{10}$ on the small pitches.

The amount of bottom clearance is here presumed to be uniformly 10 of the pitch; but if it be thought advisable to make this vary as in the case of the lateral clearance, it will then be necessary to insert a third line cB in the scale. and so related to a B that the space a c shall be throughout equal to the depth of tooth from the pitch circle to the root, and giving any bottom clearance that may be desired.

Table of Diametral Pitch, with its Equivalent Circular Pitch Opposite on the Adjoining Column.

Diametral	Circular	Diametral	Circular	Circular	Diametral	Circular	Diametral
Pitch.	Pitch.	Pitch.	Pitch.	Pitch.	Pitch.	Pitch.	Pitch.
2 2 1 2 1 2 2 3 3 4 5 6 7 8 9	1.57 1.39 1.25 1.14 1.05 .898 .785 .628 .524 .448 .392 .35 .314	11 12 14 16 18 20 22 24 26 28 30 32	.280 .262 .224 .196 .174 .157 .143 .130 .120 .112 .104 .098	13 in. 11	1.79 2.09 2.18 2.28 2.39 2.51 2.65 2.79 2.96 3.14 3.35 3.59 3.86	34 in. 116 126 127 128 127 128 129 120 120 121 121 122 123 124 125	4.19 4.57 5.03 5.58 6.28 7.18 8.38 10.06 12.56 16.75 25.12 50.24

SIMPLE RULES ON GEARING.

The following rules will apply to both Beyel and Spur Gears. When the term "pitch" is used it always signifies diametral (not circular) pitch.

For illustrations we will use gears having 64 teeth and 8

TO FIND PITCH DIAMETER:-Divide the number of teeth by the pitch: 64÷8=8 in. p. diam.

To FIND No. OF TEETH:-Multiply the pitch diam, by the

pitch: 8 in. ×8=64, No. of teeth.

To FIND THE PITCH:—Divide the number of teeth by the pitch diam. 64+8 in. =8, pitch,

TO FIND OUTSIDE DIAM. OF SPUR WHEELS:-Add 2 to the number of teeth and divide by the pitch: 64+2=66+8=814in. o. d.

To FIND CIRCULAR PITCH: - Divide the decimal 3.1416 the

diametrical pitch: $3.1416 \div 8 = .3927$ in.

TO FIND THE DISTANCE BETWEEN THE CENTERS OF TWO SPUR GEARS:—Divide half the sum of the teeth of both gears by the pitch: 64+64=128+2=64+8=8 in. centers.

A simple rule to determine the face of bevel gears is to make them seven times the pitch: 8 pitch bevel will thus

be % in. face.

The following table gives the breadth of teeth for transmitting with safety, different powers at various speeds. under ordinary circumstances; the width being 210 times the pitch; for increasing the wear, however, in practice. with coarse pitch, the breadth is usually three or four times the pitch.

į.	-kg-d	th.	dth th.	Veloci	Velocity of the wheel at the pitch Circle.						
Pitch.	Thick ness of Teeth.	Length of Teeth.	Breadtl of Teeth.	3 ft. per sec.	4ft.	5 ft. per sec.	7 ft. per sec.	11 ft. per sec.			
Ins.	Ins.	Ins.	Ins.	H.P.	H.P.	H.P.	H.P.	H.P.			
4	1.9	2.8	8.5	19	251	32	45	701			
31	1.6	2.45	7.3	143	194	241	341	54			
3~	1.4	2.1	6.3	11	141	18	34½ 25	391			
21	1.2	1.75	5.2	71	10	$12\frac{1}{2}$	173	271			
2	1.2 0.95	1.4	4.2	43	61	8	11	171			
4 312 3 212 2 114 118	0.83	1.22	3.6	$7\frac{1}{2}$ $4\frac{3}{4}$ $3\frac{1}{2}$ $2\frac{3}{4}$	5	61	81	131			
14	0.71	1.05	3.1	23	31	41	61	10 -			
11	0.59	0.87	2.6	2	21	$egin{array}{c} 4^{rac{1}{2}} \\ 3^{rac{1}{2}} \\ 2^{rac{1}{2}} \\ 2 \end{array}$	41	64			
11	0.53	0.79	2.3	1½ 1½	21	21	31	51			
1	. 0.48	0.7	2.1	11	13	2	24	42			
7	0.41	0.61	1.82	1	12	13	2^{i}_{2}	645 512 425 425 245 215			
3	0.36	0.52	1.57	7.	9		11	21			
5	0.33	0.43	1.31	1	5	3	1	1,7			
7 8 3 4 5 8 1 2	0.24	0.35	1.05	$\frac{7}{10}$ $\frac{1}{2}$ $\frac{3}{10}$	214 35 25 9 10 5 5 2 15	18 3 4 1	10	110			

TABLE FOR CUTTING SCREWS BY LATHE.

f screw.	N O Te	o. f th	f screw.	Number of Teeth.		f screw.	Number of Teeth.			f screw.	Number of Teeth.						
No. of threads per in. of screw.	Mandrel-Pinion.	Leading screw wheel.	No. of threads per in. of screw.	Mandrel-Pinion.	Stud-Wheel.	Stud-Pinion.	Leading screw wheel.	No. of threads per in. of screw	Mandrel-Pinion.	Stud-Wheel.	Stud-Pinion.	Leading screw wheel.	No. of threads per in. o	Mandrel-Pinion.	Stud-Wheel.	Stud-Pinion.	Leading screw wheel.
122223333344444444444444444444444444444	80 1 80 1 80 1 80 1 80 1 10 1 10 1 10 1	90 95 00 10 20 30 40	$ \begin{array}{c} 8\frac{3}{4} \\ 9\frac{1}{2} \\ 10 \\ 10 \\ 11 \\ 12 \\ 12 \\ 13 \\ 14 \\ 14 \\ 14 \\ 14 \\ 16 \\ 16 \\ 16 \\ 16 \\ 16 \\ 17 \\ 17 \\ 17 \\ 18 \\ 18 \\ 18 \\ 18 \\ 18 \\ 18 \\ 18 \\ 18$	60 90 60 90 60 80 90 60 80 80 45	55 85 70 90 60 75 70 55 90 90 90 90 100 110 85 100	20 20 20 20 20 20 20 20 20 20 20 20 20 2	60 90 75 95 65 80 75 120 120 90 110 120 120 120 120 120 140 140	25½ 26 27 27½ 28	30	90	20 20 20 20 20 20 20 20 20 20 20 20	120 150 100 130 120 90 140 150 150 150 140 150 150 150 150 150 150 150 150	32 33 34 35 36 38 39 40 42 44 45 50 52 52 55 56 60 65 70	35 40 30 30 30 30	80 110 85 140 90 95 120 140 110 130 140 120 130 140	20 20 20 20 20 20 20 20 20 20 20 20 20 2	120 120 120 120 120 120 120 120 120 150 150 140 150 140 150 150 150

The foregoing table shows the train of wheels to be used in cutting screws varying in pitch from 1 to 70 threads to the inch; the leading or guide screw is supposed to have two threads per inch, yet may the table be still employed when the leading screw has four threads to the inch, for the same train of wheels would suit for cutting screws of double fineness; and similarly when the leading screw has only 1 thread to the inch, a screw of only one-half the fineness will be produced with any train given in the table.

RULE for GEARING UP ENGINE LATHES for SCREW CUTTING.

Read from the lathe index the number of threads per inch cut by equal gears and multiply it by any number that will give for a product a gear on the index; put this gear upon the stud, then multiply the number of threads per inch to be cut by the same number and put the resulting gear mon the screw.

Example.—To cut 11½ threads per inch, We find on the index that 48 into 48 cuts 6 threads per inch, then

 $6\times4=24$, gear on stud, and $111/9\times4=46$, " " screw

Any multiplier may be used so long as the products include gears that belong with the lathe. For instance, instead of 4 as a multiplier we may use 6.

Thus $6\times6=36$, gear upon stud, and $111/9\times6=69$. "screw.

TABLE giving the proportions of the U. S. or SELLERS, STANDARD threads for screws, nuts and bolts.

Out Side Diam, of Screw in Inches.	Number of Threads per Inch.	Diam. of Screw at the Root of the Thread in Dec. of an Inch.	Width of Top and Bottom Thread in Dec. of an Inch.	Out Side Diam. of Screw in Inches.	Number of Threads per Inch.	Diam. of Screw at the Root of the Thread in Dec. of an.Inch.	Width of Top and Bottom Thread in Dec. of an Inch.
14 5 10 30 7 15 14 10 5 16 16 16 16 16 16 16 16 16 16 16 16 16	20 18 16 14 13 12 11 10 9 8 7 7 6 6 5 5 5	.185 .24 .294 .344 .4 .4 .507 .62 .731 .837 .94 1.065 1.16 1.288 1.389 1.491 1.616	.0062 .0074 .0078 .0089 .0096 .0104 .0113 .0126 .0138 .0156 .0178 .0208 .0208 .0208 .0227 .025	2 14 15 15 15 15 15 15 15 15 15 15 15 15 15	4 4 4 4 5 55 55 55 55 55 70 50 50 50 50 50 50 50 50 50 50 50 50 50	1.712 1.962 2.176 2.426 2.629 2.879 3.1 3.567 3.798 4.028 4.256 4.48 4.73 4.953 5.203 5.423	.0277 .0277 .0312 .0312 .0357 .0384 .0413 .0435 .0435 .0476 .05 .05 .05 .05 .05 .05 .0555

TABLE showing the number of THREADS to the inch for each diameter of SCREW bolts and SCREW taps.

(ENGLISH STANDARD.)
Screw bolts. Screw taps.

	DUTU	00000.		screw taps.						
am. Ins.	ds he ih.	lam. Ins.	s'ds	V-Th	reads.	Sq. Tap	er T's.			
Diam. in Ins.	Thre'ds to the Inch.	Diam in Ins	Thre'ds to the Inch.	Diam. in Ins.	T'ds to In.	Diam. in Ins.	T'ds to In.			
16 14 56 57 6 12 56 53 47 5 1 16 14 35 1 17 56 53 47 5 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	24 20 18 16 14 12 11 10 9 8 7 7 6 6 5 5 5 4 1 4 1 2	214-224 2223 333 34 44-224 4 45 55 55 6	4 4 33 33 4 3 2 2 2 2 2 2 2 2 2 2 2 2 2	50 100 110 01600 120 50 50 110 110 110 110 110 110 110 110	18 16 14 12 11 11 10 10 9 8 8 7 7 6 6 5 5	100 P10 P0 P10 P10 P10 P10 P10 P10 P10 P	998777766665443332412			

Proportions of Flange and Solid half-lap Couplings.

			Fle	ange					$H\epsilon$	$\mathit{ulf-L}$	ap.	
Diam. of Shaft.	Diameter of Flange.	Thickness of Flange.	Diam. of Boss.	Depth of Boss.	No. of Bolts.	Diam. of Bolt.	Diam. of Circle of Bolts.	Diam. of Shaft.	T'ck's of Metal.	D. of Coupling.	Length of Coup.	Length of Lap.
Ins 1 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	Ins 5 6½ 8 9½ 11 12½ 14 15½ 17	$\begin{array}{c} \text{Ins} \\ ^{34} \\ ^{78} \\ ^{16} \\ ^{136} \\ ^{13} \\ ^{13} \\ ^{125} \\ ^{128} \\ ^{2} \\ ^{21} \end{array}$	Ins 2444 344 5444 78 8788 934 112	$\begin{array}{c} \text{Ins} \\ 2 \\ 2\frac{1}{2} \\ 3 \\ 4 \\ 4\frac{1}{2} \\ 5 \\ 5 \\ 6 \\ 7 \end{array}$	Ins 3 4 4 4 4 6 6 6 6 6	Ins 1 1 1 1 1 1 1 1	Ins 3½344 6 744 8½3 934 11 12½ 13½ 16	Ins 1 1 2 2 2 2 2 2 2 2 2 2	Ins 1 1234 2 225834 225834	Ins 3 4½ 5½ 6½ 7¼ 8¼ 9 9¾ 10½	Ins 544 814 934 1078 1288 1348 1534	Ins 1 138 129 2187 814 38 4

Flange Couplings are a common and useful kind for

small and medium shafts, up to about 6 in. diameter.

Solid Couplings are perhaps the best of all for small shafts up to, say, 41/2 or 5 inches diameter, for large shafts they become clumsy and heavy.

TABLE of the DIAMETERS and CIRCUMFERENCES of angle iron hoops, with angles inside and outside.

From 6 inch to 6 feet diameter.

Diam- eter.	Angle Outward Circum- ference.	Angle Inward Circum- ference.	Diam- eter.	Angle Outward Circum- ference.	Angle Inward Circum- ference.
Ft. in. 6 6 7 0 8 9 10 11 1 2 2 1 1 2 2 2 3	Ft. in. 58-18-18-28 112 112-24-18-28 112 2 2 2 112 2 2 2 2 2 2 3 3 3 10-48-48-48-48-48-48-48-48-48-48-48-48-48-	Ft. in. 1 815 74 816 11 13 815 74 816 14 14 14 16 16 16 16 16 16 16 16 16 16 16 16 16	Ft. in. 45 67 8 9 0 11 0 3 6 9 0 3 6 9 0 5 5 5 6	Ft. in. 6 10 7 1 77 65534 8 8 3554 8 9 951 10 11 7555 11 12 22 13 14 17 15 4555 16 10 17 7	Ft. In. 344-1814

In the Table of Angle Outwards, the breadth or thickness of the Angle Iron must be added to the circumference; thus—suppose you require to form a ring of 2 inch Angle Iron, 1 ft. 6 in. inside diameter add 2 in. to the diameter=1 ft. 8 in. and you will find the circumference or length of Iron to be 4 ft. 11% in.

In the Table of Angle Inwards, the above rule is reversed, and the breadth or thickness of Iron must be subtracted from the outside diameter; thus—required a ring of 3 in. Angle Iron 2 ft. outside diameter, subtract 3 in. from the diameter=1 ft. 9 in. and you will find the circumference or length of Iron to be 5 ft. 1178 in.

Table showing the proper thickness for Steam-Cylinders, from 6 to 90 inches in diameter.

Diam. of	Thick-	Diam. of	Thick-	Diam. of	Thick-	Diam. of	Thick-
Cylinder.	ness.	Cylinder.	ness.	Cylinder.	ness.	Cylinder.	ness,
Ins. 6 8 10 12 14 16 18 20 22 24 26	Ins. .44 .545 .65 .755 .86 .965 1.07 1.175 1.28 1.385 1.49	Ins. 28 30 32 34 36 38 40 42 44 46 48	Ins. 1.595 1.7 1.805 1.91 2.015 2.12 2.225 2.33 2.435 2.54 2.645	1ns. 50 52 54 56 58 60 62 64 66 68 70	Ins. 2.75 2.855 2.96 3.065 3.17 3.275 3.38 3.485 3.59 3.695 3.8	Ins. 72 74 76 78 80 82 84 86 88 90	Ins. 3.905 4.01 4.115 4.22 4.325 4.43 4.535 4.64 4.745 4.85

PROPORTIONS OF PLUMMER-BLOCKS.

		-				
Diam. of Bearing.	Length of Bearing.	Height to Center.	Length of Sole.	Center of Hold- down b'lt.	Diam. of Bolts.	Size of Holes for Bolts.
Ins. 11/2 21/2 33/2 41/2 55/2 67 8 9 10 111 12	Ins. 21/2 3 1/2 4 4 1/2 5 1/2 6 6 1/2 7 8 9 10 11 12 13	Ins. 214 4 4 5 6 7 8 9 1 11 12	Ft. In. 0 9 1012 1 112 1 1 3 1 1 4 6 1 7 12 1 1012 2 5 6 12 2 8 0 3 0	Ft. In. 0 7 0 8 9½ 0 10½ 1 0½ 1 1½ 1 1 1 1 1 1 1 1 1 1 1	Inches. 1 11 12 11 11 11 11 11 11 11 11 11 11	In.

Proportions of Sunk Keys for Wheels and Pulleys.

Diam. of shaft in Ins.	1	2	3	4	5	6
Breadth of key.	3/8	34	.43	11/8	13/8	15/8
Thickness of key.			.43	.52	.61	.71
Depth sunk in shaft.	.10	.125	.15	.175	.20	.225
Depth sunk in wheel.	.15	.215	.28	.345	.41	.485
Diam. of shaft in Ins.	7	8	9	10	11	12
Breadth of key.	17/8	21/8	23/8	25/8	27/8	31/8
Thickness of key.	.80		.98	1.07	1.16	1.25
Depth sunk in shaft.	.25	.275	.30	.325	.35	.375
Depth sunk in wheel.	.55	.615	.68	.745	.81	.875

The depth sunk in the shaft and in the wheel is measured at the side of the key, and not at its center:

The thickness of METAL round the EYE of PULLEYS.

4040	Diameter of Shaft in Inches.										
e T L	1	2	3	4	5	6					
J#37 -		Thick	ness round	l eye in	inches.						
1 2 3 4 5 6 7 8 9	18	1 11014500 12016	11.55 14.555 15.55 14.755 14.755 14.755 2 14.55	136 125 56 57 15 15 15 15 15 15 15 15 15 15 15 15 15	1½ 1½ 1½ 1½ 1½ 1½ 1½ 1½ 1½ 1½ 1½ 1½ 1½ 1	15/8 147/8 2 15/8 2 14/3 2 12/2 2 12/2					

Table of the greatest admissible distances between the bearings of continuous shafts, subject to no transverse strain except from their own weights.

Diam.	Distance bearings		Diam.	Distance between bearings in feet.			
in Ins.	Wrought iron. Steel.		in Ins.	Wrought iron.	Steel.		
1 2 3 4 5 6	12.27 15.46 17.70 19.48 20.99 22.30	12.61 15.89 18.19 20.02 21.57 22.92	7 8 9 10 11 12	23.43 24.55 25.53 26.44 27.30 28.10	24.13 25.23 26.24 27.18 28.05 28.88		

AVERAGE CUTTER SPEED AND FEED ON SOFT CAST IRON SURFACES.

The figures are adapted to calculations in milling upon soft cast-iron surfaces, and are subject to change to accompany variations in condition and character of work. order to figure accurately upon milling work, the speed of cutter and amount of feed per revolution must be observed that known, the computation is simple, as follows: Multiply the number of revolutions of cutter per minute by the length of feed at one revolution and the product is inches per minute that can be milled. Allowing about 40 ft. per minute for surface speed of cutter, a ½ inch cutter should run at 300 revolutions per minute, with a feed of 1-150 of an inch to a revolution, giving a result of 2 ins. of light milling per minute. An inch cutter would make 150 revolutions per minute, with a feed of 1-100 of an inch on a moderately heavy cut, allowing 11/2 inches of milling per minute. A 3 inch cutter would run 50 revolutions per minute, with a feed of 1-50 of an inch on heavy work, giving a result of 1 inch of milling per minute. The above are examples selected from observed results in practical shop usage.

The following table of metallic baths is given in PARKES CHEMICAL ESSAYS.

No.	Edge tools to be tempered	Compos of the b	Tem. Far.			
110.	in the various baths.	Lead.	Lead. Tin.			
1	Lancets, in a bath composed of	1 7 1	4	420°		
2	Other Surgical Instruments.	71 8	4	430°		
3	Razors, &c.,	8	4	4420		
1 2 3 4	Pen knives and some imple-					
_	ments of Surgery.	81	4	450°		
5	Larger pen knives, scalpels &c,	10	4	470°		
5 6	Scissors, shears, garden hoes,					
•	cold chisels, &c.	14	4	490°		
7	Axes, firmer chisels, plane		-	1		
•	irons, pocket knives, &c.	19	4	509°		
8	Table knives. large shears, &c.	30	4 4 4	530°		
8	Swords, watch springs, &c.	48	â	550°		
10	Large springs, daggers, augers,	10	•	000		
10	small fine saws, &c.	50	2	558°		
11	Pit saws, hand saws, and some	Boilin		000		
11	particular springs.	Linseed		600°		
12	Articles which we require to be	Melting		000		
14	still somwhat softer.			612°		
	Sun Sumwhat Suiter,	Lead.		014		

TEMPERING STEEL.

2	A shade of darker "	440° \ metals.
3	Darker straw "Still darker straw "	470° For wood & 490° screw taps.
5 6 7	A brown A yellow, tinged slightly with purple. Light purple.	500° Hatchets, 520° chisels, 530° saws, &c.
8	Dark '' Dark blue.	550° Springs.
10 11 12	Paler " Still paler blue. Still paler blue, with a tinge of green	590° Too soft for 610° the above .630° purposes.

TEMPERING RECIPES.

CASE-HARDENING with PRUSSIATE of POTASH.—Heat the articles after polishing to a bright red, rub the surface over with the prussiate of potash, allow it to cool to a dull red, and immerse it in water.

CASE-HARDENING MIXTURES.—Three parts of prussiate of potash to one part of sal-ammoniac, mixed, or two parts of sal-ammoniac, two parts of bone dust, and one part of prussiate of potash.

CASE-HARDENING.—Place horn, hoof, bone-dust, or shreds of leather, together with the article to be case-hardened, in an iron box subject to a blood-red heat, then immerse the article in cold water.

TEMPERING BORING INSTRUMENTS.—Heat the tool to a blood-red heat; hammer it until it is nearly cold; reheat it to a blood-red heat, and plunge it into a mixture of 2 ozs. each of vitriol. soda: sal-ammoniae and spirits of nitre, 1 oz. of oil of vitriol, 1/2 oz. of saltpeter, and 3 gallons of water. retaining it there until it is cold.

TO GIVE IRON A TEMPER TO CUT PORPHYRY.—Make your iron red-hot, and plunge it into distilled water from nettles, and acanthus, or in the very juice pounded out from these plants.

TEMPERING BATHS FOR STEEL.—Twenty gallons of spermaceti oil; 20 lbs. beef suet rendered; 1 gallon of neatsfoot oil; 1 lb of pitch; 3 lbs. black resin.

These two last articles must be previously melted together, and then added to the other ingredients; when the whole must be heated in a proper iron vessel, with a close cover fitted to it, until the moisture is entirely evaporated, and the composition will take fire on a flaming body being presented to its surface, but which must be instantly extinguished again by putting on the cover of the vessel.

This recipe will only last for a few weeks constant use.

FOR SAWS &C.—The composition is 2 lbs. suet, and a 14 bt. of beeswax to every gallon of whale-oil, these are boiled together, and will serve for thin works and most kinds of steel. The addition of black resin, to the extent of about 1 lb; to the gallon, makes it serve for thicker pieces and for those that refused to harden before; but the resin should be added with judgment, or works will become too hard and brittle. The composition is useless when it has been constantly employed for about a month; the period depends, however, on the extent to which it is used, and the, trough should be thoroughly cleaned out before new mixture is placed in it.

Practical Thickness in Decimals of an Inch of Good

Plate Iron in Steam-Boilers, Single Riveted.

P—Steam pressure in pounds per square inch above atmosphere.

-	1	DIAM	ETER (of Boile	r in Ir	iches.		
<i>P</i> .	10 15	20 25 30	35 40	50 60	70 80	90 10	00 120	150
10 15	.10 .10 . .10 .10 .	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$.12 .13	1.13 . 14			15 .16	
20	.11 .11 .	12 .12 .13	.14 .14	.15 .16	.17 .18	.20 .2	$ \begin{array}{c c} 19 & .19 \\ 20 & .22 \end{array} $.22
$\frac{25}{30}$		$\begin{array}{c c} 12 & 13 & 14 \\ 13 & 14 & 14 \end{array}$					23 .25 25 .28	,30 .33
40 50		$\begin{array}{c ccccccccccccccccccccccccccccccccccc$.28 .3	30 .34 35 .40	.40 .47
60	.14 .14 .	16 .17 .19	.20 .22	.25 .28	.32 .34	.37 .4	10 .46	.55
70 80	.15 .16 .	17 .18 .20 $18 .20 .22$.23 .26	.30 .34	.38 .42	.46	$\begin{array}{c c} 15 & .52 \\ 50 & .58 \end{array}$.60 .70
90 100		$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		$\begin{bmatrix} .32 \\ .35 \end{bmatrix} .40$			$\begin{array}{c c} 55 & .60 \\ 60 & .70 \end{array}$.77 .85
120 150	.16 .19 .	22 .25 .28 26 .30 .33	.31 .34	.40 .46	.52 .58	.60 .'		1.00
200		$\frac{20}{30} .35 .40$						

Facts for Boiler Makers.

Rankine's Riveting Rules.—Diameter of Rivet for Plates less than 1/2 'thick to be equal to twice the thickness of the plate. For plates 1/2 and upwards 11/2 times thickness of plate. The length of rivet iron required to make the "head" equals 21/2 times the diameter of the rivet.

Boiler Maker's Rule.—In addition to the thickness of the plates the following allowance is made for the head, both giving the whole length of rivets.

RIVET.	COLD RIVETED.	HOT RIVETED.
3/8 inch.	5/8 inch.	
1/2 "	34 ···	78 inch.
34 "		11/8 "

For boilers the rivets are 134 inch from center to center in single riveting, and 2 inches in double riveting; flues the same.

To have a tight fit in the sections for a boiler or other tubular work, make the inside diameter of the inside tube equal to the inside diameter of the outside tube, less 6 times the thickness of the iron.

Fairbairn's Table of Dimensions of Rivets for Boilers.

Thick.of Plate in Inches.	Diam. of Rivet in Ins.	Length of Rivet to head in Ins.	Pitch in inches.	single Joints	double Joints	Equiv't. length of Head in Ins.
366 456 FR 129 F 50 F 60	36 56 11 10 11 11 11 11 11 11 11 11 11 11 11	1100000 14 12 22 23 31 4 15 15 15 15 15 15 15 15 15 15 15 15 15	144-1515534 1215534 2214-151534 2214-151534 2214-151534	14-18-7-18 11-12-7-18 12-7-18-18-18-18-18-18-18-18-18-18-18-18-18-	21-6 21-6 21-6 23-6 23-6 24-16-6 25-7 25-7 25-7 25-7 25-7 25-7 25-7 25-7	121500047,0 -4450-215004

Lloyd's Rule for Shipbuilding.

Diam of Rivets.	1	5/8"		3/4"			7/8"			1"		
Thick- ness of Plates:	5 16	" 6 16	7 16	, 16	9 16	10 16	11 16	12 16	13 16	" 14 16	15 16	1

Rivets to be $\frac{1}{4}$ larger in diameter in the stem stern post, and keel.

Boiler pressure allowed as per Government Rule—Diameter of Boiler in inches.

EXAMPLE.—Pressure allowed for Boiler 8 feet diameter, 3-8 iron, $8 \times 12 = 96 \div 6.930 = 72.18$ pounds.

Table showing the Diminution of Iron Boiler-Plates at High Temperatures; the maxim Tenacity being at 550°=65.000 lbs. per square

inch.

Table showing the Diminution of strength of Cop-per Boiler-Plates by addition to the Temperature the cohesion at 32° being 32.800 lbs. per square inch.

	Ti Oie Di	oucis.		Copper Boners.						
Temp. obser- ved.	Dim. of Tenac'y obser'd.	Temp. obser- ved.	Dim. of Tenac'y obser'd.	Temp. above 32°	Dim- inu- tion.	Tem. above 32°	Dim- inu- tion.			
550°	1.0000	824°	.2010	N.						
570°	.0869	932°	.3324	90°	.0175	660°	.3425			
596°	.0899	9470	.3593	180°	.054	769°	.4398			
600°	.0964	1030°	.4478	270°	.0926	812°	.4944			
630°	.1046	1111°	.5514	360°	.1513	880°	.5581			
662°	.1155	1115°	.6000	450°	.2046	984°	.6691			
722°	.1436	1159°	.6011	460°	.2133	1000°	.6741			
732°	.1491	1187°	.6352	513°	.2446	1200°	.8861			
734°	.1535	1237°	.6622	529°	.2558	1300°	1.0000			
766°	.1589	1245°	.6715			-				
770°	.1627	1317°	.7001							

Table Given Horse-Power of Boilers the Sizes: at 60 lbs. Pressure. Following

:sui [leus :mpid 7277266666666666666666666666666666666	Length shell.ft.	Num. Tubes.	Length Tubes. Feet.	Diam. Tubes. Inches.	Heating surface Square Ft.	Horse-Power.	Diam. shell Ins.	Length shell.ft.	Num. Tubes.	Length Tubes. Feet.	Diam. Tubes. Inches.	Heating surface Square Ft.	Horse-Power.
72	18 16 16 15	70	18	4	1502	100	54 48 48 48 48 48 48	12 16 16 15 14 13 12	60	12 16 16	3	624 683 684 642 600 555 513 542 495 508 476 441 408 390 355	41
72	16	$\frac{90}{112}$	16	31	1472	98	48	16	40	16	31	683	46
72	16	112	18 16 16 15 18 17 16 16 15 14 13 18 17 16 16 16 15	3	1596	98 99 93 80 76 72 72 68 63	48	16	60 40 49 49	16	3~	684	46
7 2	15	112 65 65	15	3	$1400 \\ 1200$	93	48	15	49	15	3	642	43
60	18 17	65	18	$3\frac{1}{2}$	1200	80	48	14	49	14	3	600	40
60	17	65	17	$3\frac{1}{2}$	1148	76	48	13	49 49	13 12 11	3	555	37
60	16	65	16	$3_{\frac{1}{2}}$	1075	72	48	12	49	12	3	513	34
60	16 15	80	16	3	1088	72	48	11	65 65	11	$2\frac{1}{2}$	542	36
60	15	80 80 80	15	3	1020	68	48	10 15 14 13	65	10 15	$2\frac{1}{2}$	495	33
60	14	80	14	3	952	63	42 42	15	38 38 38 38	15	3	508	34
60	13	80	13	3	884	59	42	14	38	14	3	476	32
54	18 17	50	18	$3\frac{1}{2}$	951	63	42	13	38	13	3	441	30
54	17	50	17	$3\frac{1}{2}$	900	60	42	12	38	12	3	408	27
54	16	50	16	31	795	53 55	42	11	45	11	$2\frac{1}{2}$	390	26
54	16	60	16	3	832	55	42	10	45 45 45	10	$2\frac{1}{2}$	355	24
54	15	60	15	3	780	52	42	9	45	9	$2\frac{1}{2}$	320	22
54	14	60	14 13	4	1148 1075 1088 1020 952 884 951 900 795 832 780 728 676	48 45	42	8 7	45 45	8 7	3333333333333333333333333	285	41 46 46 43 40 37 34 36 33 34 32 27 26 24 22 19 16
54	13	60	13	3	676	45	42	7	45	7	21	248	16

ALLOYS and COMPOSITION.

	DEC 1	~ ~	-	70111.	. 000	1110	41.		
Name of Metal.	Copper.	Zinc.	Tin.	Nickel.	Lead.	Antimony.	Bismuth.	Silver.	Cobalt of Iron.
Argentan.	55.	24.	1	121.	1	1	1		1
Argentiferous.	50.	2.5	2.5	40.	2.5	-	Iron	i. 2.5	
Babbitts Metal.	3.7		89.			7.3		1	
Brass Common.	84.3	5.2	10.5		-	1			
66 66	75.	25.						1	
" Engine									
bearings.	50.	1.8	6.5						
" Hard.	79.3		14.3						
" Loc'm'tive		".							100
bearings.	50.	2.5	5.		5.			-	,
" Math'ical	00.		١.		"				
Instrum'ts	92.2		7.8						
" Pinchbeck		20.	•••		1 .				
" R. Tombec		11.2			-				
" Rolled.	74.3	22.3	3.4						
" Tutenag.	50.	31.	0.1	19.	-				
" Tenacious.	88.9	2.8	8.3	10.					
" Wheels.	90.	2.0	10.						
" White.	10.	80.	10.			3.1			
" Wire.	67.	33.	10.						
" Glands.	65.	.5	8.						
" Yellow.	40.	20.	0.						
" Richer.	50.	10.		100					
" Red.		10.			5.			//	
Britannia me'l.	10.	10.	25.		υ.	2.5		1	-
when fus'd add	-		40.			2.5	25.		
Box metal.	80.	10.				4.5	20.	1	
Bronze, Yellow.	100.8		2.4	-					
" Red.	130.5		4.4						
" Alloy.	80.	2.	18.						
" Cymbals.	80.	4.	20.						
" Gun met'l.	90.		10.		- 3		,		
" Guil Het I.	93.		7.						
" Medals.	93.		7.						
" Statuary.	91.4	5.5	1.4		1.7				
Bell metal l'rge.	80.	5.5	20.		1.6				
Chinese Silver.		10.9		13.				2.48	10
" w'te cop'er.	65.1 40.4	25.0		31.6				4.40	12.
Church Bells.	80.		10.1	51.0	4.3		4	_	
" bens.	69.	9.0	31.		4.0				
Clock "	72.		26.5				Inon	1 5	
Electrotype m't.	14.				100	3.	Tron	. 1.5	
Flanges to stand			4.		100.	Э.			
Brazing.	64.	2.			2.				
Diazing.	01.	4.			1 4.				

Alloys and Composition (Continued).

				-				
Name of Metal.	Copper.	Zinc.	Tim.	Nickel.	Lead.	Antimony.	Bismuth.	Iron.
German Silver.	33.3	33.4		33.3	1			
11	40.4	25.4		31.6				2.6
" fine.	49.5	24.		24.				2.5
Gongs,	81.6		18.4					-1.5
Gun Metal for								
bearings.	90.3	9.7	.3					
House Bells.	77.		23.		i			
Lathe Bushes.	80.		20.					
Mach'ery b'r'gs.	87.5		12.5					
hard.	77.4	7.	15.6					
Metal that ex-								
pands in co'ling.	i				75.	16.7	8.3	
Muntz Metal.	90.	60.	-					
Musical Bells.	87.5		12.5			100		
Nickel-Silver		i						500
"com. English	60.	17.8		22.2				
Nickel-S. Paris-	-							
ian.	66.	13.6	- 0	19.3				
Pewter Best.		- 1	86.			14.		
**			80.		20.			
Printing Char-		- 1						
acters.	[80,	20.		
Sheathi'g Metal	56.	45.				000		
Speculum "	66.	-	22.		Arse	enic. 1	2.	
	50.	21.	29.		-00			
Stereotype Met.			10.		100.	16.		
Tough Br'ss En-	100							
gine work.	100.	15.	15.					
Tough Brass	100	ا ر	0=					
heavy bearings.	100.	5.	25.				- 7	
Telescopic Mir-	CC C		99.4					
rors.	66.6		33.4		-			
Temper White Metal.	33.4	11.	$66.6 \\ 42.6$			85.2		1.11
	69.8					00.2		
" " hard.	09.0	40.0	4.4					

Melting points of alloys.

Lead.	Tin.	Bismuth.	Melting Point.
2 parts	3 parts.	5 parts.	212 degrees
1	4 ''	5	246 "
	ī "·	1 "	286 "
	2 "	1 "	336 ''
2 - "	3 "		334 "

Horse-power which can be safely carried by shafts for prime movers gears, well supported by bearings, and making 100 revolutions per Horse-power which can be safely transmitted by shafts making 100 revolutions per minute, in which the transverse strain, if any, need not be considered.

	min	ute.				consider	red.
Diam. in Ins.	Wr'ght Iron.	Steel.	Cast- Iron.	Diam. in Ins.	Wr'ght Iron.	Steel.	Cast- Iron.
1.20 1.25 1.50	H. P. 1.00 1.95 3.37	H. P. 1.60 3.12 5.39	H. P. 0.60 1.17 2.03	1.20 1.25 1.50	H. P. 2.00 3.90 6.74	H. P. 3.20 6.24 10.78	H. P. 1.20 2.34 4.06
1.75 2.00 2.25 2.50	5.36 8.00 11.39 15.62	8.58 12.80 18.22 24.99	3.22 4.80 6.83 9.37	1.75 2.00 2.25 2.50	10.72 16.00 22.78 31.24	17.16 25.60 36.44 49.98	6.44 9.60 13.66 18.74
2.75 3.00 3.25	20.80 27.00 34.33	33.28 43.20 54.93	12.48 16.20 20.60 25.72	2.75 3.00 3.25	41.60 54.00 68.56 85.74	66.56 86.40 109.86 137.18	24.96 32.40 41.20
3.50 3.75 4.00 4.25	42.87 52.73 64.00 76.77	68.59 84.37 102.40 122.83	31.64 38.40 46.06	3.50 3.75 4.00 4.25	105.46 128.00 153.54	168.74 204.80 245.66	51.44 63.28 76.80 92.12
4.50 4.75 5.00 5.25	91.12 107.17 125.00 144.70	145.79 171.47 200.00 231.52	54.67 64.30 75.00 86.82	4.50 4.75 5.00 5.25	182.24 214.34 250.00 289.40	291.58 342.94 400.00 463.04	109.34 128.60 150.00 173.64
5.50 5.75 6.00 6.25	166.37 190.11 216.00 244.14	266.19 304.18 345.60 390.62	99.82 114.06 129.60 146.49	5.50 5.75 6.00 6.25	332.74 380.22 432.00 488.28	532.38 608.36 691.20 781.24	199.64 228.12 259.20 292.98
6.50 6.75 7.00 7.25	274.62 307.55 343.00 381.08	439.39 492.08 548.80 609.73	164.78 184.53 205.80 228.65	6.50 6.75 7.00 7.25	549.24 615.10 686.00 762.16	878.78 984.16 1097.60 1219.46	329.56 369.06 411.60 457.30
7.25 7.50 7.75 8.00 8.25	421.87 465.48 512.00 561.52	674.99 744.77 819.20 898.43	253.13 279.29 307.20 336.91	7.50 7.75 8.00 8.25	843.74 930.96 1024.00 1123.04	1349.98 1489.54 1638.40 1796.86	506.26 558.58 614.40 673.82
8.50 8.75 9.00 9.25	614.12 669.92 729.00 791.45	982.59 1071.87 1166.40 1266.32	368.47 401.95 437.40 474.87	8.50 8.75 9.00 9.25	1228.24 1339.84 1458.00 1582.90	1965.18 2143.74 2332.87 2532.64	736.94 803.90 874.80 949.74
9.50 9.75	857.37 926.86	1371.79 1482.98 1600.00	514.43 556.12 600.00	9.50 9.75 10.00	1714.74 1853.72 2000.00	2743.58 2965.96	1028.86 1112.24 1200.00

RULE:—Multiply the power given in the Tables by the number of revolutions made by the shaft per minute; divide the product by 100; the quotient will be the power which can be safely carried.

MOVERS. BEING the FIRST TABLE of the DIAMETER of SHAFTS

11		-
105		22222222222222222222222222222222222222
100		80 24 46 46 46 46 46 46 46 46 46 46 46 46 46
95	-	क्ष अंसर्क्ष अंधर्मान्क अंक
1-1		
1 90		<u> </u>
85		
98		44.44.44.66.66.66.66.66.66.66.66.66.66.6
75	Ë	88 84 86 84 84 84 84 86 86 86 86 86 86 86 86 86 86 86 86 86
20	INCHES	
65	i	20000000000000000000000000000000000000
99	SHAFTS	
22	SHA	80 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8
09	of	ಯಭ್ಯಭ.4.4.4.4.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.
45	TER	800 140 140F F0140 1
9	DIAMETER	80044444400000000000000000000000000000
35	А	$\frac{2}{2}$
30		844444900000000000000000000000000000000
72		44444000000000000000000000000000000000
20		44.0.0.0.0.0.0.0.1.2.2.2.2.2.0.0.0.0.0.0.0
15		2.50
10		
OYSe OWei		40000000000000000000000000000000000000

Transmitting Efficiency of Iron shafting at different speeds, as Prime mover or Head shaft carrying Main Driving Pulley or gear well supported by bearings.

COLD ROLLED IRON SHAFTING.

of Ins.		Nu	ımber	of Re	volutio	ons per	r Minu	ite.						
E E	60	80	100	125	150	175	200	250	300					
Diam. Shaft, 1		Horse-Power.												
11/2	2.7	3.6	4.5	5.6	6.7	7.9	9:0	11.	13.					
13/4	4.3	5.6	7.1	8.9	10.6	12.4	14.2	18.	21.					
2	6.4	8.5	10.7	13.	16.	19.	21.	- 26.	32.					
21/4	9.	12.	15.	19.	23.	26.	30.	38.	46.					
21/2	12.	17.	21.	26.	31.	36.	41.	52.	62.					
$23\sqrt{4}$	16.	22. 29.	21. 27.	34.	31. 41. 54. 68.	48.	55.	70.	62. 82.					
3	21.	29.	36.	45.	54.	63.	72.	90.	108.					
31/4	27.	36.	45. 57.	57.	68.	80.	91.	114.	136.					
31/2	34.	45.	57.	71.	87.	100.	114.	142.	172.					
33/4	42.	56.	70.	87.	105.	123.	140.	174.	210.					
4	51.	69.	82.	106.	128.	149.	170.	212.	256.					
41/2	73.	97.	121.	151.	182.	212.	243.	302.	364.					

TURNED IRON SHAFTING.

of Ins.		N	umber	of Re	volutio	ns per	Minu	te.						
E E	60	80	100	125	150	175	200	250	300					
Diam. of Shaft. Ins.		Horse-Power.												
13/4	2.6	3.4	4.3	5.4	6.4	7.5	8.6	10.7	12.9					
21/4	3.8	5.1	6.4	8.	9.6	11.2	12.8	16.	19.2					
21/4	5.4	7.3	8.1	10.	12.	14.	16.	20. 31.	24. 37.					
21/2 23/4 3	7.5	10.	12.5	15.	18.	22. 28. 35. 47.	25. 32.	31.	37.					
23/4	10.	13.	16.	20.	24. 30.	28.	32.	40.	48.					
3	13.	17.	20.	25. 34.	30.	35.	40.	50.	60.					
31/4	16.	22.	27.	34.	40.	47.	54. 68.	67.	81.					
31/2 33/4	20.	27.	34.	42. 52.	51.	59.	68.	85.	102.					
334	25.	33.	42.	52.	63.	73.	84.	105.	126.					
4 .	30.	41.	51.	64.	76.	89.	102.	127.	153.					
41/2 5	43.	58.	72.	90.	108.	126.	144.	180.	216.					
5	60.	80.	100.	125.	150.	175.	200.	250.	300.					

To find the Horse-Power of other speeds not in the table.

RULE.—Multiply the power given in the 100 revolutions column, by the number of revolutions made by the shaft per minute; divide the product by 100; the quotient will be the power which can be safely carried.

Transmitting Efficiency of Iron shafting at different speeds, as Second movers of Line shafting, Bearings 8 feet apart.

COLD ROLLED IRON SHAFTING.

of Ins.		N	umber	of Re	volutio	ns per	Minut	e.	,					
£.	100	125	150	175	200	225	250	300	350					
Diam. Shaft.		Horse-Power.												
11/2	6.7	8.4	10.1	11.8	13.5	15.2	16.8	20.	23.					
15/8	8.6	10.7	12.8	15.	17.1	19.3	21.5	26.	31.					
134	10.7	13.4	16.	18.7	21.5	24.2	26.8	32.	39.					
178	13.2	16.5	19.7	23.	26.4	29.6	32.9	39.	46.					
2	16.	20.	24.	28.	32.	36.	40.	48.	56.					
21/8	19.	24.	29.	33.	38.	43.	48.	57.	67.					
21/4	22.	28.	34.	39.	45.	50.	56.	68.	80.					
$\frac{21}{4}$	27.	33.	40.	47.	53.	60.	67.	70.	94.					
21/2	31.	39.	47.	54.	62.	69.	78.	93.	109.					
21/2 23/4	41.	52.	62.	73.	83.	93.	104.	125.	145.					
3	54.	67.	81.	94.	108.	121.	134.	162.	189.					
31/4	68.	86.	103.	120.	137.	154.	172.	205.	240.					

TURNED IRON SHAFTING.

of Ins.		Nu	mber	of Re	volutio	ons pe	r Min	ute.	
	100	125	150	175	200	225	250	300	350
Diam. Shaft.				Ног	se-Pov	VER.			
134 178	6.	7.4	8.9	10.4	11.9	13.4	14.9	17.9	20.9
17/8	7.3	9.1	10.9	12.7	14.5	16.3	18.2	21.8	25.4
2	8.9	11.1	13.3	15.5	17.7	20.	22.2	26.6	31.
21/8	10.6	13.2	15.9	18.5	21.2	23.8	26.5	31.8	37.
21/4	12.6	15.8	19.	22.	25.	28.	31.	38.	44.
21/8 21/4 23/8	15.	18.	22.	22. 26.	29.	33.	37.	44.	37. 44. 52.
$21/_{2}$	17.	21.	19. 22. 27.	30.	34.	39.	43.	52.	60.
21/2 23/4 3	23. 30.	29.	34.	40.	25. 29. 34. 46.	28. 33. 39. 52.	58.	69.	81.
3	30.	37.	45.	52.	60.	67.	75.	90.	105.
31/4	38.	47.	57.	66.	76.	85.	95.	114.	133.
31/2	47.	59.	71.	83.	95.	107.	119.	143.	167.
4	71.	89.	107.	125.	142.	160.	178.	213.	249.

To find the Horse-Power of other speeds not in the table. RULE.—Multiply the power given in the 100 revolutions column, by the number of revolutions made by the shaft per minute; divide the product by 100; the quotient will be the power which can be safely carried.

Transmitting Efficiency of Iron shafting for simply Transmitting Power and short counters.

COLD ROLLED IRON SHAFTING.

of Ins.		Number of Revolutions per Minute.											
ft.	100	125	150	175	200	267	300	367	400				
Diam. Shaft.				Hor	se-Po	WER.		-					
11/4	6.5	8.1	9.7	11.3		17.4	19.5						
13/8	8.5	10.7	12.8	15.	17.	22.7	25.5	31.	34.				
11/2	11.2	14. 17.7	16.8	19.6		30.	33.	41.	45.				
15/8	14.2 18.	22	21.2 27.	24.8 31.	28.4 35.	47	42. 53.	41. 52. 65.	57. 71.				
134 178	22.	27.	33.	38.	44.	30. 38. 47. 58.	65.	79.	87.				
270	26.	33.	40.	46.	53.	71.	80.	97.	106.				
21/8	32.	40.	47.	55.	63.	84	95.	116.	127.				
21/4	38.	47.	57.	66.	76.	101.	114.	138.	152.				
23/8	44.	55.	66.	77.	88.	118.	133.	163.	178.				
21/2	52.	65.	78.	91.	104.	138.	155.	190.	207.				
23/4	69.	84.	99.	113.	138.	184.	207.	254.	277.				

TURNED IRON SHAFTING.

of Ins.	\	Nu	mber	of Re	volutio	ns pe	r Min	ute.	
tt.	100	125	150	175	200	267	300	367	400
Diam. Shaft.				Hor	SE-Pov	VER.			
11/2 15/8	6.7	8.4	10.1	11.8	13.5	17.9	20.3	24.8	
15/8	8.6 10.7	10.7	12.8 16.	15. 18.7	17.1 21.5	22.8	25.8	31.5	
$\frac{134}{178}$	13.2	16.5	19.7		26.4	28. 35. 42.	32.	39. 48.	43. 52.
2'8	16.	20.	24	23. 28. 33. 39. 47.	32.	42.	39. 48. 57. 68.	58.	64
21/2	19.	24.	29. 34. 40.	33.	32. 38. 45. 53. 62.	51.	57.	70.	64. 76.
21/4 23/8 21/2 23/4	22. 27.	28.	34.	39.	45.	60.	68.	83. 96.	90.
23/8	27.	33.	40.	47.	53.	70.	79.	96.	105.
21/2	31.	39.	47.	54.	62.	83.	93.	114.	125.
3	41. 54.	52. 67.	62. 81.	73. 94.	83. 108.	111. 144.	125. 162.	153.	167. 216.
31/4	68.	86.	103.	120.	137.	182.	205.	198. 250.	273.

To find the Horse-Power of other speeds not in the table. RULE.—Multiply the power given in the 100 revolutions column, by the number of revolutions made by the shaft per minute; divide the product by 100; the quotient will be the power which can be safely carried.

Table of Horse-Power which may be transmitted by open Single Belts to Pulleys running 100 Revolutions per minute. The diameters of the Driving and Driven Pulley being equal.

				uney b	eing eq	uai.		
ley.			Width	of Be	lt in I	nches.		
Diam. Pulley.	2	21/2	3	31/2	4	41/2	5	6
of H				Horse-	Power			
Ins. l		I			1	1	I	1
61/6	.44 .47 .51	.54 .59 .64	.65 .71 .76	.76 .83 .89	.87 .95 1.01	.98 1.07 1.14	1.09 1.19 1.27 1.36	1.31 1.42 1.53
7 71/2 8 81/2	.55 58	.68 .73 .77	.82 .87 .93	1.02	1.09 1.16	1.23 1.31 1.39	1.36 1.45 1.55	1.64
$\frac{9}{91/2}$.62 .65 .69 .73	.82	1.04 1.09 1.20	1.15	1.31	1.48	1.64	1.86 1.97 2.08
10 11 12	.73 .80 .87 .95	.91 1.00 1.09 1.18	1.09 1.20 1.31 1.41	1.08 1.15 1.21 1.27 1.40 1.53 1.65	1.24 1.31 1.39 1.45 1.60 1.75 1.89	1.48 1.56 1.63 1.80 1.97 2.12 2.27 2.46	1.81 2.00 2.18	2.18 2.40 2.62 2.83
13 14 15	.95 1.02 1.09	1.27	1.52 1.64	1.77	$\begin{vmatrix} 2.02 \\ 2.19 \end{vmatrix}$	2.12 2.27 2.46	2.36 2.53 2.73	3.05
10 11 12 13 14 15 16 17 18 19	1.16 1.24 1.31 1.39	1.45 1.55 1.64 1.73	1.74	2.03 2.16 2.29	2.32 2.47 2.62	2.61	2.91 3.09 3.27 3.45 3.64	3.48 3.70 3.92
20	1.45	1.73 1.82 1.91	1.96 2.07 2.18	2.29 2.42 2.55 2.67 2.80	2.62 2.76 2.91 3.05	2.95 3.11 3.27 3.44	3.45 3.64 3.82	4.14 4.36 4.58 4.80
21 22 23	1.52 1.60 1.67	2.00 2.09	2.29 2.40 2.51	2.80 2.93	3.20 3.35	3.60	4. 4.18	4.80 5.02
ey.		, - *	Width	of Be	lt in In	nches.		
Diam. Pulle	4	5	6	8	10	12	14	16
of				Horse	-Power	t.		
Ins. 24 25 26	3.5 3.6	4.4 4.5	5.2 5.5	7. 7.3	8.7 9.1	10.5 10.9	12.2 12.7 13.2	14. 14.5
26 27 28	3.8	4.7 4.9 5.1	5.7 5.9 6.1	7.6 7.8 8.1	9.5 9.8 10.2 10.5	11.3 11.8 12.2	13.7	15.1 15.6 16.3
27 28 29 30 31 32 33	4.1 4.2 4.4 4.5 4.7 4.8	5.3 5.4 5.6	6.1 6.3 6.6 6.8	8.4 8.7 9.	10.9	12.6 13.1 13.5	14.8 15.3 15.8	16.9 17.4 18.
34	4.7 4.8 4.9 5.1	5.8 6. 6.2 6.4	7. 7.2 7.4 7.6	9. 9.3 9.6 9.9 10.2	11.6 12. 12.4 12.7	14. 14.4 14.8	15.8 16.3 16.8 17.3	18. 18.6 19.2 19.8
35	5.1	6.4	7.6	10.2	12.7	15.3	17.9	20.4

HORSE-POWER OF BELTS-(Continued).

Width of Belt in Inches.

E F					_					
of J	HORSE-POWER.									
36 37 38 39 40 42 44 46 48 50 66 67 78 84	5.2 5.4 5.5 5.7 5.8 6.1 6.7 7.2 7.8 8.8 9.6 10.4 11.4 12.2	6.5 6.7 6.9 7.1 7.3 7.6 8.4 8.8 9.8 10.8 12. 13. 14.2 15.2	7.8 8.1 8.3 8.5 8.7 9.2 9.6 10.4 10.9 11.8 13.1 14.4 15.6 17.	10.5 10.8 11. 11.3 11.6 12.2 12.8 13.4 14. 14.6 15.6 17.4 19.2 21. 22.6 24.4	13.1 13.5 13.8 14.2 14.7 15.3 16. 16.7 17.4 18.2 21.8 24. 26.2 28.4 30.6	15.7 16.2 16.6 17. 17.5 18.2 20.1 21. 21. 23.6 26.2 28.8 31.4 34.	18.3 18.9 19.3 19.9 20.4 21.4 22.4 23.4 24.4 25.4 26.4 30.6 33.6 36.6 39.8 42.8	20.9 21.5 22.1 22.7 23.3 24.3 25.6 26.8 29. 31.2 34.8 38.4 41.8 45.4 48.6		
- X	Width of Belt in Inches.									
Diam. Pulle	18	20	22	24	26	28	30	32		
of	-			Horse	-Power	₹.				
Ins. 24 30 36 38 40 42 44 48 50 66 72 78 84 96 120 144	16 19 24 25 26 28 29 31 33 35 39 47 51 55 63 78	17 222 226 28 29 31 32 35 36 39 44 48 52 57 61 70 88 104	19 24 29 30 32 34 35 38 40 43 48 53 58 62 67 76 96 116	21 26 31 33 35 36 38 42 44 47 52 58 68 73 84 104 126	23 28 34 36 38 40 42 45 50 57 62 68 74 79 90 114 136	24 31 37 39 41 43 45 49 51 61 67 73 80 86 86 98 122 146	26 33 39 41 44 46 48 52 54 58 65 72 78 85 91 104 130 156	28 35 42 44 47 49 51 56 58 62 70 77 84 91 112 140 168		

The Horse-Power of Double Belts is 10-7 of that given in the Tables.

RULE:--Multiply the power given in the Tables by the number of revolutions made by the pulley per minute; divide the product by 100, the quotient will be the power transmitted.

The following table exhibits the necessary width of belts to transmit different number of Horse-Power.

4 4		Diam	eter o	of Pul	leys a	nd Dr	ums i	n feet		
Horse- Power.	2	3	4	5	6	7	8	1 9	10	
FA	Width of Belt in Inches.									
1 2 3 4 5 6 7 8	1.8	1.2	$0.9 \\ 1.8 \\ 2.7$	0.7	0.6	0.5	0.45		0.3	
2	3.6	2.4	1.8	1.4	1.2 1.8	1.0	0.9	0.8	0.7	
3	$\frac{5.4}{7.2}$	3.6	2.7	2.1	1.8	1.5	0.9 1.3 1.8 2.2 2.7 3.1 3.6	1.2	1.0	
4	7.2	4.8	3.6 4.5 5.4 6.3 7.2 8.1	2.9 3.6 4.3 5.0 5.7	2.4 3.0	2.0 2.5	1.8	1.6	1.4 1.8	
5	9.0	6.0 7.2	4.5	3.6	3.0	2.5	2.2	2.0	1.8	
6	10.8	7.2	5.4	4.3	3.6	3.0	2.7	2.4	2.1	
7	12.6	8.4	6.3	5.0	4.2	3.5	3.1	2.8	2.5	
8	14.4 16.2	9.6	7.2	5.7	3.6 4.2 4.8	4.1	3.6	2.4 2.8 3.2	2.8	
9	16.2	10.8	8.1	6.4 7.2 8.6	5.4	4.6	4.0	3.6	2.8 3.2 3.6	
10 12	18.0	12.0	9.0	7.2	6.0 7.2	5.1	4.5 5.4 6.3 7.2	4.0	3.6	
12	21.6 25.2 28.8	14.4	10.0	8.6	7.2	6.1	5.4	4.8	4.3	
14 16	25.2	16.8	12.6	10.0	8.4	7.1	6.3	5.6	5.0 5.7	
16	28.8	19.2	14.4	11.5	9.6	8.2	7.2	6.4	5.7	
18	32.4	21.6	16.2	12.9	10.8	9.2	8.1	7.2	6.4	
20	36.0	24.0	18.0	14.4	12.0	10.2	9.0	8.0	7.2	
25	45.0	30.0	22.5	18.0	15.0	12.8	11.2	10.0	9.0	
30	54.0	36.0	27.0	21.6	18.0	15.4	13.5	12.0	10.8	
35	63.0	42.0	31.5	25.2	21.0	17.9	15.7	14.0	12.6	
40	72.0	48.0	36.0	28.8	24.0	20.5	18.0	16.0	14.4	
45	81.0	54.0	40.5	32.4	27.0	23.1	20.2	18.0	16.2	
50	90.0	60.0	45.0	36.0	30.0	25.7	22.5	20.0	18.0	
55		66.0	49.5	39.6	33.0	28.2-	24.7	22.0	19.8	
55 60 65		72.0	54.0	43.2	36.0	30.8	27.0	24.0	21.6	
65		78.0	58.5	46.8	39.0	33.4	29.2	26.0	23.4	
70		84.0	63.0	50.4	42.0	35.9	31.5	28.0	25.2	
75			67.5	54.0	45.0	38.5	33.7	30.0	27.0	
80			72.0	57.6	48.0	41.1	36.0	32.0	28.8	
85			76.0	61.2	51.0	43.6	38.2	34.0	30.6	
90		1	81.0	64.8	54.0	46.2	40.5	36.0	32.4	
95				68.4	57.0	48.8	42.9	38.0	34.2	
100				72.0	60.0	51.4	45.0	40.0	36.0	

EXAMPLE.—What should be the width of belt to transmit 14 horse-power from a water wheel, having on its shaft a 5 feet drum. Find 14 in column marked "Horse-Power." opposite this number in the table, in the column 5, marked "Diameter of Pulleys and Drums in feet." will be found 10 inches, which is the required width of belt.

REMARKS ON BELTING.

The average thickness of single belts is 3-16 of an inch, andwhen made of good ox-hide, well tanned, their breaking strength, per inch of width, has been determined as follows;

In the solid leather,
At the rivet holes of splices,
At the lacing holes,

675 lbs.
362 "
210 "

The safe working tension is assumed to be 45 lbs. per inch of width, which is equal to a velocity of about 60 square feet per minute per horse-power, which is safe practice for single belts in good condition.

About three-quarters of the trouble experienced in broken pulleys, hot boxes, etc., can be traced to the fault of tight belts.

The smooth side of the belt should run next to the pulley, as it will drive 25 per cent. more than if run with flesh side.

Belts that are dry and slip can be made to adhere more closely by putting on a little neats-foot or castor oil. The first is considered the best to use. Do not put rosm on the belts as it causes them to crack by making them hard.

Where narrow belts are to run over small pulleys. -15 feet is a good average—the belt having a sag of 11/2 to 2 inches.

For larger belts, working on larger pulleys. a distance of 20 to 25 feet, with a sag of $2\frac{1}{2}$ to 4 inches.

For main belts working on very large pulleys, the distance should be 25 to 30 feet, with a sag of 4 to 5 inches.

RULES for CALCULATING the SPEED of DRUMS and PULLEYS.

The diameter of the driver being given, to find its number of revolutions.

Rule:—Multiply the diameter of the driver by number of its revolutions, and divide the product by the diameter of the driven, the quotient will be the number of revolutions of the driven.

The diameter and revolutions of the driver being given, to find the diameter of the driven that shall make any given number of revolutions in the same time.

Rule:--Multiply the diameter of the driver by its number of revolutions and divide the product by the number of revolutions of the driven; the quotient will be its diameter.

To ascertain the size of the driver.

Rule:—Multiply the diameter of the driven by the number of revolutions you wish to make, and divide the product by the revolutions of the driver; the quotient will be the diameter of the driver.

N. B.—In ordering Pulleys, be careful to give the exact size of the Shaft on which they are to go, also state how you wish them finished on the face; Flat face for shifting belt, Rounding for non-shifting belt.

The following table shows the velocity of belts; the column marked "Revolution Shaft" shows the number of revolutions which the line or driven shaft is supposed to make per minute; the column marked "Diameter of Drum" shows the diameter of the drum on the line or driven shaft.

-											
olu- Shaft			1	Diamet	er of	Drum					
	2	21/2	3	31/2	4	41/2	5	51/2	6		
Rev tion		Number of Feet.									
100	628	785	942	1099	1256	1413	1570	1727	1884		
110	690	863	1036	1208	1381	1554	1727	1899	2072		
120	753	942	1130	1318	1507	1695	1884	2072	2260		
130	816	1020	1224	1428	1632	1836	2041	2245	2449		
140	879	1099	1318	1538	1758	1978	2138	2417	2637		
150	942	1177	1413	1648	1884	2119	2355	2590	2826		
160	1004	1256	1507	1758	2009	2260	2512	2763	3014		
170	1067	1334	1601	1868	2135	2402	2669	2935	3202		
180	1130	1413	1695	1978	2260	2543	2826	3108	3391		
190	1193	1491	1789	2088	2386	2684	2983	3281	3579		
200	1256	1570	1884	2198	2512	2826	3140	3454	3768		

Example 1.—The line shaft is required to make 120 turns per minute, and it is desired to have the belt run 1800 feet per minute; required, the diameter of the driven drum. Find 120 in the column marked "Revolution Shaft;" opposite to this number in the table find 1800 or the nearest to it, which is 1884 feet; over this number in the column marked "Diameter of Drum," will be found 5 feet, the diameter of the drum.

Example 2.—The line shaft makes 100 turns per minute, the diameter of the driven drum is 4 feet; required, the number of feet the belt moves a minute. Find 100 in the column marked "Revolution Shaft," opposite to the number in the table, and under 4 in the column marked "Diameter of Drnm," will be found 1256 feet.

The following table shows the width of the counter-belt that drives the counter-shaft, from which any number of

large size board-planing machines from one to four may be driven. The columns marked "Pulleys," shows the diameter of the smallest of the two pulleys on which the counter-belt runs; the columns marked "No. Machinea," shows the number of machines to be driven.

.s.		No. M	achine	es.	S.	No. Machines,			
ulleys.	1	2	3	4	ulleys.	1	2	3	4
P.	Width of Belt.				l P		Widtl	of B	elt.
12 14 16 18 20 22 24	$ \begin{array}{c c} 7_{\frac{1}{2}} \\ 6_{\frac{1}{2}} \\ 5_{\frac{1}{2}} \\ 5 \\ 4_{\frac{1}{2}} \\ 4 \\ 3_{\frac{3}{4}} \end{array} $	15 13 1114 10 9 84 712	22½ 19½ 16¾ 15 13½ 12¼ 11¼	$ \begin{vmatrix} 30 \\ 26 \\ 22\frac{1}{2} \\ 20 \\ 18 \\ 16\frac{1}{2} \\ 15 \end{vmatrix} $	26 28 30 32 34 36	314 3	$\begin{array}{ c c }\hline 7\\ 6\frac{1}{2}\\ 6\\ 5\frac{1}{2}\\ 5\frac{1}{4}\\ 5\end{array}$	$ \begin{vmatrix} 10\frac{1}{4} \\ 9\frac{1}{2} \\ 9 \\ 8\frac{1}{2} \\ 8 \\ 7\frac{1}{2} \end{vmatrix} $	$\begin{bmatrix} 13\frac{3}{4} \\ 12\frac{3}{4} \\ 12 \\ 11\frac{1}{4} \\ 10\frac{1}{3} \\ 10 \end{bmatrix}$

EXAMPLE—Required the width of a belt to drive two board-planing machines, the diameter of the smallest pulley being 20 inches. Find 20 in the column marked "Pulley," opposite to this number in the table, and under 2 in the column marked "No. Machines," will be found 9 inches, the required width of a counter-belt that drives a counter-shaft which drives two large size board-planing machines.

Table of Power Transmitted by Wire Ropes.

Diam		Diam	Rev	olutions	per Minu	ite.
Diam. of wh'el	No. of	At I	80	100	120	140
in feet.		Rope.		HORSE-	POWER.	- 7.
- 4	24	38 7	3.3	4.1	5.0	5.8
5	23		6.9	8.6	10.3	12.1
	23 22	15	10.7	13.4	16.1	18.7
67	22	15	16.9	21.1	25.3	29.6
8	21	1 1	22.0	27.5	33.0	38.5
8 9	20	5	40.0	41.5	50.0	51.9
10	19	11	55.0	58.4	73.0	82.5
11	18	11	64.9	75.5	81.0	97.3
12	17	3	93.4	99.3	116.7	124.1
13	17	3	112.0	140.0	168.0	
14	16	7	141.0	148.0	185.0	
15	16	65252 13131312581661664347878	217.0	259.0	300.0	40

WEIGHTS of MATERIALS.

TABLE Showing Standard Sizes of AMERICAN and ENGLISH WIRE GAUGES In Parts of an Inch.

a	Amer'n Gauge in Decimals.	Amer'n Gauge in Fracti'ns.	English Gauge in Decimals.	English Gauge in Fracti'ns.	of Se.	Amer'n Gauge in Decimals.	Amer'n Gauge in Fracti'ns.	English Gauge in Decimals.	Eng. Ga'g' in Fract.
No. of Gauge.	in Ser	9 8 3	Englis Gauge Jecima	Englis Gauge 'racti'ı	No. of Gauge.	Amer'n Gauge Jecimal	E gg G	E SE	E F
<u>0</u> 2	E 25 E	1888	15,32	F 2 2	No.	C E E	388	SES	Pic T
20	∀ರಿ	A P.E	H 2 9	HOT!	75	429 0	ACF	政のの	물.=
_	Inch	Inch	Inch	Inch	1	Inch	Inch	In.	In.
0000	.46	15-32	.454	15-32	18	.0403	-111011	.049	111.
000	.4096	13-32	.425	27-64	19	.0359	-	.042	3-64
00	.3648	23-61	.380	3-8	20	.0319	1-32	.035	0 01
Õ	.3248	21-64	.340	11-32	21	.0284		.032	1-32
1	.2893	19-61	.300	19-64	22 23	.0253	b	.028	
2	.2576	1-4	.284	9-32	23	.0225		.025	
2 3 4 5 6 7	.2294	15-61	.259	1-4	24 25	.0201		.022	
4	.2043	13-64	.238	15-16	25	.0179	1-64	.02	-
5	.1819	3-16	.220		$\frac{26}{27}$.016		.018	1-64
6	.1620	5-32	.203	13-64	27	.0142		.016	
7	.1443	9-61	.180	3-16	28	.0126		.014	
8	.1285	1-8	.165	5-32	29	.0112		.012	
9	.1144		.148	9-64	30 31	.012		.01	
10	.1019	7-64	.134	- 0	31	.01		.009	
11	.0907	3-32	.120	1-8	32	.0079		.008	
12	.0808	F C4	.109	7-64	33	.007		.007	
13	.0719	5-64	.095	3-32	34	.0063		.005	
14	.0641		.033	E C4	35	.0056		.004	
15	:057		.072	5-64	36	.005			
16 17	.0508	9 64	.058	1 16	37				
17	1.0404	3-64	1.000	1-16	11 30	1	l	1	1

Table showing the thickness and weight of Galvanized Sheet Iron by American gauge.

Wire Gauge.	Thick- ness.	Weight per Sq Foot.	Wire Gauge.	Thick- ness.	Weight per Sq Foot.
No.	Ins.	OZ.	No.	Ins.	OZ.
30	.012	10	22	.0253	21
_ 29	.0112	11	21	.0284	21 24
28	.0126	12	20	.0319	28
27	.0142	14	19	.0359	28 33 37
26 25	.016	15	18	.0403	37
25	.0179	16	17	.0452	43
24	.0201	17	16	.0508	43, 48' 60
23	.0225	19	14	.0641	60

Table showing weight of Lead Pipe required for a given head (or fall) of water.

in .	q.	Calibre in Inches.								
fee ad	r sq nch.	3/8	1/2	5/8	3/4	1	11/4	11/2		
He	Pr pe	4	Weight per foot in lbs.							
20	10	.38	.63	.87 1.38	1. 1.5	1.5	2.	3.5		
40	20	.68 .75	1.	1.75	2.	2.5	2.5	4.		
20 30 40 50 75	15 20 25 38	.75	1.25 1.63	2.38	3.38	3.	4. 5. 7.	5.		
100	50	1.25	2.	3.	4.0	5.		10.		
150 200	75 100	1.38 1.5	2.5 3.	3.5 4.	4.5 5.	6.	9. 12.	12. 15.		

The above weights of pipe are of sufficient strength to permit the water to be shut off, or stopped. When the water is permitted to run constantly, two-thirds of the above weight will answer.

LEAD PIPE. Weight per lineal foot. (AMERICAN).

- 0		Thickness in Inches.								
eule am	16	1/8	3	1/4	3/8	1/2	5/8	3/4		
Calcula- ted inside Diam.		Weight in Pounds.								
Ins.	.427	.97	1.65	2.44	4.38 5.11	7.70	-			
3/8 1/2 - 5/8 3/4 7/8	.548 .670 .791	1.21 1.46 1.70	2.01 2.38 2.74	2.93 3.42 3.90 4.39	5.85 6.58	7.79 8.77 9.75	12.2 13.4	17.6		
1	.911 1.03 1.28	1.95 2.19 2.69	3.11 3.47 4.21	4.39 4.88 5.85	7.31 8.04 9.5	10.7 11.7 13 7	14.6 15.8 18.3	19.1 20.5 23.4		
11/4 11/2 13/4 2 21/4 21/2 23/4 3 31/2	1.52 1.76 2.01	3.18 3.67 4.16	4.94 5.67 6.40	6.83 7.81 8.78	11. 12.4 13.9	15.6 17.6 19.5	20.7 23.2 25.6	26.3 29.3 32.2		
21/4 21/2	2.25 2.49	4.65 5.14	7.13 7.86	9.76 10.7	15.4 16.8	21.5 23.4	28.1 30.5	35.1 38.0		
23/4 3	2.73 2.98 3.46	5.63 6.12 7.10	8.59 9.32 10.8	11.7 12.7 14.6	18.3 19.7 22.7	25.4 27.3 31.3	32.9 35.4 40.3	41. 43.9 49.7		
4	3.95	8.08	12.2	16.6	25.6	35.2	45.2	55.6		

Joints to lead pipes require 1 lb. of solder for every inch diameter.

Weight of Lead Pipe. (ENGLISH.)

	7		Com- mon.	Med- ium.	Strong.
1/2 in. h	ore w'g'	t per 15 ft. length.	lbs.	lbs.	lbs.
/ 	66	"	15 18	18	22
5/8	44	"		$\frac{22}{32}$	47
34		"	24	32	42
1	66		42	56	64
114	6.	12	$\overline{42}$	52	64 63
11%	6.6	66	50	72	04
134	64	6.6			84
194	. 6	44	70	81	90
4		1	84	96	112

Weight and Dimensions of Leaden Balls. Number of balls in a pound from 15-16 ths to .237 of an inch in Diameter.

Diameter in Inches.	No.	Diameter in Inches.	No.	Diameter in Inches.	No.
1.67	1	.57	25	.301	170
1.326	1 2 3 4 5 6 7	.537	30	.295	180
1.157	3	.51	35	.29	190
1.051	4	.505	36	.285	200
.977	5	.488	40	.281	210
.919	6	.469	45	.276	220
.873	7	.453	50	.272	230
.835	8	.426	60	.268	240
.802	9	.407	70	.265	250
775	8 9 10	.395	75	.262	260
.75	ĪĬ	.388	80	.259	270
.73	$\overline{12}$.375	88	.256	280
.71	$\bar{1}\bar{3}$.372	90	.252	290
.693	14	.359	100	.249	300
.677	$\tilde{1}\tilde{5}$.348	110	.247	310
.662	16	.338	120	.244	320
.65	17	.329	130	242	330
.637	18	.321	140	.239	340
.625	19	.314	150	.237	350
.615	20	.307	160	.201	000

Thickness and weight per square foot of Window Glass.

No.	Thick- ness.	Weight.	No.	Thick- ness.	Weight.
12 13 15 16 17 19	Ins. .059 .063 .071 .077 .083	oz. 12 13 15 16 17 19	21 24 26 32 36 42	Ins. .1 .111 .125 .154 .167	21 24 26 32 36 42

Diameter and number of Pellets in an ounce of shot. (American Standard).

Num- ber.	Diam. in Inches.	Pel lets.	Num- ber.	Diam. in Inches.	Pel- lets.
TT	.21	32 38	5	.12	149
T	.20	38	6	.11	209
BBB	.19	44	1 7	.10	278
BB	.18	49	8	.09	209 278 375
. B	.19 .18 .17	49 58	9	.08	560
1	.16	69	10	.07	560 822
$\overline{2}$.15	82	11	.06	982
3	.14	98	11 12	.05	1778
4	.13	121			

Table Showing Weight per Foot of Sheet and Bar Brass.

Thickness, or Diameter, or Side, inches.	Square foot.	Square Bars, 1 foot long.	Round Bars, 1 foot long.	Thickness, or Diameter, or Side, inches.	Sheets, Square foot.	Square Bars, I foot long,	Round Bars, 1 foot long.
1-16	2.7	.015	.011	1-16	45.95	4.08	3.20
1/8 3-16	5.41	.055	.045	1/8	48.68	4.55	3.57
3-16	8.12	.125	.1	3-16	51.4	5.08	3.97
1/4	10.76	.225	.175	1/4 5-16	54.18	5.65	4.41
5-16	13.48	.350	.275	5-16	56.85	6.22	4.86
5-16 3/8 7-16	16.25	.51	.395	3/8 7-16	59.55	6.81	5.35
7-16	19.	.69	.54 .71	7-16	62.25	7.45	5.85
1/2 9-16	21.65	.905	.71	1/2	65.	8.13	6.37
9-16	24.3	1.15	.9	9-16	67.75	8.83	6.92
5/8 11-16	27.12	1.4	1.1	5/8 11-I6	70.35	9.55	7.48
11-16	29.77	1.72	1.35	11-16	73.	10.27	8.05
3/4	32.46	2.05	1.06	3/4	75.86	11.	8.65
13-16	35.18	2.4	1.85	13-16	78.55	11.82	9.29
7/8	37.85	2.75	2.15	7/8 15-16	81.25	12.68	9.95
15-16	40.55	3.15	2.48	15-16	84.	13.5	10.58
1	43.29	3.65	2.89	1	86.75	14.35	11.25

WEIGHT	of	ROUND	BOLT	COPPER,	PER F	оот.
 1	Vei	ght ner	foot	~.	Weig	rht ne

Diam.	in length.	Diam.	in length.
3/8 inch.	.424 lbs.	11/4 inch.	4.71 lbs.
1/2	755 ···	13/2 "	5.71 "
5/8 "	1.17 "	11/2 "	6.79 "
3/4 "	1.69 "	15/8 "	7.94 "
34 ··· 78 ···	2.31 "	134 "	9.21 "
1 "	3.02	17/8 ''	10.61 ''
11/2 "	3.82 "	2	12.08 "

Plate or Sheet Iron, Brass, Copper and Lead. Weight of a Superficial Foot in Pounds. (AVOIRDIPOIS)

/	of a Su	•	al Foo IRDUP	t in Po Dis).	unds.		•
-	Thickr	ess in	Parts	of an l	nch.		7
Inch.	16 18	16	1 5	3 1	76 1/2	5 3	1 1 7
Iron in lbs. 2 Brass " " 2 Cop'er" " 2	1.5 5. 1.7 5.5 1.9 5.8	7.5 10 8.2 10 8.7 11 11.1 14	0.9 13.6 1.6 14.5		$\begin{array}{c c} .5 & 20. \\ . & 21.8 \\ .3 & 23.2 \end{array}$	25. 34 27.1 32 28.9 34 37. 44	35. 37.9 .7 40.4 .4 57.8
Thickness by	the Bi	rmingl	nam w	ire-gau	ge, and	l in de	ci'als.
Wire Gauge.	0000.	000.	00.	0	1	2	3_
Thickness in decimals of an inch.	.454	.425	.380	.340	.300	.284	.259
Iron in lbs. Brass" " Copper "	18.99 21.11 21.61	17.78 19.76 20.53	15.89 17.67 18.37	14.22 15.81 16.43	12.5 13.75 14.5	12. 13.2 13.9	11. 12.1 12.75
Thickness by	the Bi	rmingl	nam w	ire-gau	ge, an	l in de	ci'als.
Wire Gauge.	1 4	5	6	7	8	9	10
Thickness in decimals of an inch.	.238	.220	.203	.180	.165	.148	.134
Iron in lbs. Brass" " Copper "	10. 11. 11.6	8.74 9.61 10.1	8.12 8.93 9.4	7.5 8.25 8.7	6.86 7.54 7.9	$\left \begin{array}{c} 6.24 \\ 6.86 \\ 7.2 \end{array} \right $	5.62 6.18 6.5
Thickness by	the Bi	rmingl	nam w	ire-gau	ge, an	d in de	eci'als
Wire Gauge.	11	12	13	14	15	16	17
Thick.in dec. of an inch.	.120	.109	.095	.083	.072	.065	.058
Iron in lbs. Brass. " Copper."	5. 5.5 5.8	4.38 4.81 5.08	3.75 4.12 4.34	3.12 3.43 3.6	2.82 3.1 3.27	$egin{array}{c} 2.5 \\ 2.75 \\ 2.9 \\ \end{array}$	$egin{array}{c} 2.18 \\ 2.4 \\ 2.52 \\ \end{array}$
Thickness by	the Bi	rming	ham w	ire-gau	ige, an	d in de	ci'als
Wire Gauge.	18	19	20	21	22	23	24
Thick. in dec. of an inch.	.049	.042	.035	.032	.028	.025	.022
Iron in lbs. Brass. " Copper. "	$\begin{vmatrix} 1.86 \\ 2.04 \\ 2.15 \end{vmatrix}$	1.7 1.87 1.97	1.54 1.69 1.78	$1.4 \\ 1.54 \\ 1.62$	1.25 1.37 1.45	1.12 1.23 1.3	1. 1.1 1.16

Cast-Iron Pipes, Hollow Columns, or Cylinders, Weight per lineal foot.

Diam.				Thic	kness	in Inc	hes.	-	
Bore.	1/4:	3/8	1/2	5/8	3/4	7/8	1	11/8	11/4
Ins.	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.
1	3.06	5.06	7.36		12.89	16.11	19.63		
11/4	3.68	5.98	8.59	11.51	14.73	18.25	22.09		
11/2	4.29	6.9	9.82	13.04	16.56	20.4	24.54		
13/4	4.91 5.53	7.83	11.05	14.57	18.41	22.5	27.		
2	5.53	8.75	12.25	16.11	20.25	24.7	29.45		
21/4	6.14		13.5	17.64	22.09	26.84	31.85		o.
21/2		10.58	14.72	19.17	23.92 25.71	28.93	34.36		
23/4	7.36	11.5	15.91	20.7	25.71	31.14	36.81	40	
3	7.98	12.43	17.18	22.19	27.62	33.29	39.25 41.72	45.56	52.2
31/4	8.59	13.34	18.35	23.78	29.45 31.3 33.13	35.44 37.58 39.73	41.72	48.32	55.22
31/2	9.2	14.21	19.64	25.31	31.3	37.58	44.18	51.08	58.29
334	9.76	15.19	20.86	26.85	33.13	39.73	46.63	53.84	61.36
4	10.44	10.11	22.1	28.38	34.98 36.87	41.88	49.	56.61	64.25
41/4	11.1	17.08	23.37	29.97 31.44 32.98 34.54	30.57	44.03	51.6	59.42	67.45
41/2	11.00	17.94	24.04	31.44	38.65	46.17	53.99	62.12	70.56
43/4	12.27	10.07	20.77	34.90	40.5	48.32	56.45	64.89	
5	12.00	19.70	27.	34.04	42.25	50.46	58.9	67.64	76.25
51/4	13.5	20.71	20.23	36.05	44.18	52.62	61.36	70.41	79.77
51/2	14.11	21.05	23.40	37.58 39.12	46.02 47.86	54.76	63.81	73.17	82.84 85.91
	14.70	22.00	91.00	10 CF	49.5	56.91	66.27 68.5	75.94 78.7	89.
6	17.70	23.47 27.15	96.0	40.65 46.79	56.84	59.06 67.65	78.5	90.74	101.25
6	90.09	30.83	41 7	52.92	64.42	76.23	00.05	100.78	101.20
7 8 9		34.52	46.5	59.07	71.5	84.84	99.5	111.84	196
10	25.16		51.5	65.2	79.16	93.42	100	122.87	190
11		41.88		71.33	86,5	102.01	117 5	133.92	150.9
12		45.55		77.46	93.6	110.6	197.95	144.96	
14	30.00	40.00	OI.	90.6	109.6	190.0	149 8	169 7	189.
16		-		30.0	124.5	129. 146.4	148.8 168.6	168.7 181.0	213.8
18					139.4	163.7	188.4	213.3	238.5
20			-		100.4	181.1	208.2	235.6	263.3
94					182.	101.1	247.9	280.2	312.9
24 28		-			213.		286.	200.2	360.
30					227.		305.		384.
34					257.		345.		443.

Weight of Cast-Iron, Brass, Copper and Lead Balls from 1 inch to 12 inches in diameter.

								Cop- per. Le'd
Ins. 1 11/2 2	15s. .136 .46 1.09	fbs. .158 .537 1.25	15s. .166 .56 1.3	1bs. .214 .727 1.7	Ins. 7 71/2 8	1bs. 47.76 57.52 69.81	1bs. 54.5 67.11 81.4	1bs. lbs. 57.1 73.7 70.0 90. 85.2 110.1

(TABLE CONTINUED).

Diam. Cast-	Br'ss. Cop- I	e'd Diam	Cast- Iron. B	\mathbf{r} 'ss. $\begin{vmatrix} \mathbf{C} 0 \\ \mathbf{p} \mathbf{c} \end{vmatrix}$	p- Le'd
Ins. lbs. 21/2 2.13 3.68 31/4 5.84 4 8.72 41/2 12.42 5 17.04 51/2 22.68 61/2 37.44	$ \begin{array}{c cccc} 2.50 & 2.60 \\ 4.3 & 4.5 \\ 6.82 & 7.14 \\ 10.2 & 10.7 & 1 \\ 14.5 & 15.25 & 1 \\ \end{array} $	6.9 11 6.0 111/2 6.4 12	83.73 1 99.4 1 116.9 1 136.35 1 157.84 1 181.48 2 207.37 2	115.9 12 136.4 14 159.0 16 184.0 19 211.8 22 242.0 25	s. lbs. 2.3 132.3 1.3 156.7 3.0 184.7 66.4 215.0 3.0 250.0 1.8 286.7 3.5 327.7 8.1 372.3

Weight of Parallel Angle Iron of equal sides, and Parallel T Iron, equal depth and width.

Parallel Angle Iron. Parallel T Iron. Uniform |W'g't of 1||Width of |Uniform |W'g't of 1 Length thickn'ss lineal ft. top table thickn'ss lineal ft. of sides Through- in lbs and and total through- in lbs and in Ins. out. dec. parts depth. out. dec. parts Ins. Ins. Ins. Ins. 3 8.0 1/2 7-16 18.25 13.75 7.0 5 5.75 4 3/2 9.7521/4 2 23/4 31/2 3/8 4.5 8.5 full 3.75 3 3/8 7.5 3.0 21/2 21/4 5-16 4.63 2.5 5-16 4.5 No. 6 w.g. 1.75 5-16 3.75 114 1.5 13/4 3.0 1/4 1.25 11/8 9 1/4 2.25 $11/_{2}$ 10 1.0 114 1.75 .875 3-16 10 1 1.0 1/8 3/4 11 .625 7/2 .73 $.5\overline{63}$ 1/8 11 34 .63 $1\overline{2}$ 1/2 .5

Table Showing Number of Rivets in One Hundred Pounds.

Len- gth in	Dian	neter iı	n Inch	ies.	Len- gth in	Diameter in Inches.			
Ins.	1/2	1 5/8	11	3/4	Ins.	1/2	5/8	116	3/4
34 78 1 11/8 11/4 13/8 11/2 15/8	1092 1027 940 840 797 760 730 711	665 597 538 512 487 460 440 420	450 415 389 370 357 340	356 329 280 271	31/4 31/2 33/4 4 41/4 41/2 43/4 5	433 413 395	267 248 241 230 220 210 200 190	212 201 192 184 177 171 166 161	180 169 160 158 150 146 138 135

Table Showing No. of	Rivets in 100 Pounds.	(CONTINUED).

Len-	Diai	neter i	n Inc	hes.	Len- gth in	Diameter in Inches.			
Ins.	1/2	1 5/8	116	3/4	Ins.	1/2	5/8	11	3/4
13/4	693	390	325	262	51/4		180	156	130
17/8	648	375	312	257	51/2		172	151	124
2	608	360	297	243	$53\overline{4}$		164	145	120
21/8	573	354	289	237	6		157	140	115
21/4	555	347	280	232	61/4	-	150	138	111
21/2	525	335	260	220	61/2		146	134	107
23/4	500	312	242	208	634		143	129	104
3	460	290	224	197	7		140	125	100

Weights of Taper Angle Iron, of equal Sides, and Taper T Iron.

Tap	er An equa	igle II I Side	ron, of es.	Taper T Iron.					
Length of sides in Ins.	Thickness of Edges.	Thickness of Root.	W'g't of 1 lin- eal ft. in lbs. & dec. parts.	Width of top table in lns.	Total depth in inches.	Thickness of top table at edges.	Uniform thickness of rib.	Thickness of top table at root.	W'g'tof 1 lineal ft. in lbs.
Ins. 4 3 23/4 21/2 21/4 2 13/4 11/2*	1/2 1/2 7-16 3/8 5-16‡ 1/4 1/4	5-16‡ 5-16 5-16*	14.0 10.37 8.25 6.5 5. 5.87 3.25 2.62	Ins 3 2 21/2 2 2 2	Ins 31/4 25/8 3 21/2 11/2 11/2	Ins 3/8 3/8 5-16	Ins 7-16 1/2 5-16 1/2‡ 3/8 1/4	Ins 1/2 7-16 7-16 5/8 5/8‡ 5-16	8.0 8.0 5.25 6.5 3.5 2.87
		* Be	re.				† Ful	77	

ire. ‡ Fui

Number of Nails in a Pound.

Title.	Size.	No.	per lb		Title.	Siz	e.	No.per	lb.
2 penny fine.	111/8 I	n. 760	nails.	116	pen. f	31/2	In	(32 nail	S.
3 "	11/4	" 480	66	20		4	4.6	24 "	~•
4 "	11/2	. 300	66	30		41/9	66	18 "	
5 "	134	" 200	66	40		5	.1	14 "	
6, "	2	" 160	66	50		51/2	66	12 "	
7 "	21/4	" 128	66	60		16	66	10 "	
8 "	21/2	" 92	66	6	fence	2	64	80 "	
9 "	234	" 72	66	18	6.	21/9	66	50 "	
10	3	" 60	66	10	66	3	-6%	34 "	
12 "	314	. 41	**	12		314	66	29 "	

Number of Tacks in a Pound.

Title.	Length.	No. per lb.	0	Title.	Length.	No. per lb.
1 oz.	1/2 In.	16,000	11	10 oz.	11-16	1.600
11/2	3-16	10.666	Н	12	3/4	1.333
2'4	1/4	8.000		14	13-16	1.143
21/2	1/4 5-16	6.400	Ш	16	7/8	1.000
3'- i	3/8	5.333	li .	18	7/8 15-16	.888
4	7-16	4.000		20	1	.800
6	9-16	2.666		22	1 1-16	.727
8	5/8	2.000		$\overline{24}$	1 1/8	.666

Table Showing Weight of 100 feet of Iron, Steel, Copper and Brass Wire. (English and American Gauges).

Wire per 100	rican Eng. gauge		American Gauge.					irmir	ighar	n Gai	ige.
Ins Ibs. Ibs. Ibs. Ibs. Ins Ibs. Ib	meric nd En	ick's Dec.)	Dec Dec				
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	NoaA	Eri	I	S.	. C.	B.	Fi	I.	S.	C.	B.
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	3000										
00											
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	000		44.46	44.88	00.79	47.99		47.80			
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	00			35.59	40.28	38.06					
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$.34	30.03			
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1							23.80			
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	2					18.98	284	21.37			
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	3				10.93		. 259		17.94	20.03	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	4	.204		11.10	14.00	11.95	. 238	10.01	10.10		
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	9	181	6.77	0.00	10.02	9.40	.22	12.82	12.90	14.65	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	9	.102	0.90	7.02	6.90	1.00	203	10.92		12.47	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	6	100	0.01	0.00	4.00	0.90	10	0.00	0.00	9.00	9.40
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	Ö		9.46	9.50	9.00	9.74	. 100	7.21	1.20	6.24	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	10		3.40	3.90	3.90	3.74	.148	0.80	9.89	0.03	0.20
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	10		2.75	2.77	3.14	2.90	. 134	4.75	4.80	5.43	5.13
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	11		2.18	4.20	2.49	2.50	.12	3.81	5.80	4.50	4.11
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	12	.080	1.75	1.74	1.97	1.80		3.15	3.18	3.59	3.39
17 .043 .54 .54 .54 .58 .058 .68 .89 .90 1.08 .96 18 .040 .43 .43 .49 .46 .049 .63 .64 .72 .68 19 .035 .34 .34 .38 .36 .042 .46 .47 .53 .51 20 .031 .27 .27 .30 .29 .035 .32 .33 .37 .35 21 .028 .21 .21 .24 .23 .032 .27 .27 .31 .29 22 .025 .17 .17 .19 .18 .028 .20 .21 .23 .22 23 .022 .13 .13 .15 .14 .025 .16 .16 .19 .18 24 .020 .10 .10 .12 .11 .022 .12 .13 .15 .14	13		1.37	1.38	1.56	1.48	.095	2.39	2.41	2.73	2.58
17 .043 .54 .54 .54 .58 .058 .68 .89 .90 1.08 .96 18 .040 .43 .43 .49 .46 .049 .63 .64 .72 .68 19 .035 .34 .34 .38 .36 .042 .46 .47 .53 .51 20 .031 .27 .27 .30 .29 .035 .32 .33 .37 .35 21 .028 .21 .21 .24 .23 .032 .27 .27 .31 .29 22 .025 .17 .17 .19 .18 .028 .20 .21 .23 .22 23 .022 .13 .13 .15 .14 .025 .16 .16 .19 .18 24 .020 .10 .10 .12 .11 .022 .12 .13 .15 .14			1.08	1.09	1.21	1.17		1.82	1.84	2.08	1.96
17 .043 .54 .54 .54 .58 .058 .68 .89 .90 1.08 .96 18 .040 .43 .43 .49 .46 .049 .63 .64 .72 .68 19 .035 .34 .34 .38 .36 .042 .46 .47 .53 .51 20 .031 .27 .27 .30 .29 .035 .32 .33 .37 .35 21 .028 .21 .21 .24 .23 .032 .27 .27 .31 .29 22 .025 .17 .17 .19 .18 .028 .20 .21 .23 .22 23 .022 .13 .13 .15 .14 .025 .16 .16 .19 .18 24 .020 .10 .10 .12 .11 .022 .12 .13 .15 .14	15				.98	.93		1.37	1.38	1.57	1.48
17 .043 .54 .54 .54 .58 .058 .68 .89 .90 1.08 .96 18 .040 .43 .43 .49 .46 .049 .63 .64 .72 .68 19 .035 .34 .34 .38 .36 .042 .46 .47 .53 .51 20 .031 .27 .27 .30 .29 .035 .32 .33 .37 .35 21 .028 .21 .21 .24 .23 .032 .27 .27 .31 .29 22 .025 .17 .17 .19 .18 .028 .20 .21 .23 .22 23 .022 .13 .13 .15 .14 .025 .16 .16 .19 .18 24 .020 .10 .10 .12 .11 .022 .12 .13 .15 .14	16			.69	.78	.75	.065	1.12	1.13	1.28	1.21
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	17		.54	.54	.61	.58		.89	.90	1.08	.96
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$.43	.43	.49	.46		.63		.72	.68
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	19		.34	.34	.38	.36		.46	.47	.53	.51
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	20	.031	.27	.27	.30	.29		.32	.33	.37	.35
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	21		.21	.21	.24	.23		.27	.27	.31	.29
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	22		.17	.17	.19	.18		.20	.21	.23	.22
25 .017 .08 .08 .09 .09 .02 .10 .10 .12 .11	23		.13	.13	.15	.14		.16			.18
	24		.10	, 10				.12			.14
26 [.015] .06[.06] .07[.07[].018[.08[.08] .09[.09											
25 11525 1 1001 1001 1011 1011110201 1001 1101 1101	26	.015	.06	.06	.07	.07	1.018	.08	.08	.09	.09

Table Showing Weight of Wrought Iron, Steel, Copper and Brass. (American and English Gauges).

rican Eng. gauge	, A	meri	can (auge		В	irmir	ighan	n Gar	ige.
ಕ್ಷಕ್ಷ	ick's Dec.	Plates per Sq. foot.		nick's Dec.	Plat	es pe	r Sq.	fooot		
An No.	Thi	I.	S.	C.	B.	EE	Ι.	S.	C.	В.
	Ins	lbs.	lbs.	lbs.	lbs.	Ins	lbs.	lbs.		lbs.
0000	.46	18.45	18.70	20.83	19.68		18.21	18.45	20.56	
000	.409	16.43	16.65	18.55	17.53		17.05			
00	.364	14.63				1.38		15.45		16.26
0	.324	13.03	13.20			.34			15.40	
- 1	.289	11.60	11.76	13.10	12.38	.3	12.03		13.59	
234 567 89	.257	10.33	10.47		11.02	.284	11.39	11.54	12.86	12.15
3	.229	9.20	9.32	10.39	9.81	.259	10.39	10.53	11.73	
4	.204	8.19	8.30	9.25	8.74	.238	9.54	9.67	10.78	10.18
5	.181	7.30	7.39	8.24	7.78	1.22	8.82	8.94	9.96	9.41
6	.162	6.50	6.58	7.33	6.93	.203	8.14	8.25	9.19	8.68
7	.144	5.78	5.86			1.18	7.22	7.31	8.15	7.70
8	.128	5.15		5.82			6.62	6.70		7.06
9	.114	4.59	4.65	5.18					6.70	
10	.101	4.08	4.14		4.36		5.37	5.44		
11	.090	3.64		4.11	3.88	.12	4.81	4.87		
12	.080	3.24	3.28	3.66			4.37	4.83		
13	.071	2.88		3.25	3.07	.095	3.81	3.86	4.30	4.06
14	.064	2.57	2.60	2.90			3.33	3.37	3.75	3.55
15	.057	2.28	2.32	2.58	2.44	072	2.88	2.92		
16	.050	2.03			2.17	.065		2.64		2.78
17	.045	1.81	1.84	2.05	1.93	.058	2.32	2.35	2.62	
18	.040	1.61	1.63		1.72	.049				2.09
19	.035	1.44			1.53	.042		1.70		1.79
20	1.031	1.28	1.29			.035				
21	.028	1.14		1.28	1.21	.032	1.28	1.30	1.44	1.36
21 22	.025	1.01		1.14			1.12	1.13		1.19
23	.022	.90	.91	1.02			1.00			1.07
24	.020	.80	.81	.91			.88	.89		
25	.017	.71	.81 .72	.81	.76		.80	.81	.90	
26	.015	.63	.64	.72						
	1.010	1 .00	1 .01	1	1 .00	11.010		,	1 .01	

Weight of a lineal foot of Square and Round Malleable Bar Iron from 1-4 inch to 12 inches in diameter. (AVOIRDUPOIS POUNDS).

Size Inches. Sq.Rolled bar Iron Round ""	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	6 3/4 7 1.87 3 1.47
Size Inches. Sq. Rolled Iron. Round " "	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	4 1 1 5 0 5.74 9 4.51

Square and Round Malleable Bar Iron. (Continued).

		1			
Size Ins. Sq.R.I.bar Round "	$\begin{array}{c c} 1_{16}^{3} & 1_{16}^{7} \\ 6.30 & 6.88 \\ 4.95 & 5.40 \end{array}$	7.50 8.15	8.80 9.50	$ \begin{vmatrix} 134 & 1\frac{1}{8} & 1\\ 10.20 & 10.69 & 11\\ 8.01 & 8.60 & 9 \end{vmatrix} $.75
· Do	$\begin{array}{ c c c c c }\hline 1\frac{1}{1}\frac{5}{6} & 2 \\ 12.52 & 13.33\end{array}$	21/8 21/4 15.05 16.87	23/8 21/2 18.80 20.80	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	7/8 .55
Do	$ \begin{vmatrix} 3 & 31/8 \\ 30. & 32.55 \\ 23.56 & 25.56 \end{vmatrix} $	$egin{array}{c c} 31/4 & 33/8 \\ 35.20 & 37.96 \\ 27.65 & 29.82 \\ \end{array}$	$\begin{vmatrix} 31/2 & 35/6 \\ 40.80 & 43.80 \\ 32.07 & 34.40 \end{vmatrix}$	33/4 37/8 46.87 50.05 53 36.81 39.31 41	4 3.33 .81
Do	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$egin{array}{c c} 45\% & 43/4 \\ 71.30 & 75.20 \\ 56. & 59.06 \\ \hline \end{array}$	$egin{array}{c c c c} 47/8 & 5 & 5 \\ 79.21 & 83.33 & 93 \\ 62.21 & 65.45 & 73 \\ \hline \end{array}$	1.4
Do	$\begin{vmatrix} 51/2 & 53/4 \\ 102.2 & 111.8 \\ 80.3 & 87.8 \end{vmatrix}$	$ \begin{vmatrix} 6 & 61/4 \\ 127. & 132.0 \\ 95.6 & 103.6 \end{vmatrix} $	$egin{array}{c c c} 61/2 & 63/4 \\ 142.8 & 154.0 \\ 112.2 & 121.0 \\ \end{array}$	$egin{array}{c c c c c c c c c c c c c c c c c c c $	$0.1 \\ 9.3$
Ъо	$\begin{smallmatrix} 8 & 81/2 \\ 216.3 & 244.2 \\ 169.9 & 191.8 \end{smallmatrix}$	$\begin{array}{c c} 9 & 91/2 \\ 273.8 & 305.1 \\ 215.0 & 239.6 \end{array}$	$egin{array}{c c c} 10 & 101/2 \\ 337.9 & 372.7 \\ 266.3 & 292.7 \\ \hline \end{array}$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	2 6.7 2.2

Weight of 9 feet length, of flanged Cast-Iron Pipes of various diameters.

s of Bore.	Thickn'ss of Metal.	Diameter of Flange	Thickn'ss of flange.	Diameter of Cir.thr- o'gh hole'	Diam. of Holes.	No. of Holes	Weight.
Ins. 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18	Ins. 388224444444444444444444444444444444444	Ins. 61/2 71/2 91/2 101/2 12 14 15 161/2 19 20 21 22 251/2 261/2 28 29	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	Ins. 434 6 734 834 10 1134 1234 1414 1512 1634 1934 2034 223 24 25	Ins. 55844444444444444444444444444444444444	444446666666688888888888888888888888888	$\begin{array}{c} \text{Cwt-qr-ID} \\ 0-3-0 \\ 1-0-3 \\ 1-0-3 \\ 1-3-5 \\ 2-1-12 \\ 2-2-1 \\ 4-3-17 \\ 5-2-9 \\ 6-1-12 \\ 7-0-0 \\ 8-3-24 \\ 9-3-5 \\ 10-2-0 \\ 11-0-26 \\ 12-0-25 \\ 12-3-8 \\ 13-2-17 \\ 16-1-15 \\ 17-2-13 \\ 18-0-26 \\ \end{array}$

TABLE SHOWING WEIGHT OF I FOOT OF SEAMLESS
DRAWN BRASS AND COPPER TUBING.

Outside	Length	Brown & Sharpe's	Weight	per Ft.
Diameter.	Feet.	Gauge.	Brass.	Copper.
38 1/2 58 34 13-16 78 15-16 1 11/4 13-16 1 13-16 1 13-16 1 12-16 22/8 21/2 25/8 21/2 25/8 21/2 25/8 21/2 25/8 21/2 25/8 21/2 25/8 21/2 25/8 21/2 25/8 21/2 25/8 25/8 25/8 25/8 25/8 25/8 25/8 25	12 12 12 12 12 12 12 12 12 12 12 12 12 1	No. 17 16 16 15 15 15 15 15 14 14 13 121/2 12 111/2 11 11 & 10	18455. 175. 177. 125 .338 .422 .477 .528 .666 .855 .98 1.200 1.355 1.750 1.822 1.95 2.05 2.36 3.67 3.75 3.92 4.50 6.75	108

WEIGHT OF A SQUARE FOOT OF CAST AND WROUGHT IRON, COPPER, LEAD, BRASS AND ZING.

From I-16 to 2 inches in Thickness.

Thick- ness.	Cast- Iron.	Wr'g't Iron.	Copper.	Lead.	Brass.	Zinc.
Ins.	lbs,	lbs.	lbs.	lbs.	lbs	lbs.
1-16	2.346	2.517	2.89	3.691	2.675	2.34
1/8	4.693	5.035	5.781	7.382	5.35	4.68
3-16	7.039	7.552	8.672	11.074	8.025	7.02
1/4	9.386	10.07	11.562	14.765	10.7	9.36

WEIGHT OF A SQUARE FOOT OF CAST AND WROUGHT IRON, COPPER, LEAD, BRASS AND ZINC. (TABLE CONTINUED).

Thick- ness.	Cast- Iron.	Wr'g't Iron.	Copper.	Lead.	Brass.	Zinc.
Ins.	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.
5-16	11.733	12.588	14.453	18.456	13.375	11.07
3/8	14.079	15.106	17.344	22.148	16.05	14.04
7-16	16.426	17.623	20.234	25.839	18.725	16.34
1/2	18.773	20.141	23.125	29.53	21.4	18.72
9-16	21.119	22.659	26.016	33.222	24.075	
5/8	23.466	25.176	28.906	36.913	26.75	
11-16	25.812	27.694	31.797	40.604	29.425	
3/4	28.159	30.211	34.688	44.296	32.1	
13-16	30.505	32.729	37.578	47.987	-	
7/8	32.852	35.247	40.469	51.678		
15-16	35.199	37.764	43.359	55.37		
1	37.545	40.282	46.250	59.061		
11/8	42.238	45.317	52.031			
11/4	46.931	50.352	57.813			
13/8	51.625	55.387	63.594		i	
11/2	56.317	60.422	69.375			-
1½ 15%	61.011	65.458	75.156			
134	65.704	70.493	80.938			
17/8	70.397	75.528	86.719			
2	75.090	80.563	92,500			

Weight of a lineal foot of Flat Rolled Iron from 1-4 inch to 15-16 inch thick by 1 inch to 3 inches wide.

f d	Thickness in Inches.
W'd'h of Iron.	14 18 38 16 1/2 18 58 18 34 18 78 18
lbs. 1 11/8 11/4 13/8 11/2 15/4 13/4	$\begin{array}{c} bs. bs. bs. lbs. lbs$
21/8 21/4 23/8 21/8 23/4 23/4 23/4 23/8	$\begin{array}{l} 1.66[2.08]2.50[2.91] [3.33] 3.75[4.16]4.58[5.5] 5.41[5.83]6.25\\ 1.77[2.21] 2.65[3.09] 2.54[3.98]4.42[4.86]5.31]5.75[6.19]6.64\\ 1.87[2.34]2.81[3.28]3.75[4.21]4.68[5.15]5.62[6.09]6.56[7.03]\\ 1.97[2.47]2.96[3.46]3.95[4.45]4.94[5.44]5.93[6.43]6.92[7.42]\\ 2.08[2.60]3.12[3.64]4.16[4.68]5.20[5.72]6.25[6.77]7.29[7.81]\\ 2.18[2.73]3.28[3.82]4.37[4.92]5.46[6.01]6.56[7.10]7.65[8.20]\\ 2.29[2.86]3.43[4.01]4.58[5.15]5.72[6.30[6.87]7.44[8.02]8.59[2.39]2.99[3.59]4.19[4.79]5.39[5.98]6.58[7.18]7.78[3.88]8.98\\ 2.50[3.14]3.75[4.37]5.\\ [5.62]6.25[6.87]7.50[8.12]8.75[9.37]\\ \end{array}$

To ascertain the Weights of larger sizes take the half size of that required, and double it. Thus, required the weight of $4\times1/2$ in. refer to $2\times1/2$ in.=3.33 \times 2=6.66 lbs.

Table showing the weight of water in pipes of various diameters, one foot in length.

Diam.	Weight	Diam.	Weight	Diam.	Weight	Diam.	Weight,	Diam.	Weight
in Ins.	in lbs.	in Ins.	in lbs.	in Ins.	in lbs.	in Ins.	in lbs.	in Ins.	in lbs.
3 3 4 4 4 4 4 5 5 5 5 6 6 6 6 7 7 7 7 8 8 14	3 1 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	812874 9 914-12874 10 1014 11 11 11 11 11 11 11 11 11 11 11 11 11	2412 26 27244 3024 3242 34144 445 447 49 51344 45 5744 5744 6244 6244	14 144 144 15 154 154 164 164 17 17 17 17 18 18 18 18 18 19 19	6634 6914141414141414141414141414141414141414	$ \begin{array}{c} 19\frac{1}{2}\\ 19\frac{3}{4}\\ 20\\ 20\frac{1}{2}\\ 21\\ 21\frac{1}{2}\\ 22\\ 22\frac{1}{2}\\ 23\\ 23\frac{1}{2}\\ 24\\ 24\frac{1}{2}\\ 25\\ 26\frac{1}{2}\\ 26\frac{1}{2}\\ 27\frac{1}{2}\\ 28\\ 28\frac{1}{2}\\ 29\frac{1}{2}\\ 29\frac{1}{2$	129½ 132 136¼ 143¼ 150¼ 157½ 165 172½ 180¼ 188¼ 143½ 213½ 220½ 230½ 230½ 248½ 2576¼ 276½ 276½ 276½ 286½ 296½ 296½ 296½ 296½ 296½ 296½ 296½ 29	$ \begin{vmatrix} 30 \\ 301^{\frac{1}{2}} \\ 311^{\frac{1}{2}} \\ 321^{\frac{1}{2}} \\ 331^{\frac{1}{2}} \\ 341^{\frac{1}{2}} \\ 341^{\frac{1}{2}} \\ 351^{\frac{1}{2}} \\ 361^{\frac{1}{2}} \\ 371^{\frac{1}{2}} \\ 381^{\frac{1}{2}} \\ 391^{\frac{1}{2}} \\ 40 \end{vmatrix} $	3063 3174 3274 3384 349 360 371 429 441 451 441 450 505 441 505 515 545 545 545 545 545 545 545 545 54

TABLE SHOWING the WEIGHT of WATER at DIFFERENT TEMPERATURES.

Temp Farh.	W'g't of a Cubic foot.	Temp. Farh.	W'g't of a Cubic foot.	Temp. Farh.	W'g't of a Cubic foot.	Temp. Farh.	W'g't of a Cubic foot.
40°	62.408	102°	61.092	172°	60.72	275°	58.17
-42	62.406	112	61.078	182	60.55	300	57.42
52	62.377	122	61.063	192	60.28	350	55.94
62	62.321	132	61.047	202	60.05	400	54.34
72	62.025	142	61.030	212	59.82	450	52.70
82	62.015	152	61.011	230	59.37	500	51.02
92	62.004	162	60.920	250	58.85	600	47.64

The boiling point of water decreases one degree (on an average) for every 530 feet above sea level. The boiling point at sea level being 212 degrees.

$\begin{array}{c} DIMENSIONS\ OF\ BOLT\ AND\ NUTS\ SQUARE\\ AND\ HEXAGONAL. \end{array}$

meter Bolt.	of.	of ut.	of Nut	of d.		VOLU	JME.	
Diameter of Bolt.	Depth Nut.	Width of Sq. Nut.	Diam Hex'l	Width of Head.	Hexa'l Nut.	Square Nut.	Hexa'l Head.	Bolt per inch of Length.
Ins.	Ins	Ins	Ins.	Ins.	Cu. Ins.	Cu. Ins.	Cu.Ins.	Cu.Ins.
1/8 3-16	.15	.2	1/4	.2	.00425		.0045	.01227
3-16	.2	.3	3/8	.3	.01276		.0152	.02761
1/4 5-16	.25	.45 .55	3/8/2/3/4/5/3/4/5/8/7/8	.4	.02836		.036	.04908
5-16	.35	.55	5/3	.5	.06235	.07903	.07	.07669
3/8 7-1 6	.4	.6	3/4	.6	.10209	.09984	.1215	.1104
7-16	.5	.75	7/8	.7	.17368	.2061	.1929	.1503
1/2 9-16	.55	.85	1	.75	.25584	.28941	2531	.1963
9-16	.6	.95	11/8	.85	.34449	.3924	.3658	.2485
5/8 11-16	.7	1.1	11/4	.95	.49625	.6323	.5076	.3067
11-16	.75	1.2	13/8	1.05	.64328	.8016	.6822	.3712
3/4 13-16	.8	1.3	$1\frac{1}{2}$	1.125	.81664	.9986	.8543	.4417 .5184
13-16	.9	1.4	15/8	1.25	1.0782	1.2977	1.143	.5184
7/8 1	.95	1.5	13/4	1.35	1.3199	1.5663	1.435	.6013
1	1.1	1.75	2	1.5	1.996	2.5048	2.025	.7854
11/8 11/4	1.25	1.95	$\bar{2}\frac{1}{4}$	1.7	2.8701	3.5106	2.926	.994
11/4		2.15	21/2	1.875	2.8846	4.6518	3.955	1.227
19/8	1.5	2.4	$2\frac{1}{4}$	2.1	5.1474	6.414	5.457	1.484
13/8 11/2 15/8	1.65	2.6	3	2.25	6.737	8.2384	6.834	1.767
19/8	1.8	2.8	31/4	2.45	8.6267	10.381	8.778	2.073
134	$\frac{1.9}{2.05}$	3.	$\frac{31}{2}$	2.625	10.559	12.53	10.853	2.405
17/8	2.05	3.25	33/4	2.8	13.058	15.993	13.23	2.761
2	2.2	3.45	4	3	15.97	19.275	16.2	3.141

MARKS and weight of English Tin-Plates.

Brand.	Plates per Box.	Length and Breadth.	Net W'g't per Box.
	No.	Inches.	lbs.
1C or 1 com	225	1334 by 10	112
2C	66	1314 " 934	105
3C	66	1234 " 91/2	98
HC	6.6	1334 " 10	119
HX	6.6	1334 " 10	157
1X	44	1334 " 10	140
1X 2X	- 44	1314 " 934	133
$3\tilde{X}$	46	1234 " 91/2	126
1XX	16	1334 " 1074	161
1XXX	44	1334 " 10	182
1XXXX	44	1334 " 10	203
1XXXXX	44	1334 " 10	224
1XXXXXX	44	1334 " 10	245
DC	100	1634 " 121/9	98
DX	100	1634 " 121/2	126

MARKS and weight of ENGLISH Tin-Plates. (Continued).

Brand.	Plates per Box.	Length and Breadth.	Net W'g't per Box.
	No.	Inches.	lbs.
DXX	100	163/4 " 121/9	147
DXXX	~ "	163/4 " 121/2	168
DXXXX	66	1634 " 121/2	189
SDC	200	15 " 11"	168
SDX	-11	15 " 11	188
SDXX	. 66	15 " 11	209
SDXXX	66	15 " 11	230
SDXXXX	- 66	15 " 11	251
SDXXXXX	66	15 "11	272
SDXXXXXX	44	15 " 11	293
Leaded IC	112	20 - 14	112
" IX	112	20 " 14	140
ICW IX	225	1334 " 10	112
IXW	225	1334 " 10	140
CSDW			
	200	15 " 11	168
CIIW	100	1094 1242	105
XIIW	100	1094 1442	126
TT	450	1004 10	112
XTT -	450	133/4 " 10	126

Note:—When the plates are 14 by 20 inches there are 112 in a box.

Table of Standard Dimensions of Wrought Iron Welded Tubes.

- 4				****	ucu	i uoco.			
Nominal Diameter.	External Diameter.	Thickness.	Internal Diameter.	Internal Circum.	External Circum.	Length of pipes per sq. foot.of Int'al and Extern'l sufaces.	Internal area.	Wei	No. of threads per inch of Screw.
Ins.	Ins.	Ins	Ins.	Ins.		Feet Feet	Ins.	Ibs.	
1/8	.40	.068	.27	.85	1.27	14.15 9.44	.057 .104	.24	27
1/4	.54	.088	.36	1.14	1.7	10.5 7.075	.104	.42	18
1/8 1/4 3/8 1/2 3/4	.67	.091	.36 .49 .62 .82 1.05	1.55	2.12	7.67 5.657	.192 .305 .533 .863	1bs. .24 .42 .56 .84 1.13	18
1/2	.84 1.05	.109	.62	1.96 2.59 3.29	2.65	6.13 4.502	.305	.84	14
3/4	1.05	.113	.82	2.59	3.3	4.64 3.637	.533	1.13	14
1	1.31	.134	1.05	3.29	4.13	3.66 2.903	.863	1.67	$111/_{2}$
11/4	1.66	.14	1.38	4.33	5.21	2.77 2.301	1.496	2.26	111/2
11/2	1.9	.145	1.61	4.33 5.06	5.97	2.37 2.10	2.038	2.69	111/2
2	2.37	.154	2.07	6.49	7.46	1.85 1.611	3.355	3.67 5.77	14 111/ ₂ 111/ ₂ 111/ ₂ 111/ ₂ 8
21/2	2.87	.204	2.47	7.75	9.03		4.783	5.77	8
11/ ₂ 11/ ₂ 2 21/ ₂ 3	3.5	.217	3.07	9.64	11.	1.24 1.091	7.388	7.55	8

(TABLE CONTINUED).

Nominal Diameter.	External Diameter.	Thickness.	Internal Diameter.	Internal Circum.	External Circum.	In'l.	x and Exter'al surfaces.	Internal area.	Weight per ft.	No. of threads per inch of Screw.
Ins. 31/2	Ins. 4.	Ins .226	Ins.	Ins. 11.15	Ins.	Feet	Feet 0.995	Ins. 9.887	fbs. 9.05	Q
4		.237	4.07	12.69	14.14	.95	0.849	12.73	10.73	888888888
41/ ₂ 5 6 7 8 9	5.	.247	4.51	14.15	15.71	.85	0.765	15.939	12.49	8
5	5.56	.259	5.01	15.85	17.47	.78	0.629	19.99	14.56	8
6	6.62	.28	6.06	19.05	20.81	.63	0.577	28.889	18.77	8
7	7.62	.301	7.02	22.00	23.95	.54	0.505	38.737	23.41	8
- 8	8.62	.322	7.98	25.08	27.1	.48	0.444	50.039	28.35	8
-9	9.69	.344	9.	28.28	30.43	.42	0.394	63.633	34.08	8
10	10.75	.366	10.02	31.47	33.77	.38	0.355	78.838	40.64	8

Tables of the different quantities of Coal-gas of the Specific gravity .420, delivered in one hour, from horizontal pipes of different diameters and lengths, and under different pressure.

Quantities delivered by a 2 inch main in Cubic feet.

- V			3						
ngth pip's yds.		sure in i and parts		Perpendicular Head of water.					
E F	0.50	0.75	1.00	1.50	2.00	3.00			
10	2896	3558	4135	4923	5792	6950			
īš l	2364	2904	3331	4080	4728	5768			
. 20	2047	2507	- 2886	3541	4094	4994			
20 25	1830	2241	2580	3165	3660	4465			
30	1673	2049	2368	2894	3346	4082			
40	1445	1770	2037	2490	2890	3525			
50	1294	1585	1824	2238	2588	3157			
100	915	1121	1290	1582	1830	2232			
150	748	916	1054 -	1304	1496	1825			
200	647	792	912	1119	1294	1578			
250	579	709	816	1010	1158	1412			
300	522	639	736	903	1044	1273			
400	457	559	644	790	914	1115			
500	409	500	576	707	818	997			

Rule:—The discharge of the same gas through different openings and under the same pressure are proportional to the areas of the orifices in circular inches or to the square of their diameters,

QUANTITIES DELIVERED BY A 6 INCH MAIN IN CUBIC FEET.

Length of pipe		sure in i and part		Perpendicular Head of water.					
in yds.	0.50	0.75	1.00	1.50	2.00	3.00			
100	8240	10095	11657	14276	16484	20190			
150	6730	8242	9517	11657	13460	16484			
200	5828	7138	8242	10095	11657	14276			
300	4759	5828	6730	8242	9517	11657			
400	3929	4813	. 5557	6806	7858	9626			
- 500	3686	4515	5213	6384	7372	9030			
600	3365	4121	4759	5828	6730	8242			
700	3115	3816	4406	5396	6230	7632			
- 800	2778	3403	3929	4813	5557	6807			
900	2747	3365	3886	4759	5494	6730			
1000	2606	3192	3686	4515	5213	6384			
1760	1965	2406	2778	3403	3929	4813			
2640	1604	1965	2269	2778	3208	3929			
3520	1389	1702	1965	2406	2778	3403			
5280	1134	1389	1604	1965	2269	2778			
7040	982	1149	1389	1702	1965	2298			
8800	879	1076	1287	1521	1758	2152			
10000	824	1010	1166	1428	1648	- 2019			

For a 12 inch main multiply by 4 " "24 " "16 " "16 " divide " 4

Diameter and length of gas-pipe to transmit given volumes of gas to branch.

Diam- eter.	Length.	Volume per hour.	Diam- eter.	Length.	Volume per hour.
Ins .4 1. 1.97 2.65 3.16 3.87	Feet. 100 200 600 1000 1000 1000	50 250 500 700 1000 1500	Ins. 5.32 6.33 7. 7.75 9.21 10.95	Feet. 2000 4000 6000 1000 2000 1000	2000 2000 2000 2000 6000 6000 8000

The pressure with which gas is forced through pipes should seldom exceed 2½ inches of water at the Works, or the leakage will exceed the advantages to be obtained from increased pressure.

When pipes are laid at an inclination either above or below the horizon, a correction will have to be made in estimating the supply, by adding or deducting $\frac{1}{100}$ of an inch from the initial pressure for every foot of rise or fall in the length of the pipe.

Size of pipe required to furnish gas from the main from 2 lamps to 30.

Number	Length	Diam.	Number	Length	Diam.
of	from	of	of	from	of
Lamps.	Main.	Pipe.	Lamps.	Main.	Pipe.
2 3 4 6 10	Feet. 40 30 40 50 100	Ins. 3/8 3/8 1/2 5/8 3/4	15 20 25 30	Feet. 130 150 180 200	Ins. 1 11/4 13/4 11/2

Regulation of the diameter and Extreme length of Tubing and number of burners permitted.

Diameter of Tubing.	Length.	Number of Burners	Capacity of Meters.	Number of Burners
Ins. 14 38 158 34 1 11/2 2	Feet. 6 20 30 40 50 70 100 150 200	1 3 6 12 20 35 60 100 200	Light. 3 5 10 20 30 45 60 100	6 10 20 40 60 90 120 200

HOW TO TELL THE STATE OF THE METER.

Each figure or division, on the different dials of the Index, indicates as follows: On the right hand dial, 100, 200, 300 cubic feet, &c.; on the middle dial, 1,000, 2,000. 3,000, &c.; on the left hand dial, 10,000, 20,000, 80,000, &c.



Look at the left hand dial, and set down the figure at the least value next the pointer, which, on the above diagram, is 1. Next look at the middle dial. As before, set down the least figure next the pointer, which, in the diagram, is 3. Next, look at the right hand dial. Take whichever figure is nearest, which, in the diagram is 5. Set all these figures down, thus: 135, and add two ciphers, to represent hundreds, and you have 13,500, which is the present state of the meter. If a previous observation has been taken, subtract the state of the meter at that observation from the present state, and the difference is the amount consumed in interval.

STRENGTH of MATERIALS.

A Table of the depths of square beams or bars of Cast-Iron, calculated to support from 1 cwt to 14 tons in the middle, the Deflexion not to exceed 1-40 of an inch for each foot in length.

is it	14.1				1	r.E.I	VGT	T	IN	FFF	ידי			
Weight in cwts.	Weigh in Ibs.	41	6	81	10			16	18	20	22	24 T	26	28
Wein	We	-1	-	0 1			TE		NIN				20 1	
1	112	1 6	1.4	1 71				2.4				2.0	3.0	3.1
2	224	1.2 1.4	1.4 1.7 1.9 2.0 2.2 2.3 2.4 2.5 2.6 2.7 2.8 2.8	20	2.2	2. 4	2.6	2.8	2.5 3.0	2.6 3.1	2.7 3.3	2.9	3.6	3.7
2 3 4 5 6 7	336	1.6	1.9	2.2	2.4	$\frac{7}{2}$. $\frac{1}{7}$	2.9	3.1	3.3	3.4	3.6	3.8	3.9	4.1
4	448	1.7 1.8	2.0	2.4	2.6	2. 9	$\frac{3.1}{3.3}$	3.3	3.5 3.7	3.7	3.9	4.0	4.2	4.3
5	560	1.8	2.2	2.5	2.8	3.0	3.3	3.5	3.7	3.9	4.1	4.3	4.4	4.6
6	672	1.8	2.2	2.6	2.9	3. 2	3.4 3.6 3.7 3.8 3.9	3.7	3.9	4.1	4.3	4.5	4.6	4.8
8	784 896	1.9 2.0	2.3	2.7	3.0	3. 3	3.6	3.8	4.1	4.2 4.4	4.4	4.6	4.8	5.0
9	1.008	2.0	2.4	2.0	0.1	0.4 9.5	3.6	1.0	4.2 4.3	4.4	4.6	4.8 4.9	5.0 5.1	5.2 5.3
10	1 100	2.1	2.6	3.0	3.2	3. 6	3 9	4 2	4.4	4.7	4.9	5.2	5.3	5.4
11	1.232	2.1	2.6	3.0	3.4	3. 7	4.0	4.3	4.5	4.8	5.0	5.3	5.4	5.6
12	1.344	2.2	2.7	3.1	3.5	3.8	4.1	4.4	4.7	4.9	5.1	5.3	5.5	5.6 5.7
13	1.456	2.2	2.7	3.1	3.5	3. 8	4.2	4.4	4.7	4.9	5.2	5.4	5.6	5.9
14	1.568	2.3	2.8	3.2	3.6	3. 9	4.2	4.5	4.8	5.0	5.3	5.5	5.7	6.0
15	1.000	2.3	2.8	3.2	3.0	4. 0	4.3	4.0	4.9 5.0	5.2 5.2	5.4	5.6 5.7	5.8 5.9	6.1
16 17	1 904	2.4	2.9	3 4	3.8	4 1	4 4	4 7	5.0	5.3	5.5 5.5	5.8	6.0	6.2
18	2.016	2.4	3.0	3.4	3.8	4. 2	4.5	4.8	5.1	5.4	5.6	5.9	6.1	6.4
19 1 T	2.128	2.5	3.0	3.5	3.9	4. 2	4.6	4.9	5.2	5.4	5.7	6.0	6.2	6.5
1T	2.240	2.5	3.0	3.5	3.9	4, 3	4.6	4.9	5.2 5.5	5.5	5.8	6.0	6.3	6.5
11/4 11/2	2.800	2.6	3.2	3.7	4.1	4. 5	4.9	5.2	5.5	5.8	6.1	6.4	6.6	6.9
11/2	3.360	2.8	3.4	3.9	4.3	4.7	1.6	5.5	5.8	6.1	6.4 6.7	6.7	7.0	7.2
13/4 2	4.480	2.9	3.5	4.0	4.0	4. U	5.5	5.7	6.2	6.3 6.5	6.8	$\frac{6.9}{7.2}$	7.2 7.6	7.5
21/2	5.600	3.1	3.8	4 4	4.9	5.5	5.8	6.2	6.6	6.9	7.3	7.6	7.9	8.2
374	6.720	3.3	4.0	4.6	5.1	5.7	6.1	6.5	6.9	7.3	7.6	7.9	8.3	8.6
31/2	7.840	3.4	4.1	4.8	5.3	5.8	6.3	6.7	7.1	7.5	7.9	8.2	8.6	8.9
4	8.960	3.5	4.3	4.9	5.5	6.0	6.5	7.0	-7.4	7.8	8.2	8.5	8.9	9,2
41/2	10.080		4.4	5.1	5.7	6.2	6.7	7.2	7.6	8.0	8.4		9.1	9.5
5	1.230 1.344 1.456 1.568 1.792 1.904 2.016 2.128 2.240 2.360 3.920 4.480 5.600 6.720 7.840 8.960 10.080 11.200 11.3440 15.680		4.0	5.5	6.0	6.7	7.9	7.4	7.8	8.2 8.6	8.6 9.0	9.0 9.4	9.4	$9.7 \\ 10.2$
7	15.680			57	6.3	6.9	7.5	80	8.5	8.9	9.4	9.4	10.2	
6 7 8	17.920))		15.9	6.6	7.2	7.8	8.3	8.2 8.5 8.8	9.3	9.7	10.1		
9	20.160)		6.0	6.8	7.4	8.0	8.5	9.0	9.3 9.5	10.0	10.4	10.9	11.3
10	22.400				6.9	7.6	6.9 7.2 7.5 7.8 8.0 8.2 8.4	8.8	9.3 9.5 9.7	9.8	10.3	10.7	11.2	11.6
11	24.640				7.1	7.8	8.4	9.0	9.5	10.0	10.5	11.0	11.5	11.9
12 13	26.880 29.120				16.4	1.0	0.0	3.4	9.1	10.2	10.8	11.2	11.7	
14	31.360				7.4	8.1	8.0	9.4	9.9 10.1	10.4	11.0	11.5	11.9	12.4 12.6
	lexion	1	1	1)	1		10.1	10.0	11.1	11.1	14.1	1
	nches.	.1	.15	.2	.25	.3	.35	.4	.45	.5	.55	.6	.65	.7
441 1	1101106.	1	1	1		5	1	t	1	1				

TABLE (Continued).

is pt	s.				Le	engtl	h in	Feet				
elght tons.	eight 1 Ibs.	10	12	114	16	18	20	22	24	26	28	30
N.H	₩ü	-			De	pth	in I	nche	s.			
15	133600	7.7	8.4	9.1				3 11.4				13.2
16	35840	7.8	8.5	9.2	9.8	10.4	11.0	11.5	12.0	12.5	13.0	13.5
17	38080	7.9	8.7	9.4	10.0	10.6	11.2	2 11.7 3 11.9	12.2	12.7	13.2	13.7
18 19	40320 42560	8.0 8.1	8.8	9.0	110.1	10.0	11.6	12.2	12.4	12.9	12.4	14.1
20	44800	0.1	9.0	9.7	10.3	11 0	11 6	12.5	12.7	13 2	13.8	14 2
22	49280			10.0	10.7	11.3	111.9	12.8	13.0	13.6	14.1	14.6
$\tilde{24}$	53760		9.4	10.2	10.9	11.5	12.2	12.8 13.0	13.4	13.9	14.4	14.9
26	58240		9.6	10.4	11.1	11.8	12.4	1 13.3	13.6	14.2	14.7	15.2
28	62720		9.8	10.6	11.4	12.0	12.7	113.5	13.9	14.4	15.0	15.5
Defle	exion	.25	.3	.35	.4	.45	.5	.55	1.6	.65	.7	.75
in I	nches.	.40	1.0	.55	1.2	1.10	.0	.00	1.0	.00		1.10
Len	gth in		1	4.0		100	101		20	00	00	04
	eet.	14	16	18	20	22	24	26	28	30	32	34
30	67200	10.8	11.5	12.2	12.9	13.5	14.1	14.7		15.7		
32	71680			12.4	13.1	13.7	14.3	14.9	15.5	16.0	16.5	17.0
34	76160		11.9	12.6	13.3	15.9	14.5	15.1	15.7	16.2	16.8	17.3
36	80640 85120			12.8	13.4	14.1	14.7	15.3	10.9	16.5	17.0	17.0
38 40	89600	11.4		19.0	19.0	14.5	15.1	$15.5 \\ 15.7$	16.1	16.0	$\frac{17.2}{17.5}$	18.0
42	94080		12.5	18 8	14.0	14.7	15.1	15.9	16.5	17 1		18.2
44	98560		12.7	13.5	14.2	14.9	15.5	16.1	16.8	17.4	17.9	18.5
46	103040		12.8	13.6	14.3	15.0	15.7	16.3	17.0	17.6		18.7
48	107520		13.0					16.5				
50	112000							16.6				
52	116480			14.0	14.7	15.5	16.2	16.8	17.5	18.1	18.7	19.2
54	120960					15.7	16.3	17.0	17.6	18.2	18.8	19.4
56	125440					15.8	10.0	17.1	17.8	10.4	19.0	19.6
58 60	$129920 \\ 134400$							$17.3 \\ 17.4$				
-				17.0	10.0	120.0	10.1	11.1	10.1	10.1	10.0	10.0
	lexion nehes.	35	.4	.45	.5	.55	.6	.65	.7	.75	.8	.85

Examples illustrative of the Table:—1 To find the depth of a rectangular bar of cast-iron to support a weight of 10 tons in the middle of its length the deflexion not to exceed 1-40 of an inch per foot in length, and its length 20 feet, also let the depth be six times the breadth.

Opposite six times the weight an under 20 ft. in length is 15.3 inches, the depth, and 1-6 of 15.3=2.6 inches, the breadth.

(2). To find the diameter for cast-iron shaft or solid cylinder that will bear a given pressure the flexure in the

middle not to exceed 1-40 of an inch for each foot of its length, the distance of the bearing being 20 ft. and on the

middle equals 10 tons.

Constant multiplier 1.7 for round shafts, then $10\times1.7 = 17$. and opposite 17 tons and under 20 ft. is 11.2 inches for the diameter. But half that flexure is quite enough for revolving shafts; hence $17\times2=34$ tons, and opposite 34 tons is 13.3 inches for the diameter.

Tensile Strength of Metals. Weight necessary to tear asunder one square inch.

Name of Materials.	In pounds Avoirdupois.	In Tons of 2,000 lbs.
Antimony Cast.	1.060	0.5
Bismuth "	3.250	1.6
Brass, fine yellow cast.	17.968	8.9
" Wire.	49.000	24.5
Copper Cast.	19.000	9.5
Sheets.	30.000	15 0
" Bolts.	33.000	16.5
" Wire.	60.000	30.0
Gun metal.	36.000	18.0
Lead Cast.	1.824	0.9
" Sheet.	3.300	1.6
Steel	111.500	57.5
Tin Cast.	4.600	2.3
Platinum.	56.000	28.0
Silver.	40.000	20.0
Gold Cast.	20.000	10.0
" Wire.	30.000	15.0
Zinc.	7.500	3.5
Cast-Iron.	20.834	10.4
Wrought-Iron.	56,000	28.0
Cast Steel.	88.600	44.3

RELATIVE POWER of METAL to RESIST TORISON, WROUGHT-IRON BEING UNITY.

Wrought-Iron	1		- (-		-		-		-		_		_		1.
Cast-Iron		-		-		-		9		-		-		-		-		-	.90
Cast-Steel	=		-		-		-		-		-		-		-		-		1.93
Gun Metal		-		-		-		-		-		-		-		~		-	.27
Brass -	-		-		-		-		-		-		-		-		-		.23
Copper -		-		-		-		-		-		-		-		-		-	.22
Tin	-		-		-		-		-		-		-		-		-		.13
Lead		-				-		-		-		-		-		-		-	.10

HANDY MECHANICAL,

Strength of White Pine Struts or Pillars. (Moderately Seasoned).

th.				of Cros			inches	
Length in feet.	4×5	4 ×6		4×8			4×11	4×12
그림	l			oad in '				
6	4.1	5.0	5.8	6.6	7.4 6.8 6.3	8.3	9.1	9.9
7	3.8 3.5	4.5	5.3 4.9	6.0 5.6	6.3	7.5 7.0	8.3	9.0 8.4
8 9 10	3.2	3.9	4.6	5.2 4.6	5.9 5.2	6.5	7.2	7.8
10	2.9	3.5	4.0	4.6	5.2	5.8	6.3	6.9
11 12	2.6	3.2	3.7	4.2 3.8 3.2 2.8 2.2	4.7 4.3 3.6	5.3	5.8	6.3
13	$\frac{2.4}{2.0}$	2.9 2.4	2.8	3.2	3.6	4.0	5.2 4.4	5.7 4.8
14 15	1.8	2.1	2.8 2.5	2.8	3.2 2.5 2.0	3.5	3.9	4.2
15	1.4	1.7	1.9	2.2	2.5	2.8	3.0	3.3
16 17	1.1	1.4	1.6 1.4	1.8 1.6	2.0 1.8	2.3	2.5 2.2	2.7
18	0.9	1.2	1.2	1.4	1.6	1.8	1.9	2.4 2.1
	5×5		5×7	5×8	5×9	5×10	5×11	5×12
8	5.0	6.0	7.0	8.0	9.0	10.0	11.0	12.0
9	4.7	5.6	6.6	7.5 7.0	8.5 7.9	9.4 8.8	10.3	11.3
10	4.4	5.3 4.9	6.2 5.7	6.6	7.9	8.8	9.7 9.0	10.6 9.8
11 12 13	4.1 3.8	4.6	5.3	6.1	7.4 6.8	8.2 7.6	8.4	9.1
13	3.5	4.2 3.8	4.9 4.5	5.6	6.4	7.0	7.7	8.4
14 15	3.2 2.9	3.8 3.5	4.5	5.1 4.6	5.8 5.2	6.4 5.8	7.0 6.4	7.7
16	2.6	3.1	3.6	4.2	4.7	5.2	5.7	6.2
16 17	2.3	2.8	3.2	3.7	4.1 3.8	4.6	5.1	5.5
18 19	2.1	2.5	2.9	3.4	3.8	4.2	4.6	5.0
20	1.8 1.5	2.2 1.8	2.5 2.1	2.9 2.4	3.2 2.7	3.6	3.2	4.3 3.6
20		1.6×6		6×8	6×9	6×10		6×12
10	6.9	7.1	8.3	9.5	10.7	11.8	13.0	14.2
11	5.6	6.7	7.8	8.9	10.0	11.2	12.3	13 4
12 13	5.3	6.3	7.4	8.4	9.5	10.5	11.5	12.6
13	5 0 4.7	5.9 5.6	6.9 6.5	7.9 7.5	8.8 8.4	9.8 9.3	10.8 10.3	11.8 11.2
14 15	4.4	5.3	6.2	7.1	7.9	8.8	9.7	10.6
16 17	4.1	4.9	6.2 5.7	6.5	7.3	8.2	9.0	9.8
17	3.8	4.5	4.3	5.9	6.8	7.5	8.3	9.0
18 19	3.5 3.2	4.2 3.8	4.9	5.6 5.1	6.3 5.7	7.0 6.4	7.7	8.4 7.6
20	3.0	3.5	4.1	4.7	5.2	5.8	6.4	7.0
21	2.6	3.1	3.6	4.1	4.7	5.2	5.7	6.2
22	2.3	2.8	3.3	3.7	4.2	4.7	5.2	5.6

Strength of White Pine Struts or Pillars. (Continued).

(Moderately Seasoned).

Length in feet.	7×5	1 70			s-Secti			
		7×6	7×7	7×8	7×9	7×10	7×11	7×12
i e i				ad in T		f 2000 I	bs.	
10	8.7	9.2	10.8	12.3	13.9	15.4	16.9	18.4
11 12	7.2 6.8	8.6	10.1 9.5	11.5 10.9	13.0 12.2	14.4	15.8	17.2
13	6.5	7.7	9.0	10.9	11.6	13.6 13.0	15.0 14.2	16.0 15.4
14	6.2	7.4	8.6	9.8	11.1	12.4	13.5	14.8
15	5.9	7.0	8.2	9.4	10.5	11.8	12.9	14.0
16	5.6	6.7	7.8	8.9	10.0	11.2	12.2	13.4
17 18	5.3	6.4	7.4	8.5 8.0	9.5 9.0	10.6 10.0	11.7 11.0	12.8 12.0
19	4.7	5.6	6.6	7.5	8.5	9.4	10.3	11.2
20	4.4	5.2	6.1	7.0	7.8	8.8	9.6	10.4
21	4.1	4.9	5.7	6.5	7.3	8.2	. 8.9	9.8
22	3.8	4.6	5.3	6.1	6.8	7.6	8.4	9.2
	8×5	8×6	8×7	8×8	8×9	8×10		0712
10	9.6	11.5	13.4	15.3	17.2	19.2	21.0	23.0
11 12	9.0 8.5	10.8 10.2	12.6 11.9	14.4 13.6	16.2 15.3	18.0 17.0	19.8 18.7	$21.6 \\ 20.4$
13	8.1	9.7	11.3	12.9	14.5	16.2	17.7	19.4
14	7.7	9.2	10.8	12.3	13.9	15.4	16.9	18.4
15	7.3	8.8	10.2	11.7	13.1	14.6	16.1	17.6
16	7.0	8.4	9.8	11.2	12.6	14.0	15.4	16.8
17 18	6.7	8.0 7.7	9.4 9.0	10.7 10.2	12.1 11.5	13.4 12.8	14.7 14.1	16.0 15.4
19	6.1	7.4	8.5	9.7	10.9	12.2	13.3	14.8
20	5.8	7.0	8.1	9.3	10.4	11.6	12.8	14.0
21 22	5.5	6.6	7.7	8.8	9.9	11.0	12.1	13.2
22	5.3	6.3	7.4	8.4	9.5	10.6	11.6	12.6
	9×5	9×6	9×7	9×8	9×9	9×10		
10	11.9	14.3	16.7	19.2	21.5	23.8	26.3	28.6
11	11.0	13.1 12.4	15.3	17.6 16.4	19.7	$\frac{22.0}{20.6}$	24.1 22.7	26.2 24.8
12 13	10.3 9.8	11.7	14.4 13.7	15.6	18.5 17.5	19.6	21.5	23.4
14	9.3	11.3	13.0	14.8	16.7	18.6	20.5	22.6
15	8.9	10.7	12.5	14.2	16.0	17.8	19.6	21.4
16	8,5	10.2	11.9	13.6	15.3	17.0	18.7	20.4
17	8.2	9.8	11.4	13.0	14.7	16.4	17.9	19.8
18	7.9 7.6	9.5 9.1	11.1 10.7	12.6 12.0	14.2 13.7	15.8 15.2	17.4 16.7	19.0 18.2
20	7.3	8.7	10.7	11.6	13.1	14.6	16.0	19.4
21	7.0	8.4	9.8	11.2	12.6	14.0	15.4	17.8
22	6.8	8.1	9.5	10.8	12.1	13.6	14.9	16.2

HANDY MECHANICAL,

Strength of White Pine Struts or Pillars. (Continued). (Moderately Seasoned).

t.b	I	Dimensi	ons of (cross-Se	ctions i	n inches	3.
ng Gee	10×6	10×7	10×8	10×9	10×10	10×11	10×12
Length in feet.		Sa	fe load	in Tons	of 2000	lbs.	
10	17.5	20.4	23.4	26.3	29.2	32.1	35.0
11	16.2	18.9	21.6	24.3	27.0	29.7	32.4
12	15.1	17.6	20.0	22.6	25.1	27.6	32.2
13	14.2	16.6	19.0	21.3	23.7	26.1	28.4
14	13.5	15.8	18.0	20.3	22.5	24.8	27.0
15	12.9	15.1	17.2	19.4	21.5	23.7	25.8
16	12.3	14.4	16.4	18.5	20.5	22.6	24.6
17	11.8	13.7	15.6	17.6	19.6	21.6	23.6
18	11.3	13.1	15.2	17.0	18.9	20.8	22.6
19	10.9	12.7	14.6	. 16.4	18.2	20.0	21.8
20	10.5	12.2	14.0	15.8	17.5	19.3	21.0
21	10.0	11.7	13.4	15.0	16.7	18.4	20.0
22	9.6	11.2	12.8	14.4	16.0	17.6	19.2
	11×6	11×7	11×8	11×9	11×10	11×11	11×12
12	18.0	21.0	24.0	27.0	30.0	33.0	36.0
13	16.9	19.7	22.6	25.4	28.2	31.0	33.8
14	16.0	18.7	21.0	24.0	26.8	29.4	32.0
15	15.4	17.9	20.4	23.0	25.6	28.1	30.8
16	14.7	17.2	19.6	22.0	24.6	26.9	29.4
17	14.2	16.5	18.8	21.2	23.6	25.9	28.4
18	13.5	15.8	18.0	20.3	22.6	24.9	27.0
19	13.0	15.2	17.4	19.5	21.8	23.9	26.0
20	12.5	14.6	16.8	18.8	21.0	23.0	25.0
21	12.0	14.0	16.0	18.0	20.0	22.0	24.0
22	11.6	13.5	15.4	17.4	19.4	21.2	23.2
$\frac{23}{24}$	11.2	13.0	14.8	16.7	18.6	20.5	22.4
24	10.8	12.6	14.4	$\frac{16.2}{12 \times 9}$	$ 18.0 $ $ 12 \times 10$	19.8 12×11	$\frac{21.6}{12 \times 12}$
10	12×6						
12	21.0	24.5	28.0	31.5	35.0	38.5	42.0 39.7
13	19.9	23.2 21.9	26.4 25.0	29.8 28.1	33.2 31.4	36.4 34.4	37.6
14 15	18.8		23.8	26.1	29.8	32.8	35.8
16	17.9	20.9 20.0	22.8	25.7	28.6	31.4	34.2
17	17.1 16.4	19.1	21.8	24.6	27.4	30.0	32.7
18	15.7	18.3	21.0	23.6	26.2	28.8	31.4
19	15.1	17.6	20.2	22.7	25.2	27.7	30.2
20	14.6	17.0	19.4	21.9	24.4	26.7	29.2
21	14.0	16.5	18.8	21.9	23.6	25.8	28.2
22	13.6	15.9	18.2	20.5	22.8	25.0	27.2
23	13.0	15.3	17.4	19.6	21.8	24.0	26.2
$\frac{25}{24}$	12.6	14.7	16.8	18.9	21.0	23.1	25.2
44	1 14.0	14.7	10.0	10.5	41.0	20.1	40.4

The strength of pillars, as well as of beams of timber, depend much on their degree of seasoning.

Well seasoned timber will stand 1½ to 2 times the weight that green timber will. In the same class of timber the slower the growth or the narrower the annular rings the better. In the same class the heavier the better. If the wood has color, deepness of color indicates strength and durability. The freshly-cut surface of wood should be firm, shining, and somewhat translucent. A dull, chalky appearance is a sign of bad timber. In resinous timber, those with least resin in their pores are strongest and most durable. In non-resinous timber, those with least sap or gum are best.

Weight that can be borne with safety by Cast-Iron Columns in 1000 lbs. (Trenton Iron Co).

American Iron.

Length			Diam	eter in 1	Inches.		
Feet.	2	3	4	5	6	7	8
5 6 7 8 9 10 12 14 16 18 20	12.4 9.4 7.2	36 30 24 20 18	102 88 76 66 56 48 38 28	184 164 146 130 114 102 80 64 52 44	288 264 242 218 198 180 136 122 100 84 72	414 386 360 332 306 282 238 200 170 144 124	560 532 502 470 440 410 354 304 262 226 196
Length	11		Diame	eter in	Inches.		
Feet.	9	10	11	12	13	14	15
5 6 7 8 9 10 12 14 16 18 20	728 698 660 630 596 560 494 432 378 332 292	916 884 850 812 774 739 658 586 520 462 410	1126 1082 1056 1016 974 932 846 774 686 616 552	1354 1320 1282 1240 1196 1152 1056 966 878 796 720	1570 1530 1486 1440 1392 1292 1192 1094 1000 912	1798 1754 1706 1656 1550 1440 1332 1228 1130	2086 2040 1992 1940 1828 1712 1596 1482 1372

SAFE LOAD for HCLLOW CAST-IRON PILLARS. (Tons 2240 lbs).

Thickness of Metal=1/2 Inc	h.
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	1 IIICK	ness of me	- 142 III	511.	
External Diam.		LENG	TH IN FI	EET.	
in Ins.	8	10	12	1 14	16
3 31/2 4 41/2 5 51/2 6	Tons. 4.0 5.9 8.1 10.6 13.3 15.3 19.0	Tons. -3.2 5.1 6.1 8.1 10.4 12.9 15.5	Tons. 2.3 3.6 4.7 6.5 8.3 10.5 12.7	Tons. 1.8 2.7 3.6 5.0 6.7 8.5 9.5	Tons. 1.4 2.3 3.4 4.4 5.4 7.0 8.7
<u> </u>		ness of Met		·	1 0.1
3 31/2 4 41/2 5 51/2 6 61/2 7	4.7 7.1 9.2 12.8 16.1 18.7 23.2 26.9 30.7	3.5 5.3 7.3 9.9 12.7 15.7 19.0 22.4 26.0	2.6 4.2 5.6 7.7 9.1 12.8 15.6 18.7 21.9	2.0 3.2 4.4 6.1 8.1 10.4 12.8 15.2 18.5	1.6 2.5 3.9 5.5 7.0 8.8 10.6 13.0 15.6
	Thic	kness of M	etal=3/4 In	ich.	
3 31/2 4 41/2 5 51/2 6 61/2 7	5.4 8.1 11.3 14.9 18.8 21.8 27.2 31.6 36.1	3.8 6.2 8.5 11.5 14.8 18.4 22.3 26.3 30.6	2.8 4.4 6.5 8.9 11.7 14.9 18.3 21.9 25.8	2.2 3.5 4.8 7.2 9.0 12.1 15.0 17.8 21.7	1,7 2.6 3.8 6.0 7.7 10.2 12.5 15.3 18.4
	Thi	ckness of 1	Ietal=1 In	ch.	-
4 41/2 5 51/2 6 61/2 7 71/2 8	13.9 18.5 23.6 27.6 34.5 40.3 46.2 52.2 58.3 70.5	10.4 14.3 18.6 23.2 28.3 33.6 39.1 44.9 50.7 62.7	8.0 11.1 14.8 18.9 23.2 28.0 33.0 38.3 43.8 55.3	6.4 8.8 11.9 15.3 19.1 22.8 27.8 32.6 37.7 48.1	4.8 7.1 9.6 12.7 15.9 19.6 23.6 27.9 32.5 42.3

STRENGTH OF ROLLED IRON BEAMS.

Depth	Size of	- 7	Spans in	feet.	
of Beam	Flange	10	15	20	25
Inches.	Inches.	Brea	king Weig	ght in To	ns.
5	2 by 1/2	6.6	1		
6	21/2" 1/2	10.	6.6	5	1
7	3 "1/2	14.	9.	7	5
8	3 "38	20.	13.	10	8
9	4 " 34	36.	24.	18	14
10	41/2" 1	60.	40.	30	24

Table to show the Weight or Pressure a column of Cast-Iron will sustain with Safety in Cwts. (112 lbs). (English Iron).

Diam.					Heig	ht in	feet				
Inches.	4	6	8	10	12	14	16	18	20	22	24
2	72		49						15	13	11
21/ ₂	119	105	91	77	65	55		40	34	29	25
3	178				111	97	84	73	64	56	49
31/2	247	232	214	191	172	156		119	106	94	83
4	326	310		266	242	220		179	160	144	130
41/2	418	400		354	327	301	275	251	229	208	189
	522	501	479	452	427	394	365	337	310	285	262
6	607	592	573	550	525	497	469	440	413	386	360
5 6 7	1032	1013	989	959	924	887	848	808	765	725	686
8	1333	1315	1289	1259	1224	1185	1142	1097	1052	1005	959
9	1716	1697	1672	1640	1603	1561	1515	1467	1416	1364	1311
10	2119	2100	2077	2045	2007	1964	1916	1865	1811	1755	1697
11								2305			
12								2780			

If the columns are hollow, the area to the given diameter is to be converted into the ring, or the difference of the outer and inner diameters multiplied by \%3, because hollow Cast-Iron, columns are stronger than solid ones in that proportion.

RELATIVE STIFFNESS OF MATERIALS TO RESIST A TRANSVERSE STRAIN.

Cast-Iron	1.	lOak'	.095
Ash	089	White Pine	1
AshBeech	073	Wronght-Iron	13
Elm.	073	Vollow Ding	007
Elli	.013	Tellow Fille	.001

Table of short-linked Crane Chains and Ropes, showing the Dimensions and Weight of each and the proof of the Chain in Tons.

•	Diameter' of Chains.	Weight per Fathom.	Proof Strain.	Circum. of Rope.	W'g't of Rope per Fathom.				
-	Ins.	I fbs.	Tons.	Ins.	fbs.				
	3-16	6.	.75	21/2	1.5				
	- 3/8 - 7-16	8.5	1.5	31/4	1.5 2.5				
	7-16	11.	2.5	4	3.75				
	1/2	14.	3.5	43/4	5.				
	1/2 9-16	18.	4.5	51/2	7.				
	5/8 11-16	24. 28. 30. 36.	-5.25	61/4	8.7				
	11-16	28.	6.5	7	10.5				
	3/4	30.	7.75	71/2	12.				
	13-16	36.	9.25	81/4	15.				
	7/8	44.	10.75	. 9	17.5				
	15-16	50.	12.5	91/2	19.5				
	1	56.	14.	10	22.				

APPROXIMATE WEIGHT AND STRENGTH OF MANILLA CORDAGE.

Size	Size	Weight	Length	Strain
Circum'ce	Diameter	of 100	of	Borne by
Inches.	Inches.	Fathoms.	One fb.	New Ropes
	I	l lbs		ibs.
3/4	1/4	15	38 ft.	450
1	5-16	25	28 "	750
11/8	- 3/8	. 29	22 "	900
11/4	7-16	31	17 "	1,250
11/2	1/2	44	12 "	1,700 :
13/4	9-16	60	10 "	2,250
${\overset{13}{4}}_{2}$	5/8	79	71/2 ''	3,000
21/4	3/4	99	6 "	4,000
21/2 23/4 3	13-16	122	5 "	5,000 6,000
$23\overline{4}$	7/8	146	4 "	6,000
3	1	176	33/8 ''	7,000
31/4	1 1-16	207	3 "	8,500
31/2	11/8	240	21/2 ''	9,500
$33\!/\!4$	11/4	275	21-6	11,000
4	1 5-16	305	2 "	12,500
41/4	13/8	355	12/3 ''	14,000
$41/_{2}$	11/2	395	11/2 "	16,000

Relative Value of Various Woods, their Crushing Strength and Stiffness being Combined. Ash, 5. Beech, 44 Cedar, 1. Elm, 4.9 English Oak, 5.7 Mahogany, 3.7 Quebec Oak, 4.6 Spruce, 3.6 Sycamore, 2.6 Teak, 9.3 Walnut, 3.2 Yellow Pine 3.

Comparative Weight and Strength of Ropes and Chain Cables length of Cables and Weight of Anchors for Vessels.

Tonnage of Ship's	of	Len'th of Cabl's.	Average Weight per fat- hom.	strain of	Anchor	
Tens.	Ins.	Fath.	lbs.	Tons.	Cwt.	Ins.
25	1/2 9-16	120	14	41/2	2	43/4
- 35	9-16	120	17	51/2	21/2	51/2
45	5/8	120	21	7'-	23/4	61/4
50	11-16	120	25	81/2	3	7
75	3/4	120	30	101/8	31/2	73/4
100	13-16	150	35	1334	1 5	81/2
125	7/8	180	41	133/4 18	61/2	91/2
150	15-16	180	48	223/4	71/2	10
150 175	1	180	54	281/8	9	103/4
200	1 1-16	180	61	34	101/2	111/4
250	11/8	210	68	401/2	121/2	12
300	1 3-16	. 210	- 76	471/2	15	123/4
350	11/4	240	84	551/8	17	131/2
400	15-16	240	93	631/4	19	141/4
450	13/8	270	102	72	21	15
500	17-16	270	110	811/4	23 -	151/2
600	11/2	270	122 132	911/8	26	16
700 .	1 9-16	300	132	1	30	171/4
800	15/8	300	143		32	181/2
900	1 11-16	300	154		35 38	20/4
1000	13/4	300	166	-	38	
1200	1 13-16	300	178		40	
1400	17/8	300	191		43	
1600	1 15-16	300	201		46	
1800	2	300	217		48	
2000	21-16	300	230		50	
2500	21/8	330	244		53	7
3000 -	21/4	360	268		57	

FLAT ROPES.

Jron Wi	re Rope	e Steel W	Rope.	Hemp	Rope.	rig ing ibs
Size in Inches.	Weight per ft in lbs	Size in Inches	Weigh per ft in lbs.	Size in Inches.	Weight per ft. in lbs.	Breaki Strair Work'ı Load I
21/2×1/2 3×5/8 4×11-16 45/8×3/4	23/4	21/8×3/8 2×1/2 23/4×5/8 31/2×5/8	1 2-5 12/3 21/2 31/3	5×11/4 53/4×11/2 81/2×21/4 10×21/2	4 1-12	$ \begin{array}{c cccc} 23 & 3 & 5.800 \\ 28 & 7.150 \\ 45 & 12.300 \\ 60 & 15.000 \end{array} $

ROUND ROPES.

	n Wire opes.		el Wire Ropes.	He Ro	mp pe.	Ch	ain.	ing ons.	ng ps.
Cir- cum- fer- ence	W'g't per 100 feet in fbs.	Circum	W'g't per 100 Feet in fbs.	Circum	Wt. per 100 feet in lbs.	Size of Link.	Wt. 100 ft.in Ibs	Break Strain T	Worki Load L
13/4 2	40 52	$ \frac{11/_{2}}{15/_{8}} $	25 33	3 5	63 100	7-16 1/2	183 266	5 7	1.666 2.333
21/4 21/2	66 83	$\frac{17/8}{2}$	50 59	51/2 6	117 130	9-16 19-32	300 341	81/2 11	2.666 3.700
21/2 23/4 3	110 139	$\frac{21}{8}$ $\frac{23}{8}$	67 83	61/2 71/4	145 185	5/8 11-16	400 466	13 15	4.300 5.000
33/8 33/4	170 240	21/2 31/8	91 130	8	236 297	3/4 13-16	533 650	19 24	6.300 8.000
41/2	$\frac{260}{285}$	$ 33/8 \ 31/2 $	153 166	$91/_{2}$ $101/_{2}$	330 428	7/8 1	750 933	28 36	9.400 12.000

External Diameter.	Thickness.	Bursting per Sq. inch of Internal Surface.	Collapsing per Sq Inch of External Surface.		
Ins. 1.25 1.375 1.5 1.625 1.75 1.875 2.125 2.125 2.75 3.75 4.4.25 4.75	Ins088 .083 .083 .083 .083 .083 .083 .095 .095 .109 .109 .12 .12 .134 .134 .134 .134 .134	Lbs. 7700 6900 6200 5700 5300 4900 4500 4500 4800 4800 4800 4800 4200 3900 3600 3400 3200 3000	Lbs. 6500 5800 5200 4700 4300 4000 3700 3800 3600 3600 3100 2700 22700 22400 2100 1900 1700 1600		
5. 5.25 5.5 5.75 6.	.134 .148 .148 .148 .148	2800 3000 2800 2700 2600	1400 1400 1200 1100 1000		

Table of Areas and Circumferences from 1 foot to 9 feet (advancing by an inch), or from 1 to 9 Inches (advancing by a twelfth).

	(advancing by a twelfth).									
Diam.	Area.	Circum.	Diam.	Area.	Circum.					
1 ft.	.7854	3.1416	5 ft.	19.635	15.708					
1	.9217	3.4034	1	20.2949	15.9698					
2	1.069	3,6652	2 1	20.9658	16.2316					
3	1.2272	3.927	3	21.6476	16,4934					
4	1.3963	4.1888	4	22.3403	16.7552					
5	1.5763	4.4506	5	23.0439	17.017					
2 3 4 5 6 7	1.7671	4.7124	2 3 4 5 6 7 8	23.7583	17.2788					
7	1.969	4.9742	7	24.4837	17.5406					
8	2.1817	5.236	0	25.201	17.8024					
9	2.4053	5.4978	9	29.9673	18.0642					
10					10.0042					
10	2.6398	5.7956	10	26.7254	18.326					
11	2.8853	6.0214	11	27.4944	18.5878					
2 ft.	3.1416	6.2832	6 ft.	28.2744	18.8496					
1	3.4088	6.545	1 1	29.0653	19.1114					
2	3.687	6.8068	2	29.867	19.3732					
2 3 4 5 6 7 8 9	3.9761	7.0686	2 3 4 5 6 7	30.6797	19.635					
4	4.2761	7.3304	4	31.5033	19.8968					
5	4.5869	7.5922	5	32.3378	20.1586					
6	4.9087	7.854	6	33.1831	20.4204					
7	5.2415	8.1158	7	34.0394	20.6822					
8	5.5852	8.3776	8	34.9067	20.944					
0 -	5.9396	8.6394	9	35.7848	21.2058					
10	6.305	8.9012	10	36.6738	21.4676					
11	6.814	9.163	11	37.5738	21.7294					
3 ft.		9.4248	7 ft.		21.9912					
	7.0686	9.4240		38.4846						
1	7.4668	9.6866	1	39.4064	22.253					
2	7.8758	9.9484	2	40.339	22.5148					
3	8.2958	10.2102	3	41.2826	22.7766					
2 3 4 5 6 7	8.7267	10.472	2 3 4 5 6	42.2371 43.2025	23.0384					
5	9.1685	10.7338	5	43.2025	23.3002					
6	9.6211	10.9956	6	44.1787	23.562					
7	10.0848	11.2574	7	45.1659	23.8238					
8	10.5593	11.5192	8	46.1641	24.0856					
9	11.0447	11.781	9	47.1731	24.3474					
10	11.541	12.0428	10	48.193	24.6092					
11	12.0483	12.3046	11	49.2238	24.871					
4 ft.	12.5664	12.5664	8 ft.	50.2656	25.1328					
1	13.0955	12.8282	1	51.3183	25.3946					
5	13.6354	13.09	1 5	52.3818	25.6564					
9		13.3518	1 4	53.4563	25.9182					
1	14.1863 14.7481	13.6136	2	54.5417	26.18					
1	15 2000	10.0150	1 3							
23456789	15.3208	13.8754	2 3 4 5 6 7 8	55.638	26.4418					
0	15.9043	14.1372	6	56.7451	26.7036					
7	16.4989	14.499	7	57.8632	26.965					
8 -	17.1043	14.6608	8	58.9923	27.227					
9	17.7206	14.9226	9	60.1322	27.489					
10	18.3478	15.1844	10	61,283	27.750					
11	18.9859	15.4462	11	62.4448	28.012					
1	~		9 ft.	63.6174	28.274					

Table of Circumferences, Areas, Squares, Cubes, Square Root, Cube Root, from 1 to 10 Advancing by 1-16 etc.

Diam. or No.	Circum- ference.	Area	Square.	Cube.	Square Root.	Cube Root.
1	3.14	.785	1.	1.	1.	1.
1-16	3.34	.886	1.13	1.19	1.031	1.020
1/8	3.53	.994	1.27	1.42	1.060	1.040
3-16	3.73	1.107	1.41	1.67	1.089	1.059
1/4	3.93	1.227	1.56	1.95	1.118	1.077
5-16	4.12	1.353	1.72	2.26	1.146	1.095
3/8	4.32	1.485	1.89	2.60	1.173	1.112
7-16	4.52	1.623	2.07	2.97	1.199	1.129
1/2	4.71	1.767	2.25	3.38	1.225	1.145
9-16	4.91	1.917	2.44	3.82	1.250	1.161
	5.11	2.074	2.64	4.29	$1.250 \\ 1.275$	1.176
5/8 11-16	5.30	2.236	2.85	4.80	1.299	1.191
3/4	5.50	2.405	3.06	5.36	1.323	1.205
13-16	5.69	2.580	3.29	5.95	1.346	1.219
	5.89	$\frac{2.360}{2.761}$	3.52	6.59	1.369	1.233
78 15-16	6.09	2.948	3.75	7.27	1.392	1.247
2	6.28	3.142	4.	8.	1.414	1.260
1-16	6.48	3.341	4.25	8.77	1.436	1.273
	6.68	3.547	4.52	9.59	1.458	1.286
¹ / ₈ 3-16	6.87	3.758	4.78	10.47	1.479	1.298
	7.07	3.976	5.06	11.39	1.500	1.310
5.16						
0.10	7.26	4.200	5.35	12.36	1.521	1.322
3/8 7-1 6	7.46	4.430	5.64	13.40	1.541	1.334
	7.66	4.666	5.94	14.48	1.561	1.346
1/2	7.85	4.909	6.25	15.63	1.581	1.358
9-16	8.05	5.157	6.57	16.83	1.600	1.369
5/8	8.25	5.412	6.89	18.08	1.620	1.380
11-16	8.44	5.673	7.22	19.41	1.639	1.391
3/4	8.64	5.940	7.56	20.79	1.658	1.402
13-16	8.84	6.213	7.91	22.25	1.677	1.412
7/8	9.03	6.492	8.27	23.76	1.695	1.422
15-16	9.23	6.777	8.63	25.34	1.714	1.432
3	9.42	7.07	9	27.	1.732	1.442
1/8	9.82	7.67	9.77	30.52	1.768	1.462
1/4	10.21	8.30	10.56	34.32	1.803	1.482
3/8	10.60	8.95	11.39	38.44	1.837	1.5
1/2	11.00	9.62	12.25	42.88	1.871	1.518
5/8	11.39	10.32	13.14	47.63	1.904	1.535
3/4	11.78	11.05	14.06	52.73	1.936	1.553
7/8	12.17	11.79	15.02	58.17	1.968	1.570
4	12.57	12.57	16.	64.	2.	1.587
1/4	13.35	14.19	18.06	76.78	2.061	1.619
$1\sqrt{2}$	14.14	15.90	20.25	91.13	2.121	1.651
3/4	14.92	17.72	22.56	107.16	2.179	1.681
5	15.71	19.63	25.	125.	2.236	1.710
1/4	16.49	21.64	27.56	144.70	2.291	1.738

Table of Circum. Areas, Squares, Etc., (Continued).

Diam. or No.	Circum.	Areas.	Square.	Cube.	Square Root.	Cube Root.
51/2	17.28	23.76	30.25	166.37	2.345	1.765
3/4	18.06	25.07	33.06	190.11	2.398	1.792
6	18.85	29.29	36.	216.	2.449	1.817
1/4	19.64	30.68	39.06	244.14	2.500	1.832
1/4 1/2 3/4 7	20.42	33.18	42.25	274.63	2.550	1.866
3/4	21.21	35.78	45.56	307.55	2.599	1.890
7	21.99	38.48	49.	343.	2.646	1.913
1/4 1/2 3/4 8	22.78	41.28	52.56	381.08	2.692	1.935
1/2	23.56	44.18	56.25	421.88	2.739	1.957
3/4	24.35	47.17	60.06	465.48	2.784	1.979
8′	25.13	50.26	64.	512.	2.828	2.
1/4 1/2 3/4 9	25.92	53.46	68.06	561.52	2.872	2.021
1/5	26.70	56.75	72.25	614.12	2.915	2.041
34	27.49	60.13	76.56	669.92	2.958	2.061
9	28.27	63.62	81.	729.	3.	2.080
1/4	29.06	67.20	85.56	791.45	3.041	2.098
1/2	29.85	70.88	90.25	857.37	3.082	2.118
1/4 1/2 3/4	30.63	74.66	95.06	926.86	3.122	2.136
10	31.41	78.54	100.	1000.	3.162	2.154

TABLE OF CIRCUMFERENCES, AREAS, SQUARES, CUBES, SOUARE ROOT AND CUBE ROOT.
Advancing by Decimals from .1 to 10.

Diam. or No.	Circum.	Areas.	Square.	Cube.	Square Root.	Cube Reot.
.1	.314	.00785	.01	.001	.316	.464
.2	.628	.0314	.04	.008	.447	.585
.3	.942	.0706	.09	.027	.548	.669
.4	1.26	.1256	.16	.064	.633	.737
.2 .3 .4 .5	1.57	.1963	.25	125	.707	.794
.6	1.88	.2827	.36	.216	.775	.843
.6	2.20	.3848	.49	.343	.837	.888
.8	2.51	.5026	.64	.512	.894	.928
.9	2.83	.6362	.81	.729	.949	.965
1.	3.14	.7854	1.	1.	1.	1.
.1	3.46	.9503	1.21	1.33	1.049	1.032
.2	3.77	1.131	1.44	1.73	1.095	1.063
.3 .4 .5	4.08	1.327	1.69	2.20	1.140	1.091
.4	4.39	1.539	1.96	2.74	1.183	1.119
.5	4.71	1.707	2.25	3.37	1.225	1.145
.6	5.02	2.011	2.56	4.10	1.265	1.170
.7	5.34	2.270	2.89	4.91	1.304	1.193
.8	5.65	2.545	3.24	5.83	1.342	1.216
.9	5.96	2.835	3.61	6.86	1.378	1.239
2.	6.28	3.142	4.	8.	1.414	1.260
.1	6.59	3.464	4.41	9.26	1.449	1.281
.2	6.91	3.801	4.84	10.65	1.483	1.301

TABLE OF CIRCUMFERENCES, AREAS, SQUARES, CUBES, SQUARE ROOT AND CUBE ROOT.

Advancing by Decimals from .1 to 10. (TABLE CONTINUED).

(TABLE CONTINUED).								
Diam. or No.	Circum.	Areas.	Square.	Cube.	Square Root.	Cube Root.		
2.3	7.22	4.155	5.29	12.17	1.517	1.320		
.4	7.53	4.524	5.76	13.82	1.549	1.339		
	7.85	4.909	6.25	15.63	1.581			
5						1.357		
.6_	8.16	5.309	6.76	17.58	1.612	1.375		
.7	8.48	5.726	7.29	19.68	1.643	1.392		
.8	8.79	6.158	7.84	21.95	1.679	1.409		
.9	9.11	6.605	8.41	24.39	1.703	1.426		
3.	9.42	7.069	9.	27.	1.732	1.442		
.2	10.05	7.548	10.24	32.77	1.789	1.474		
.4	10.68	8.553	11.56	39.30	1.844	1.504		
$\dot{.6}$	11.30	10.18	12.96	46.66	1.897	1.533		
0	11.93	11.34	14.44	54.87	1.949	1.560		
1.0		12.57	16.					
4,	12.56			64.	2.	1.587		
4, .2	13.19	13.85	17.64	74.09	2.049	1.613		
	13.82	15.21	19.36	85.18	2.098	1.639		
.6 .8	14.45	16.62	21.16	97.34	2.145	1.663		
.8	15.08	18.10	23.04	110.6	2.191	1.687		
5.	15.70	19.63	25.	125.	2.236	1.710		
.2	16.33	21.24	27.04	140.6	2.280	1.732		
.4	16.96	22.90	29.16	157.5	2.324	1.754		
.6	17.59	24.63	31.36	175.6	2.366	1.776		
.8	18.22	26.42	33.64	195.1	2.408	1.797		
6.	18.84	28.27	36.	216.	2.449	1.817		
.2	19.47	30.19	38.44	238.3	2.490	1.837		
.4	20.10	32.17	40.96	262.1	2.530	1.856		
.6	20.73	34.21	43.56	287.5	2.569	1.876		
.8	21.36	36.32	46.24	314.4	2.608	1.895		
7.	21.99	38.48	49.	343.	2.646	1.913		
.2	22.61	40.72	51.84	373.2	2.683	1.931		
.4	23.24	43.01	54.76	405.2	2.720	1.949		
.6	23.87	45.36	57.76	439.	2.757	1.966		
.8	24.50	47.78	60.84	474.6	2.793	1.983		
8.	25.13	50.27	64.	512.	2.828	2.		
.2	25.76	52.81	67.24	551.4	2.864	2.017		
.4	26.38	55.42	77.56	592.7	2.898	2.033		
.6	27.01	58.09	73:96	636.1	2.933	2.049		
.8	27.64	60.82	74.44	681.5	2.966	2.065		
9.	28.27	63.62	81.	729.	3.	2.080		
.2	28.90	66.48	84.64	778.7	3.033	2.095		
.4	29.53	69.40	88.36	830.6	3.066	2.110		
.6	30.15	72.38	92.16	884.7	3.098	2.125		
.8	30.78	75.43	96.04	941.2	3.130	2.140		
		78.54	100.	1000.	3.162			
10.	31.41	1 10.04	100.	1000.	1 3.104	2,154		

Tables of Diameters, Areas, Circumferences of Circles, Squares, Cubes, Square Root, Cube Root, and Reciprocals of Numbers (From 1 to 250).

	of Numbers (From 1 to 250).							
No.	Cir.	4	Sq're.	Cube.	S.Root.		Recip.	
1	3.14	0.79	1	1	1.000	1.000	1.00000	
2	6.28	3.14	4	8	1.414	1.260	.50000	
3	9.42	7.07	9	27	- 1.732	1.442	.33334	
4	12.57	12.57	16	64	2.000	1.587	.25000	
5 6 7	15.71	19.62	25	125	2.236	1.710	.20000	
6	18.85	28.27	36	216	2.450	1.817	.16667	
7	21.99 25.13	38.48	49	343	2.646	1.913	.14285	
8	25.13	50.27	64	512	2.828	2.000	.12500	
9	28.27	63.62	81	729	3.000	2.080	.11112	
10	31.41	78.54	100	1000	3.162	2.154	.10000	
11	34.56	95.03	121	1331	3.317	2.224	.09091	
12	37.70	113.10	144	1728	3.464	2.289	.08333	
13	40.84	132.73	169	2197	3.605	2.351	.07692	
14	43.98	153.94	196	2744	3.741	2.410	.07142	
15	47.12	176.72	225	3375	3.872	2.466	.06667	
16	50.27	201.06	256	4096	4.000	2.519	.06250	
17	53.41	226.98	289	4913	4.123	2.571	.05882	
18	56.55	254.47	324	5832	4.242 4.358	2.620	.05556	
19	59.69	283.53	361	6859	4.358	2.668	.05263	
20 21	62.82	314.15	400	8000	4.472	2.714	.05000	
21	65.97	346.36	441	9261	4.582	2.758	.04761	
22	69.12	380.13	484	10648	4.690	2.802	.04545	
23	72.26	415.48	529	12167	4.795	2.843	.04347	
24	75.40	452.39	576	13824	4.898	2.884	.04167	
25	78.54	490.87	625	15625	5.000	2.924	.04000	
26	81.68	530.93	676	17576	5.099	2.962	.03846	
27	84.82	572.56	729	19683	5.196	3.000	.03703	
28	87.96	615.75	784	21952	5.291	3.036	.03571	
29	91.11	660.52	841	24389	5.385	3.072	.03448	
30 31	94.25 97.36	706.86	900	27000	5.477	3.107	.03334	
31	97.36	754.77	961	29791	5.567	3.141	.03225	
32	100.53	804.25	1024	32768	5.657	3.174	.03125	
33	103.67	855.30	1089	35937	5.744	3.207	.03031	
34	106.82	907.92	1156	39304	5.830	3.207 3.239 3.271	.02941	
35	109.96	962.11	1225	42875	5.916	3.271	.02857	
36	113.10	1017.88	1296	46656	6.000	3.301	.02666	
37	116.24	1075.21	1369	50653	6.082	3.332	.02702	
38	119.38	1134.11	1444	54872	6.164	3.361	.02631	
39	122.52	1194.59	1521	59319	6.244	3.391	.02564	
40	125.66	1256.64	1600	64000	6.324	3.419	.02500	
41	128.81	1320.25	1681	68921	6.403	3.448	.02439	
42 43	131.95	1385.44	1764	74088	6.480	3.476	.02380	
	135.09	1452.20	1849	79507	6.557	3.503	.02325	
44	138.23	1520.53	1936	85184	6.633	3.530	.02272	
45	141.37	1590.43	2025	91125	6.708	3.556	.02222	
46 47	144.51	1661.90	2116	97336	6.782	3.583	.02173	
48	147.66	1734.94	2209	103823	6.856	3.609	.02127	
	150.80	1809.56	2304	110592	6.928	3.634	.02083	
49	153.94	1885.74	2401	117649	7.000	3.659	.02040	
50	157.08	1963.50	2500	1 25000	7.071	3.684	.02000	

Tables of Diameters, Areas, Circumfer'ces, etc., (Continued).

No.	Cir.	Areas.	Sq're.	Cube.	S.Root.	C.R't.	Recip.
51	160.22	2042.82	2601	132651	7.141	3.708	.01960
52	163.36	2123.72	2704	140608	7.211	3.732	.01923
• 53	166.50	2206.18	2809	148877	7.280	3.756	.01886
54	169.65	2290.22	2916	156464	7.348	3.779	.01851
55	172.79	2375.83	3025	166375	7.416	3.802	.01818
56	175.93	2463.01	3136	175616	7.483	3.825	.01785
57	179.07	2551.76	3249	185193	7.549	3.848	.01754
58	182.21	2642.08	3364	195112	7.615	3.870	.01724
59	185.35	2733.97	3481	205379	7.681	3.892	.01694
60	188.50	2827.43	3600	216000	7.746	3.915	.01667
61	191.64	2922.47	3721	226981	7.810	3.936	.01639
62	194.78	3019.07	3844	238328	7.874	3.957	.01612
63	196.94	3117.25	3969	250047	7,936	3.979	.01587
64	201.06	3216.99	4096	262144	8.000	4.000	.01562
65	204.20	3318.31	4225	274625	8.062	4.020	.01538
66	207.35	3421.19	4356	287496	8.124	4.041	.01515
67	210.49	3525.65	4489	300763	8.185	4.061	.01492
68	213.63	3631.68	4624	314432	8.246	4.081	.01470
69	216.77	3739.28	4761	328509	8.306	4.101	.01449
70	219.91	3848.45	4900	343000	8.367	4.121	.01428
71	223.05	3959.19	5041	357911	8.426	4.140	.01408
72	226.19	4071.50	5184	373248	8.485	4.160	.01389
73	229.34	4185.09	5329	399017	8.544	4.179	.01369
74	234.48	4300.84	5476	405224	8.602	4.198	.01351
75	235.62	4417.86	5625	421875	8.660	4.217	.01333
76	238.76	4536.46	5776	438976	8.717	4.235	.01315
77	241.90	4656.63	5929	456533	8.775	4.254	.01298
78	245.04	4778.36	6084	474552	8.831	4.272	.01282
79	248.19	4901.67	6241	493039	8.888	4.290	.01265
80	251.33	5026,55	6400	512000	9.944	4.309	.01250
81	251.35 254.47	5153.00	6561	531441	9.000	4.326	.01234
82	257.61	5281.02	6724	551368	9.055	4.344	.01219
83	260.75	5410.61	6889	571787	9.110	4.362	01204
84	263.89	5541.77	7056	592704	9.165	4.379	.01190
85	267.04	5674.50	7225	614125	9.219	4.396	.01176
86	270.18	5808.80	7326	636056	9.273	4.414	.01162
87	273.32	5944.68	7569	658503	9.327	4.431	.01149
88	276.46	6082.12	7744	681472	9.380	4.447	.01136
89	279.60	6221.44	7921	704969	9.433	4.461	.01123
			8100	729000		4.481	.01111
90 91	282.74	6361.72	8281		9.487 9.539	4.497	.01098
	285.89	6503.88		753571			01096
92	289.03	6647.61	8464	778688	9.591	4.514	.01086
93	292.17	6792.91	8649	804357	9.643	4.530	.01075
94	297.31	6939.78	8836	830584	9.695	4.546	.01063
95	298.45	7088.22	9025	857375	9.746	4.562	.01052
96	301.59	7238.23	9216	884736	9.797	4.578	.01041
97	304.73	7389.81	9409	912673	9.848	4.594	.01030
98	307.87	7542.96	9604	941192	9.899	4.610	.01020
99	311.02	7697.69	9801	970299	9.949	4.626	.01010
100	314.16	7853.98	10000	1000000	10.000	4.642	.01000

Tables of Diameters, Areas, Circumfer'ces, etc., (Continued).

No.	· Cir.	Areas	Sq're.	Cube.	S.Root.	C. R't.	Recip.
101	317.30	8011.85	10201	1030301	10.049	4.657	.00990
102	320.44	8171.28	10404	1061208	10.099	4.672	.00980
103	323.58	8332,29	10609	1092727	10.148	4.687	.00970
104	326.73	8494.87	10816	1124864	10.198	4.702	.00961
105	329.87	8659.01	11025	1157625	10.246	4.717	.00952
106	333.01	8824.73	11236	1191016	10.295	4.732	.00943
107	336.15	8992.02	11449	1225043	10.344	4.747	.00933
108	339.29	9160.88	11664	1259712	10.392	4.762	.00925
109	342.43	9331.32	11881	1295029	10.440	4.776	.00917
110	345.58	9503.32	12100	1331000	10.488	4.791	.00909
111	348.72	9676.89	12321	1367631	10.536	4.806	.00900
112	351.86	9852.03	12544	1404928	10.583	4.820	.00892
113	355.00	10028.75	12769	1442897	10.630	4.834	.00884
114	358.14	10207.03	12996	1481544	10.677	4.848	.00877
115	361.28	10386.89	13225	1520875	10.723	4.862	.00869
116	364.42	10568.32	13456	1560896	10.770	4.876	.00862
117	367.56	10751.32	13689	1601613	10.816	4.890	.00854
118	370.70	10935.88	13924	1643032	10.862	4.904	.00847
119	373.85	11122.02	14161	1685159	10.908	4.918	.00840
120	376.99	11309.73	14400	1728000	10.954	4.932	.00834
121	380.13	11499,10	14641	1771561	11.000	4.946	.00826
122	383.27	11689.87	14884	1815848	11.045	4.959	.00819
123	386.41	11882.29	15129	1860867	11.090	4.973	.00813
124	389.56	12076.28	15376	1906624	11.135	4.986	.00806
125	392.70	12271.85	15625	1953125	11.180	5.000	.00800
126	395.84	12468.98	15876	2000376	11.224	5.013	.00793
127	398.98	12667.69	16129	2048383	11.269	5.026	.00787
128	402.12	12867.96	16384	2097152	11.314	5.039	.00781
129	405.27	13069.81	16641	2146689	11.357	5.052	.00775
130	408.41	13273.23	16900	2197000	11.401	5.065	.00769
131	411.55	13478.22	17161	2248091	11.445	5.078	.00763
132	414.69	13684.78	17424	2299968	11.489	5.091	.00757
133	417.83	13892.91	17689	2352637	11.532	5.104	.00751
134	420.97	14102.61	17956	2406104	11.575	5.117	.00746
135	424.12	14313.88	18225	2460375	11.618	5.129	.00740
136	427.26	14526.72	18496	2515456	11.661	5.142	.00735
137	430.40	14741.14	18769	2571353	11.704	5.155	.00729
138	433.54	14957.12	19044	2600872	11.747	5.166	.00724
139	436.68	15174.68	19321	2685619	11.789	5.180	.00719
140	439.82	15393.81	19600	2744000	11.832	5.192	.00714
141	442.96	15614.50	19881	2803221	11.874	5.204	.00709
142	446.11	15836.77	20164	2863288	11.916	5.217	.00704
143	449.25	16060.61	20449	2924207	11.958	5.229	.00699
144	452.39	16286.02	20736	2985984	12.000	5.241	.00694
145 146	455.53	16513.00	21025	3048625	12.041 12.083	5.253 5.265	.00689
140	458.67	16741.55 16971.67	·21316 21609	3112136 3176523	12.083	5.265	.00684
148	464.96	17203.36	21904	3241792	12.124	5.289	.00675
149	468.10	17436.62	22201	3307949	12.103	5.301	.00675
150	471.24	17671.46	22500	3375000	12.247	5.313	.00667
150	111.44	17071.40	1 44000	1 99 19000	14.441	0.013	1.00007

Tables of Diameters, Areas, Circumfer'ces, etc., (Continued).

100	ies of Die	ineters, A	reas, c	creamjer	ccs, e.c.	, (Conce	nueu).
No.			Sq're.		S.Root.		
151	474.38	17907.86	22801	3442951	12.288	5.325	.00662
152	477.52	18145.84	23104	3511808	12.328	5.336	.00657
153	480.66	18385.39	23409	3581577	12.369	5.348	.00653
154	483.81	18626.50	23716	3652264	12.409	5.360	.00649
155	486.95	18869.19	24025	3723875	12.449	5.371	.00645
156	490.09	19113.45	24336	3796416	12.489	5.383	.00641
157	493.23	19359.28	24649	3869893	12.529	5.394	.00636
158	496.37	19606.68	24964	3944312	12.569	5.406	.00632
159	499.51	19855.65	25281	4019679	12.609	5,417	.00628
160	502.65	20106.19	25600	4096000	12.649	5.428	.00625
161	505.80	20358.31	25921	4173281	12.688	5.440	.00621
162	508.94	20611.99	26244	4251528	12.727	5.451	.00617
163	512.08	20867.19	26569	4330747	12.767	5.462	.00613
164	515.22	21124.07	26896	4410944	12.806	5.473	.00609
165	518.36	21382.47	27225	4492125	12.845	5.484	.00606
166	521.50	21642.43	27556	4574296	12.884	5.495	.00602
167	524.65	21904.0	27889	4657463	12.922	5.506	.00598
168	527.79	22167.1	28224	4741632	12.961	5.517	.00595
169	530.93	22431.8	28561	4826809	13.000	5.528	.00591
170	534.07	22698.0	28900	4913000	13.038	5.539	.00588
171	537.21	22965,8	29240	5000211	13.076	5.550	.00584
172	540.36	23235.2	29584	5088448	13.114	5.561	.00581
173	543.50	23506.2	29929	5177717	13.152	5.572	.00578
174	546.64	23778.7	30276	5268024	13.190	5.582	.00574
175	549.78	24052.8	30625	5359375	13.228	5.593	.00571
176	552.92	24328.5	30976	5451776	13.266	5.604	.00568
177	556.06	24605.7	31329	5545233	13.304	5.614	.00564
178	559.20	24884.6	31684	5639752	13.341	5.625	.00561
179	562.34	25164.9	32041	5735339	13.379	5.635	.00558
180	565.49	25446.9	32400	5832000	13.416	5.646	.00555
181	568.63	25730.4	32761	5929741	13.453	5.656	.00552
182	571.77	26015.5	33124	6028578	13.490	5.667	.00549
183	574.91	26302.2	33489	6128487	13.527	5.677	.00546
184	578.05	26590.4	33856	6229504	13.564	5.687	.00543
185	581.19	26880.3	34225	6331625	13.601	5.698	.00540
186	584.34	27171.6	34596	6434856	13.638	5.708	.00537
187	587.48	27464.6	34969	6539203	13.674	5.718	.00534
188	590.62	27759.1	35344	6644672	13.711	5.728	.00531
189	593.76	28055.2	35721	6751269	13.747	5.738	.00529
190	596.90	28352.9	36100	6859000	13.784	5.748	.00526
191	600.04	28652.1	36481	6967871	13.820	5.758	.00523
192	603.19	28952.9	36864	7077888	13.856	5.768	.00520
193	606.33	29255.3	37249	7189057	13.892	5.778	.00518
194	609.47	29559.2	37636	7301384	13.928	5.788	.00515
195	612.61	29864.8	38025	7414875	13.964	5.798	.00512
196	615.75	30171.9	38410	7529536	14.000	5.808	.00510
197	618.89	30480.5	38809	7645373	14.035	5.818	.00507
198	622.04	30790.7	39204	7762392	14.071	5.828	.00505
199	625.18	31102.6	39601	7880599	14.106	5.838	.00502
200	628.32	31415.9	40000	8000000	14.142	5.848	.00500

Tables of Diameters, Areas, Circumfer'ces, etc., (Continued).

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1	Vo.	Cir.	Areas.	Sq're.	Sec. 1	S.Root.	14.	
$\bar{2}$	01	631.46	31730.9	40401	8120601		5.857	.00497
2	02	634.60	32047.4	40804	8242408	14.212	5.867	.00495
	03	637.74	32365.5	41209	8365427	14.247	5.877	.00492
	04	640.88	32685.1	41616	8489664	14.282	5.886	.00490
	05	644.03	33006.4	42025	8615125	14.317	5.896	.00487
	06	647.17	33329.2	42436	8741816	14.352	5.905	.00485
	07	650.31	33653.5	42849	8869743	14.387	5.915	.00483
	08	653.45	33979.5	43264	8998912	14.422	5.924	.00480
	09	656.59	34307.0	43681	9123329	14.456	5.934	.00478
2.	10	659.63	34636.1	44100	9261000	14.491	5.943	.00476
2	11	662.87	34966.7	44521	9393931	14.525	5.953	.00473
2	12	DDD.UI	35298.9	44944	9528128	14.560	5.962	.00471
2.	13	669.16	35632.7	45369	9663597	14.594	5.972	.00469
	14	672.30	35968.1	45796	9800344	14.628	5.981	.00467
	15	675.44	36305.0	46225	9938375	14.662	5.990	.00465
	16	678.58	36643.5	46656	10077696	14.696	6.000	.00462
2		681.73	36983.6	47689	10218313	14.730	6.009	.00460
	18	684.87	37325.3	47525	10360232	14.764	6.018	.00458
	19	688.01	37668.5	47961	10503459	14.798	6.027	.00456
22	20	691.15	38013.3	48400	10648000	14.832	6.036	.00454
2		694.29	38359.6	48841	10793861	14.866	6.045	.00452
22		697.43	38707.6	49284	10941048	14.899	6.055	.00450
22		700.57	39057.1	49729	11089567	14.933	6.064	.00448
22		703.71	39408.1	50176	11239424	14.966	6.073	.00446
22	20	706.86	39760.8	50625	11390625	15.000	6.082	.00444
22		710.00	40115.0	50876	11543176	15.033	6.091	.00442
22		713.14	40470.8	51529	11697083	15.066	6.100	.00440
22		716.28	40828.1 41187.1	51984	11852352 12008989	15.099	6.109	.00438
24	49	719.42 722.57	41547.6	52441 52900	12167000	15.132	6.118	.00436
25	50	725.71	41909.6	53361	12326391	15.165 15.198	6.126 6.135	.00434 $.00432$
25	20		42273.3	53824	12487168			.00434
23	94	728.85 731.99	42638.5	54289	12649336	15.231 15.264	6.144 6.153	.00431
2	00	735.13	43005.3	54756	12812904	15.297	6.162	.00429
23	05	738.27	43373.6	55225	12977874	15.329	6.171	.00425
2	36	741.42	43743.5	55696	13144256	15.362	6.179	.00423
2:		744.56	44145.8	56169	13312053	15.394	6.188	.00423
23		747.70	44488.1	56644	13481272	15.427	6.197	.00421
2:		750.84	44862.7	57121	13651919	15.459	6.205	.00420
24		753.98	45238.9	57600	13824000	15.491	6.214	.00416
24	ii/	757.12	45616.7	58081	13997521	15.524	6.223	.00414
24		760.27	45996.1	58564	14172488	15.556	6.231	.00413
24		763.41	46377.0	59049	14348907	15.588	6.240	.00411
24		766.55	46759.5	59536	14526784	15.620	6.248	.00409
24	15	769.69	47143.5	60025	14706125	15.652	6.257	.00408
24		772.83	47529.2	60516	14886936	15.684	6.265	.00406
24		775.96	47916.4	61009	15069223	15.716	6.274	.00404
24	18	779.11	48305.1	61504	15252992	15.748	6 282	.00403
24		782.26	48695.5	62001	15438249	15.779	6.282 6.291	.00401
	50	785.40	49087.4		15625000	15.811	6.299	.00400

TABLE of AREAS of SQUARES and CIRCLES, SIDE of SQUARE both in DECIMALS and FRACTIONS.

From 1-16 to 12.

Diam.	Area	Area	Side of	Square.
Diani.	of □ in Ins,	in O Ins.	In decim'ls.	In fracti'ns
1.6 1.6 1.6 1.6 1.6 1.6 1.6 1.6 1.6 1.6	.0039	.0081 .0123 .0276	.0553	16 in. 15 " 128 "
1 8	.0156	.0123	.1108 .1662	128
16	.0156 .0351 .0625	.0276	.1662	7×5
1	.0625	.0491	.2216	32 "
.5 T.6	.0976 .1406	.0767	.2769	
38	.1406	.1104	.3325	• 21 66
7	.1914	1503	.3877	
į	.25	.1963	.4431	. 76 -"
20	.3166	.2485	.4985	i" "
5	.3906	.3068	.5539	35 " 64 77 "
î,	.4727	.3712	.6093	77 60
3	.5625	.4418	.6646	21 " 32 "
13	.6603	.5185	.72	32
16 Z	.7656	.6013	7754	49 66
7 8 15 16	.879	.6903	.7754 .8308	64
116	1.	.7854	.8862	7 44
	1.129	.8868	.9416	8 66
16	1.266	.994		63 "
8,	1.409	1.107	.997 1.052	64
16	1.562	1.227	1.108	17 66
ą.	1.723			184 "
16		1.353	1.163	17 "
ř,	1.891	1.485	1.218	137 "
16	2.067	1.623	1.274	121 "
2	2.25	1.767	1.329	181 "
16	2.439	1.916	1.385	
8	2.641	2.764	1.44	17 "
16	2.864	2.25	1.495	
34	3.063	2.405	1.551	135 "
13	3.287	2.581	1.606	139 "
7 8	3.516	2.761	1.661	121 ''
11-18-11-14-51-1386-71-12-9-1-58-1-16-8-1-1-78-1-1-58-1-1-78-1-1-1-1	3.752	2.948	1.717	10000000000000000000000000000000000000
2	4.	3.142	1.772	125 "
1	4.516	3.546	1.883	-32
년(6 년 년 (3)(8 년(8 15)(8 (8)(4 주)(8	5.062 5.640 6.25 6.889	3.976	1.994	163 "
3	5.640	4.430	2.105	2.7. "
î	6.25	4,908	2.215	$\frac{2^{7}}{2^{7}}$ " $\frac{2^{7}}{3^{2}}$ "
5	6.889	5.412	2.326	221 "
3	7.56	5.939	2.437	264
4	8,264	6.492	2.548	935 "
$3_{\underline{s}}$	9.	7.069	2.659	921 66
	9.764	7.67	2.769	235 "
8.			2.709	97 "
3	10.561	8.296	2.88	25 " 263 "
100-148:00-164	11.388 12.25	8.946	2.991	264
2	14.20	9.621	3.102	37 "

TABLE of AREAS of SQUARES and CIRCLES, SIDE of SQUARE both in DECIMALS and FRACTIONS.

(Continued).

Diam	Area	Area	Side of	Square.
Diam.	of \square in Ins,	in O Ins.	In decim'ls.	In fracti'ns
358 344 7.8 4	13.138	10.321	3.213	$3\frac{7}{32}$ in. $3\frac{21}{64}$
3	14.065	11.045	3.323	321 "
7	15.01	11.793	3.434	37 "
48	16.	12.566	3.545	335 "
1	17.012	13.364	3.656	054 0716 0364 0364 0364 0364
i	18.058	14.186	3.766	349 "
3	19.141	15.033	3.877	37 "
8	20.254	15.904	3.987	363 "
10 14 300 10 10 10 10 10 10 10 10 10 10 10 10 1	21.385	16.8	4.098	47 "-
8	22.556	17.721	4.208	
7	23.748	18.655	4.321	47 "
_ B		10.000	4.041	421 "
9	25.	19.635	4.431	116
18143812583478 6	26.26	20.629	4.542	127
4	27.557	21.648	4.653	739
8	28.884	22.69	4.764	462
2	30.25	23.758	4.875	1 4点
- 8	31.641	24.851	4.985	463 "
34	33.06	25.967	5.096	53 "
8	34.516	27.109	5.317	53 " 513 " 564 "
6	36.	28.274	5.207	521 "
7	39.063	30.679	5.538	564 " 517 "
i	42.25	33.183	5.76	53 "
. 3	45.562	35.785	5.982	563 " 67 "
7	49.	38,485	6.203	67 "
8	52,562	41.282	6.425	627 "
i	56.25	44.179	6.646	641 "
3	60.062	47.173	6.868	655 "
8	64.	50.266	7.09	732 "
. 1	68.062	53.456	7.311	75 16
1	72.25	56.745	7.533	75 " 77 "
3	76.562	60.132	7.754	749 "
9	81.	63.617	7.976	749 " 763 "
1	85,563	67.201	8.198	Q13 ·
1 2 3 4	90.25	70.882	8.419	1 027
2 3	95.062			022
10		74.662	8.641	ORA
	99.98	78.54	8.862	064
4	105.04	82.516	9.084	3128
14 12 34	110.23	86.59	9.304	061
114	115.55	90.763	9.527	324
11	121.	95.033	9:748	93 "
14	126.54	99.402	9.975	1 10 "
. 2	132.22	103.87	10.19	1013 "
4	138.06	108.43	10.42	1013
12	144.	113.1	10.64	1041 "

ELECTRICITY.

Conductors.

Most Perfect.

All known Metals. Well-burned Charcoal. Plumbago. Burning Gaseous Matter or flame.

Smoke.

Smoke.

Less Perfect.

Concentrated Acids.
Dilute. Acids
Saline Fluids.
Living Animals.
"Vegetables.

Wood, in the ordinary state Snow, and Ice from

32° to 0°

Water.

Imperfect.

Common Earth and Stone. Dry Chalk and Lime. Marble and Porcelain.

Paper. Alkaline matter. Aqueous vapor. Non-Conductors.

Less Perfect.

Ice at 0° Farht. Dry Vegetable sub-

stances.
Dry Animal substan-

ces generally.
Parchment, Leather,
Feathers.

Baked Wood. [ces. Oil and Fatty substan-Silk.

Most Perfect.

Fur and Hair.

Dry gases including air. Pure Steam of highpressure.

Glass and all vitrifac-

Diamonds and transparent Gems.

Talc. Amber.

All Resinous Bodies.

Brimstone. Shell-lac. Bees-Wax.

The following is a short list of substances which may be used to receive the deposit of metal.

In all metallic solutions, acid,

Palladium. do. do. do. Silver. { In all alkaline, in all but the preceding, saline and acid.

do. Copper. do. do. Lead. do. do. do. Bismuth. do. do. do. Antimony. do. do. do. Tin. do. do. do. Iron. do. do. do.

Zinc. In some alkaline and acid.

NON-METALLIC SUBSTANCES.

In all saline or acid solutions; but not in alkaline. Sealing Wax, White Wax, Bees Wax and Rosin, Stearine, Spermaceti, Plaster of Paris prepared, some Animal substances, Most vegetables substances.

DEPOSITION of METALS. GOLD BATHS.

FOR SILVER, COPPER, or ALLOYS RICH IN THESE.

Distilled water, 1 gallon.
Phosphate of soda, cryst,
Bisulphite of soda
Cyanide of potassium, pure,
Gold Chloride, 160 grains,

Dissolve in a portion of the water, heated, phosphate of soda. Dissolve in another portion of the water the bisulphite of soda and cyanide of potassium. Dissolve the gold choloride in the remaining water, stir the solution slowly into the cold phosphate of soda solution, and finally add the solution of cyanide bisulphite. The bath, now ready for use, should be colorless. Used at a temperature of from 120° to 175° Fah.

BATH FOR IRON OR STEEL UNCOATED.

Distilled water 1 gallon. Phosphate of Soda. 7 4-5 oz. Bisulphite of Soda. Cyanide of potassium, pure. 3-5 dr. 160 grains.

Dissolve as before. Heat to 175° or 180° Fah. Pass the second metal through the hot potash, then through dilute muriatic acid (acid 1, water 15), brush, and connect at once. Requires a very intense current at first.

COLD ELECTRIC-GILDING BATH.

Water, distilled. 1 gallon. Potassium Cyanide, pure. 3 1-5 oz. Gold Chloride. 3 1-10 "

Dissolve the Cyanide in a part of the water, then gradually add the gold chloride dissolved in the remainder. Boil for half an hour before using. (Use cold).

ZINC BATH.

Zinc is used for the preservation of iron, by electro-depostion. The iron is first rendered perfectly clean and free from oxide, by placing it in a bath of heated sulphuric acid and water; then in a cold solution of sulphate of zinc. The positive pole of a galvanic battery is attached to a zinc plate, and the negative to the iron to be covered; the pure metal is deposited, and the zinc and the iron are amalgamated.

PLATINUM.

The best solution to be employed is the nitro-muriate of platinum, to which sufficient soda is added to render it neutral. The object to be coated should be smooth, and thoroughly cleansed by potash before the process is com-

6

menced. Having proceeded thus far, and the solution of platinum being ready, a fine-platinum wire in connection with the silver or positive pole of the battery, must be placed so as to dip into the solution, but must not be immersed beyond a very short distance. The object to be platinated is now ready for connection with the zinc or negative pole of the battery; after this is effected it is to be dipped in the solution.

SILVER BATH.

For electro-silver plating the double salt of silver and potassium cyanide is almost universally employed. The following are the proportions viz:

Water (soft), Cyanide of Potassium (pure), Nitrate of Silver, 1 gallon. 8 ounces. 514 "

Dissolve the nitrate of silver in a sufficient quantity of pure water (soft), and add to it gradually, with constant stirring hydrocyanic (prussic) acid until all the silver has been precipitated as cyanide, which may be known by the formation of no cloud in a portion of the clear liquid when a drop of the acid is added to it, avoid adding an excess of the acid. Throw the precipitate upon a fine cotton cloth filter, and as the liquid runs through wash the precipitate on the cloth several times with pure water. Dissolve the cyanide of potassium in the water, and stir in the cyanide of silver carefully removed from the cloth. If it does not dissolve in the liquid entirely, add more cyanide of potassium until it does, stirring continually. Let the impurities settle, and the bath is ready for use.

NICKEL BATH.

The nickel salts commonly used are the nickel ammonium sulphate (called double sulphate) and the corresponding chloride, Other salts, such as the nickel potassium cyanide, the acetate and sulphate, have been used, but not successfully as these.

The double sulphate bath may be prepared by dissolving three-fourths of a pound of the salt in each gallon of water, (soft). It should be kept neutral and up to about six degrees of hydrometer.

The double chloride bath requires about four ounces of the salt per gallon, and works better slightly acid, the tendency in working being towards alkalinity. The bath should be filtered when freshly prepared, and should be kept in a separate room, or at least away from the apartment in which the buffing or polishing is performed, to avoid contamination by dust as much as possible. Exposed to the air the bath (the water) evaporates, and the water thus lost must be replaced from time to time. Keep out dust as much as possible. It is well to cover the bath when not in use.

BRASS BATH.

Where the ordinary cheap commercial cyanide is employed the following answers very well:

Sulphate of Copper, Sulphate of Zinc, 4 to 5 ': Water, 1 gal.

Dissolve and precipitate with 30 ounces of carbonate of soda; allow to settle, and decant the clear liquid, and wash the precipitate several times with fresh water—after as many settling add to the washed precipitates:

Carbonate of Soda, Bisulphite of Soda, Water, 15 oz. 71/2 " 1 gal.

Stir to effect solution of these last two, then stir in ordinary cyanide of potassium until the liquid becomes clear and colorless. Filter if much iron or iron oxide (derived from impure zinc salt and cyanide) remains suspended in the liquid. An additional half ounce or so of the cyanide improves the conductivity of the solution.

COLD BRASS BATH FOR ALL METALS.

Carbonate of Copper (recently prepared). 2 oz. Corbonate of Zinc, 2 oz. Carbonate Soda 4 oz. Bisulphite of Soda, 4 oz. Cyanide of Potassium (pure), 4 oz. Arsenious Acid, 1-20 oz. Water, 1 gal.

Filter if necessary.

The arsenious acid is added to brighten the deposit, an excess is apt to give the metal a grayish-white color.

STEEL BATH.

In order to render copper-plates, which are used in printing, more durable, they can be covered with an electrolytic deposit of iron, which possesses an unusual degree of hardness, almost superior to steel. The salt usually employed has been the double sulphate of iron and ammonia. Professor Böttger, who first used this combination of salts in the process, has recently devised an improvement in the bath employed. He dissolves ten parts of ferrocyanide potassium (yellow prussiate of potash) and twenty parts of the double tartrate of soda and potash (Rochelle salts) in 200 parts of water, and to this he adds three parts of persulphate of iron dissolved in fifty parts of water. A large precipitate of prussian blue is formed; to the whole is added, drop by drop, with constant stirring, a solution of caustic soda until the blue precipitate entirely disappears, leaving a perfectly clear, light yellow liquid, which is now ready for use.

TIN BATH.

The following is one of the best solutions for plating with tin by the battery process:

Potassium pyrophosphate,	12 oz.
Protochloride of tin,	41/2"
Water	20 ""

The anode or feeding plate used in this bath consists of pure Banca tin. A moderately strong battery is required, and the work is finished by scratch-brushing.

COPPER BATH FOR ELECTROTYPING.

Dissolve sulphate of copper in water until the solution registers 15° by an acid hydrometer, then add enough sulphuric acid to make the hydrometer register 18°. This bath need not be filtered. It should be stirred about once or twice a week when using.

COPPER:-Cold Bath for Iron, Steel Etc.

Acetate of Copper.	3 oz.
Carbonate of Soda,	6 1-5"
Bisulphite of Soda,	3 1-5"
Cyanide of Potassium,	31/4 "
Water,	1 gallon.
Aqua Ammonia,	2 1-5 ft oz.

WARM BATH.

Acetate of Copper,	3 1-5 oz.
Carbonate of Soda,	3 1-5 "
Bisulphite of Soda,	1 1-5 "
Cyanide of Potassium,	41/2 "
Water,	1 gallon.
Aqua Ámmonia,	1 4-5 fl. oz.

In the preparation of these baths the salts are all dissolved together, except the copper acetate and ammonia. which are added after dissolving together in a small quantity of the water.

The deep blue color of the ammonia-copper solution should entirely disappear on mixing it with the other solution; otherwise, it becomes necessary to add more cyanide.

Cleansing Copper and Copper Alloys.

Potash, Caustic.	1 pound.
Water, Soft,	1 gallon.

Heat nearly to boiling in a cast iron pot provided with a cover. If the articles are much oxidized, pickle in a bath composed of-

Water. 1 gallon.

Sulphuric Acid, 1 pint.
until the darker portion is removed. Rinse in running water and dip in the following solution:

Water, soft, 1 gallon. Cyanide of Potassium, 8 ounces.

Remove from the bath, and quickly go over every part with a brush and fine pumice stone powder moistened with the cyanide solution.

CLEANSING CAST-IRON.

Cast-iron is freed from grease, etc., by dipping in hot alkali solution used for a similar purpose with copper, and after rinsing thoroughly it is pickled in water containing one per cent of sulphuric acid for several hours; then rinsed in water and scoured with a fine sharp sand or pumice powder and a fiber brush.

It is then rinsed and returned to the acid pickle for a short time, rinsed again, and put into the plating bath

directly.

CLEANSING WROUGHT-IRON.

The cleansing of wrought-iron, if much oxidized, is effected in the same manner as cast-iron; but it will bear a stronger pickle and a longer exposure. Whitened, filed, or polished iron may be treated like steel.

CLEANSING STEEL.

Dip in the caustic lye used for copper, etc., rinse thoroughly, scour with pumice powder moistened, rinse, and pass through the following dip:

> Water. 1 gallon. Hydrochloric Acid. 4 lbs.

Rinse quickly (but thoroughly) and plunge in the bath. Clean wrought-iron and steel gild well without an intermediary coating in hot electro-gilding baths. It is difficult to obtain an adhering coating of silver on these metals without interposing an intermediate coating of copper or brass, which renders the further operation of silver plating easy.

Cleansing Zinc, Tin and Lead.

Zinc is cleansed by dipping a few moments only (as the alkali quickly attacks the metal) in the hot potash lye, rinsing, and dipping into water containing about 10 per cent of sulphuric acid for a few minutes. Rinse in plenty of hot water, and, if necessary, scour with pumice stone powder and a stiff brush, moistened with a weak cyanide solution, or scratch brush. This last operation is especially useful when parts have been united with tin solder.

Tin, lead, and the alloys of these metals are more diffi-

cult to cleanse perfectly than zinc or iron.

Scour rapidly with the hot potash and brush, rinse quickly and brush, or dress with a piece of soft clean wood.

It is very difficult to obtain a satisfactory deposit of gold

or silver directly upon these metals or their alloys. The results are much better if a coating of pure copper is interposed.

GOLD PLATING BY SOLUTION.

A solution of gold is made in nitro-muriatic acid, and there is added to it twice as much sulphuric ether. The mixture must be shaken and allowed to repose when the ether with the chloride of gold will separate from the remaining liquid and rest above it. This dark colored ethereal solution is poured off from the light colored liquid beneath, and can be preserved for use in tight bottles, excluded from light. When applied it is with a very fine brush, or camels hair pencil the ether evaporates immediately leaving a coating of gold. This is burnished after being heated. The adhesion is more perfect, however, if the article be raised to a temperature approaching redness.

GILDING BRASS AND COPPER.

Brass and copper may be readily gilt, by being dipped in a dilute *neutral* solution of chloride of gold, and then washed and burnished.

GILDING BRASS AND COPPER.

A process was patented in 1836 by an English toy maker, and is well adapted for small articles. It consists in immersion them in hot solution of chloride of gold, to which has been added a considerable excess of bicarbonate of soda.

COPPER DEPOSITS BY DIPPING.

This is seldom practiced except on iron, as the deposits thus obtained are generally wanting in lasting qualities, since, from the thinness of the coating, the iron is but imperfectly protected from atmospheric influences. If the iron is dipped in a solution of—

Sulphate of Copper, $3\frac{1}{2}$ oz. Sulphuric Acid, $3\frac{1}{2}$ "Water, 1 to 2 gal,

it becomes covered with a coating of pure copper, having a certain adhesion; but should it remain there a few minutes, the deposit becomes thick and muddy, and not stand any rubbing. Small articles such as pins, hooks, and nails, are thus coppered by tumbling them for a few moments in sand, bran, or sawdust impregnated with the above solution diluted with 3 or 4 volumes of water.

TIN DEPOSIT BY DIPPING.

When immersed in a hot solution of tin properly prepared the metal is precipitated upon their surfaces. One of the best solutions for this purpose is the following:

Ammonia Alum, 1714 oz. Boiling Water, 121/2 ". Protochloride of Tin. 1

The articles to be tinned, first thoroughly cleaned, are put into the hot solution until properly whitened. A better coating can be obtained by using the following bath, and placing the pieces in contact with a strip of clean zinc also immersed:

Bitartrate of Potassa, 14 oz. Water (soft) - 24 "
Protochloride of Tin. 1 "

It should be boiled for a few minutes before using.

BRONZE DIP.

Nitric Acid, 8 oz. Alum, 1 oz. Muriatic Acid, 1 qt. Salt, 2 "
Sal-Ammoniac 2 oz. Water, 2 gal
Add the salt after boiling the other ingredients, and use hot.

BROWN BRONZE DIP.

Iron scales, 1lb; Arsenic, 1 oz; Muriatic Acid, 1 lb: A piece of solid Zinc, 1 oz. in weight to be kept in while useing.

NICKEL-PLATING DIP.

Into the plating vessel which may be of porcelain, or copper, is placed a concentrated solution of zinc chloride, which is diluted with from 1 to 2 volumes of water and heated to boiling. (If any precipitate separates, it is to be redissolved by adding a few drops of hydrochloric acid). As much powdered zinc as can be taken on the point of a knife is thrown in, by which the vessel becomes covered internally with a coating of zinc. The nickel salt for which purpose either the chloride or sulphate may be used—is then added until the liquid is distinctly green; and the articles to be plated, previously thoroughly cleaned, are introduced, together with some zinc fragments. The boiling continues for fifteen minutes, when the coating of nickel is completed, and the process is finished. The articles are well washed with water and cleaned with chalk. If a thicker coating be desired, the operation may be repeated.

SILVERING POWDER.

Silver powder may be prepared in the following manner: Precipitate, silver from its solution in nitrie acid, by dropping into it some plates of clean copper. Take 20 grs. of this powder and mix with it 2 drachms of cream of tartar the same quantity of common salt, and half a drachm of alum. These articles must be finely pulverized, and inti-

mately mixed in a mortar. If a little of this powder be moistened, and rubbed on a clean surface of brass or copper, the silver will be precipitated, and the surface of the metal will be covered with it.

STONE-WORK.

Stone walls are measured by the perch. A perch of stone is 24.75 cubic feet. When built in the wall, 234 cubic feet are allowed for the mortar and filling; hence, 22 cubic feet of stone make one perch of wall.

Masons estimate 3 pecks of lime and 4 bushels of sand

to a perch of wall.

To find the number of perches of stone in a wall, multiply together the length, height and thickness, in feet, and

divide by 22.

Openings less than 3 feet wide are counted solid; over 3 feet deducted, but 18 inches are added to the running measure for each jamb. Built arches are counted solid from their spring. Corners of buildings are measured twice. Pillars less than 3 feet are counted on 3 sides, as lineal, multiplied by fourth side and depth.

A cord of stone, 3 bushels of lime and a cubic yard of

sand will lay 100 cubic feet of wall.

It is customary to measure all foundations and dimension of stone by the cubic foot. Water tables and base courses by lineal feet. All sills and lintels or ashlar, by superficial feet, and no wall less than 18 inches thick.

The Greatest Load per Superficial foot.

Granite Piers.	=	: 40	Tons
Lime Stone Piers.		: 35	
Sand " "	=	: 15	66
Brickwork in Cement.	=	: 3	"
Rubble Masonry.	=		66
Lime Concrete foundation	-	: 2	1/9 "

The height of brick or stone piers should not exceed 12 times their least thickness at base.

BRICK-WORK.

Brick work is generally measured by 1000 bricks laid in wall. In consequence of variation in size of bricks, no rule for volume of laid brick can be exact. The following scale is, however, a fair average.

7	common	bricks	to a	superficial	foo	t 4	inch	wall.
15		66	66	- 66	66	8	6.	-66
23		44	66	66	_66	12	66	66
30		6.6	64	6.	4.6	16	4.4	66
38	64	6.6	4.6	4.6	46	20	6.6	66
45	4.4	6.6	64	44	66	24	6.6	-46 -

Corners are not measured twice as in stone work. Openings over two feet square are deducted. Arches are counted from the spring. Fancy work counted 1½ bricks for 1. Pillars are measured on their face only.

A cubic yard of mortar requires one cubic yard of sand and 9 bushels of lime, and will fill 30 hods.

One thousand bricks, closely stacked, occupy about 56 cubic feet.

One thousand old bricks, cleaned and loosely stacked, occupy about 72 cubic feet.

Five courses of brick will lay one foot in height on a chimney.

Nine bricks in a course will make a flue eight inches wide and twenty inches long, and eight bricks in a course will make a flue eight inches wide and 16 inches long.

One superficial foot of gauged arches requires 10 bricks. Common bricks are 734 to 8 inches long by 414 wide and 216 thick. Front bricks are 14 inch longer and wider.

It requires 20 common bricks to lay one cubic foot. In an 8 inch wall 15 common bricks make one foot of wall.

Stock bricks commonly measure 8¾ inches by 4¼ inches, by 2¾ inches, and weigh from 5 to 6 pounds each.

Paving-bricks should measure 9 inches, by $4\frac{1}{2}$ by $1\frac{3}{4}$ inches, and weigh about $4\frac{1}{2}$ pounds each.

One yard of paving requires 36 stock bricks, of above dimensions, laid flat, or 52 on edge; and 35 paving laid flat, or 82 on edge.

To find the number of bricks in a wall 12 inches or more in thickness, multiply together the length, height and thickness, in feet, and that 'again by 20. For an 8 inch wall, multiply the length by the height, and that by 15, and the product will be the number of bricks in the wall. If the wall is perforated by openings, such as door, windows, etc., multiply the length of such openings by the width, and that by the thickness, and deduct from the cubic contents of the wall before multiplying by 15 or 20 as above.

Bricks should be well wetted before use. Sea sand should not be used in the composition of mortar.

RED WASH FOR BRICKS.

To remove the green that gathers on bricks, pour over them boiling water in which any vegetables, (not greasy), have been boiled. Repeat for a few days, and green will disappear. For the red wash melt one ounce of glue in one gallon of water; while hot add alum size of an egg, one-half pound Venetian red, one pound Spanish brown. Try it; if too light add more red and brown. If too dark, water. Number of Brick required to Construct any Building. (Reckoning 7 bricks per superficial foot).

Super. ft. of	Number of Bricks to Thickness of Wall.						
Wall.	4 inch.	8 inch.	12 inch.	16 inch.	20 inch.	24 inch	
1	7	15	23	30	38	45	
2	15	30	45	60	75	90	
3	23	45	68	90	113	135	
2 3 4 5 6	30	60	90	120	150	180	
5	38	75	113	150	188	225	
6	45	90	135	180	225	270	
7	53	105	158	210	263	315	
7 8	60	120	180	240	300	360	
9	68	135	203	270	338	405	
10	75	150	225	300	375	450	
$\overline{20}$	150	300	450	600	750	900	
30	225	450	675	900	1125	1350	
40	300	600	900	1200	1500	1800	
50	375	750	1125	1500	1875	2250	
60	450	900	1350	1800	2250	2700	
70	525	1050	1575	2100	2625	3150	
80	600	1200	1800	2400	3000	3600	
90	675	1350	2025	2700	3375	4050	
100	750	1500	2250	3000	3750	4500	
200	1500	3000	4500	6000	7500	9000	
300	2250	4500	6750	9000	11250	13500	
400	3000	6000	9000	12000	15000	18000	
500	3750	7500	11250	15000	18750	22500	
600	4500	9000	13500	18000	22500	27000	
700	5250	10500	15750	21000	26250	31500	
800	6000	12000	18000	24000	30000	36000	
900	6750	13500	20250	27000	33750	40500	
1000	7500	15000	22500	30000	37500	45000	

PLASTERING.

Estimate of	Material for 100 sq	uare yaras.
MATERIALS.	Two coats, slipped coat finished.	Three coats with hard finish.
Quick Lime, " for fine stuff	3½ casks,	4 casks.
Plaster of Paris,		1/2 '' 2000
Laths,	2000	$2\bar{0}00$
Hair,	3 bushels,	4 bushels.
Common Sand,	6 loads.	7 loads.
White Sand,		21/2 bushels.
Nails.	13 pounds,	13 pounds.
Masons Labor,	31/2 days,	4 days.
Laborer,	2 days,	3 days.
Cartage.	34 days	1 day.

Plastering laths are usually of white or yellow pine, 11/2 inches wide, 1/4 inch thick, and 3 or 4 feet long. They are nailed up horizontally, about 1/2 inch apart. the upright stud or partitions are spaced at such distance apart (usually about 15 inches, centre to centre), that the ends of the laths may be nailed to them.

Laths are sold in bundles of 50 to 100 each. A square foot of surface requires, 11/2 four-feet laths, or 1000 such laths will-cover 74 square yards, and 12 pounds of nails will lay them on.

A carpenter can nail up the laths for from 40 to 60 square yards of plastering in a day of 10 hours, depending on the number of angles in the room, etc.

Plastering is always measured by the square yard for plain work, by the superficial foot for cornices or plain members, and by lineal foot for enriched members or carved mouldings in cornices.

The mortars used for inside plastering are termed conrse, fine, gauge or hard finish, and stucco.

Course stuff-Lime 1 part, sand 2 parts, hair 1-6 part.

Fine stuff (lime putty). Lump lime sclacked to a paste with a moderate volume of water. and afterwards diluted to the consistency of cream, and then to harden by evaporation to the required consistency for working.

Gauge stuff or Hard finish, is composed of from 3 to 4 volumes of fine stuff and one volume plaster of Paris, in proportions regulated by the degree of rapidity required in hardening; for cornices etc., etc., the proportions are equal volumes of each, fine stuff and plaster.

Stucco is composed of from 3 to 4 volumes of white sand, and one volume of fine stuff, or lime putty,

SHINGLES.

The best shingles are of white cedar.

When of good quality, they will last about 45 years in our northern State. Cypress and white pine are much used for shingles, but will not last half as long as white cedar.

Shingles are packed 250 in the bundle, or 4 bundles to 1000. One bundle 16-inch shingles will cover 30 square feet.

One bundle 18-inch shingles will cover 33 square feet. When laid 51/2 inches to the weather, 5 fbs., (4p) or 33/4 fbs. (3p) nails will lay them on.

COST of TIN ROOFING.

The following table shows the cost per square and sq. foot of tin roofing laid with 14 by 20 tin and 20 by 28 tin both flat and standing seam.

(A square is 100 square feet).

(11 04 300 0 00 100 04 0000).						
Flat S	eam Roo	fing.	Standing Seam Roofing.			
Cost w	ith 14×20	Tin.	Cost v	Cost with 14×20		
T. per box	T. per box Per sq. Per sq.ft.			Per sq.	Per sq.ft.	
\$4.25	\$2.21	.0221	\$4.25	\$2.37	.0237	
4.50	2.34	.0234	4.50	2.51	.0251	
4.75	2.47	.0247	4.75	2.65	.0265	
5.00	2.60	.0260	5.00	2.79	.0279	
5.25	2.73	.0273	5.25	2.93	.0293	
5.50	2.86	.0286	5.50	3.06	.0306	
5.75	2.99	.0299	5.75	3.20	.0320	
6.00	3.12	.0312	6.00	3.34	.0334	
6.25	3.25	.0325	6.25	3.48	.0348	
6.50	3.38	.0338	6.50	3.62	.0362	
6.75	3.51	.0351	6.75	3.76	.0376	
7.00	3.64	.0364	7.00	3.90	.0390	
Cost w	ith 20×28	3 Tin.	Cost with 20×28 Tin.			
\$8.00	\$2.01	.0201	\$8.00	\$2.15	.0215	
8.50	2.13	.0213	8.50	2.28	.0228	
-9.00	2.26	.0226	9.00	2.41	.0241	
9.50	2.38	.0238	9.50	2.55	.0255	
10.00	2.51	.0251	10.00	2.68	.0268	
10.50	2.63	.0263	10.50	2.82	.0282	
11.00	2.76	.0276	11.00	2.95	.0295	
11.50	2.88	.0288	11.50	3.09	.0309	
12.00.	3.00	.0300	12.00	3.21	.0321	
12.50	3.13	.0313	12.50	3.35	.0335	
13.00	3.25	.0325	13.00	3.48	.0348	
- 13.50	3.38	.0338	13.50	3.62	.0362	

For solders see page 210

SLATING.

A square of slate or slating is 100 superficial feet. In measuring, the width of the eaves is allowed at the widest part. Hips, valleys, and cutting are to be measured lineal, and 6 inches width extra is allowed.

The thickness of slates, ranges from 3-16 to 5-16 of an inch, and their weight varies from 2.6 to 4.5 lbs per square foot.

The lap of slates varies from 2 to 4 inches. The standard is assumed to be 3 inches.

The pitch of a slate roof should not be less than 1 inch in height to 4 inches in length.

66 66

DIMENSIONS OF SLATES AND NUMBER REQUIRED TO A SQUARE. (AMERICAN).

	SIZE		No. of Slate.	Weight per Sq. about.	8	SIZE		No. of Slate.	Weight per Sq. about.
12 12 12 14 14	by	6	533] lbs.	18	by	11	174) lbs.
12	"	7	457	 ≻ 850	20	"	10	169	
12	66	8	400		20	66	11	154	≻ 650
14	66	8	374	1	20	66	12	141	
14	66	. 8	327	≻ 750	22	66	11	138	
14	66	9	291		22	66	12	126	Υ
16	66	9	277	1	22	66	$\overline{13}$	116	
16	66	9	291 277 246		22 22 22 24	66	12	114	675
16	66	10	221	} 650	24	66	13	105	1 0.0
14 16 16 16 18	66	9	213	000	$-\frac{21}{24}$	66	14	98	
18	46	10	192		21		11	30	,

To compute the number of slates of a given size required per square. Subtract the lap from the length of the slate, and half the remainder will give the length of the surface exposed, which, when multiplied by the width of the slate, will give the surface required, and for which the party requiring the slating only pays.

Divide 14400 (the area of a square in inches) by the sur-

face thus obtained, and the quotient will give the number

of slates required for a square.

Illustration:—A slate is 24×12 inches, and the lap is 3 inches.

24-3=21, and $21\div 2=10.5$, which $\times 12=126$ inches; $14400\div$

126=144.29 slates.

Good American slate weighs about 174 pounds per cubic foot. Hence-

Slabs 34 inch thick weigh 10.86 pounds per square foot. 14.5

••	11/4	**	**	**	18.12	••	•••	••	
66	11/6	66	66		21.72	66	66	66	
66	11/ ₂ 11/ ₂	66	66		29.	66	66	"	

CORRUGATED IRON ROOFING.

Birmingham Wire Gauge.	W'g't per Square (100 Sq. feet). Plain or Painted.	GALVANIZED IRON.*
No. 28	97 fbs.	
26	105 "	Galvanized iron weighs
24	128 "	from 5 to 15 per cent.
24 22 20		heavier than plain, accord-
20	185 "	ing to the No. Birmigham
18		Wire Gauge.
16	340 "	mare dauger

^{*}See page 38 for sizes.

Lighter than No. 22 is not recommended, for a good durable roof.

Corrugated iron is usually made in sheets from 2 to 3

feet wide, and from 6 to 8 long.

The sheets when used for roofing should overlap about 6 inches in girth, and be double-riveted at the joints.

One-third of the net width may be allowed approximate-

ly for lappage and corrugations.

From 21/2 to 31/2 pounds of rivets will be required for a square.

PAINTING. *

For outside wood-work, paint made from white lead ground in linseed oil is most used. If the oil is raw, or unboiled, dryer is added; if boiled no dryer is necessary. Not less than four coats should be applied,—five are better.

Paint, ready mixed, put up in cans or kegs, may be procured from manufacturers or dealers. These paints have to be thinned by adding 1 pint of oil to about 2½ pounds of paint. When thinned, 1 pound will cover about 2 square yards; of first coat, 3 yards of second, and 4 yards of each subsequent coat; or 13% pounds, to the square yard will be required for 4 coats, and 15% for 5 coats.

For inside work, either white lead or oxide of zinc is

used, and for good work 4 coats are necessary.

For iron exposed to the weather, metallic paint, such as yellow and red iron othres or brown hematite ore, finely pulverized and mixed with oil or dryer, are best. If to the action of the water red lead is best.

Plastered walls should stand a year before painting.

Painting is measured by the square yard, girding every part of the work that is covered by paint and allowing an addition to the actual surface for the difficulty of covering deep quirk of mouldings and for "cutting in" as in sash and shelving, or where there is a change of color, on some work. Painters putty is made of spanish whiting, pulverized, 80 parts; boiled oil 20 parts; make into a stiff paste. If not intended for immediate use, raw oil shuld be used. One pound of putty for stopping every 20 yards.

GLAZIERS PUTTY.

Whiting, 70 pounds; boiled oil. 30 pounds; water 2 gals, mix. If too thin add more whiting; if too thick add more oil.

TO SOFTEN PUTTY.

To remove old putty from broken windows, dip a small brush in nitro-muriatic acid or caustic soda (concentrated lye), and with it anoint or paint over the dry putty that adheres to the broken glass and frames of your windows; after an hours interval the putty will have become so soft as to be easly removable.

* For mixing colors see page 109.

WASHES.

FOR OUTSIDE WORK.—In a tight box, slack half a bushel of fresh lime by pouring over it boiling water sufficient to cover it 4 or 5 inches deep, stir until slacked; add 2 lbs. of sulphate of zinc dissolved in water, add water enough to bring all to the consistency of thick white-wash

FOR INSIDE WORK.—Add 2 quarts of thin size to a pailful of wash just before using. The common practice of mixing salt with white-wash should not be permitted.

WHITE-WASH.—Whiting 4 pounds; common glue, two ounces; stand glue in cold water over night; mix whiting with cold water, heat glue till dissolved, and pour it hot into the former. Make of consistency to apply with common white-wash brush.

WHITE-WASH that will not rub off.—Mix up half pail full of lime and water, ready to put on the wall; then take one-fourth pint of flour, mix it with water, then pour on it a sufficient quantity of boiling water to thicken it, and pour it while hot into the white-wash; stir all well together, and it is ready for use.

FOR BRICK OR STONE WORK.—Slack 1/2 bushel of lime, as before in a barrel; then fill the barrel 2/3 full of water and add a bushel of hydraulic cement; add 3 pounds sulphate of zinc dissolved in water. The washes may be colored by adding powdered ochre, umber, etc.

DYEING.

GENERAL REMARKS.

Everything should be clean. The goods should be scoured in soap and the soap rinsed out. They are often steeped in soap lye over night. Dip them into water just before putting them into preparations, to prevent spotting. Soft water should be used, sufficient to cover the goods well—this is always understood where quantity is not mentioned. When goods are dyed, air, rinse well, and hang up to dry. Do not wring silk or merino dresses when scouring or dyeing them. If cotton goods are to be dyed a light color, they should be bleached.

SILKS.

BLACK.—Make a weak dye as for black on woolens; work goods in bichromate of potash a little below boiling heat, then dip in the logwood in same way; if colored in blue vitriol dye, use about the same heat.

ORANGE.—For one pound goods—annotto, one pound; soda, one pound; repeat as desired.

GREEN.-Very Handsome—For one pound goods—yellow oak bark, eight ounces; boil one half hour; turn off liquor from bark and add alum, six ounces; let stand until cold;

while making this, color goods in blue dye-tub a light blue; dry and wash; dip in the alum and bark dye. If it does not take well, warm the dye a little.

PURPLE.—For one pound goods.—First obtain a light blue, by dipping in home-made dye-tub; then dry; dip in alum, four ounces, with water to cover, when little warm. If color is not full enough add chemic.

YELLOW.—For one pound goods—alum, three ounces; sugar of lead, three-fourths ounce; immerse goods in solution over night; take out; drain, and make a new dye with fustic one pound; dip until required color is obtained.

CRIMSON.—For one pound goods—alum, three ounces; dip at hand heat one hour; take out and drain while making new dye by boiling ten minutes, cochineal, three ounces, brulsed nut-galls, two ounces, and cream-tartar, one-fourth ounce, in one pail of water; when little cool, begin to dip, raising heat to boil; dip one hour; wash and dry.

SKY BLUE ON SILK OR COTTON.—Very beautiful.—Give goods as much color from a solution of blue vitriol, two ounces, to water, one gallon. as it will take up in dipping fifteen minutes, and then run it through lime water. This will make a beautiful and durable sky blue.

Brown on SILK OR COTTON.—Very beautiful—After obtaining a blue color as above, run goods through a solution of prussiate of potash, one ounce, to water, one gallon

LIGHT BLUE.—For cold water, one gallon, dissolve alum, one-half tablespoon, in hot water, one tea-cup, and add to it, then add chemic, one teaspoon at a time to obtain the desired color—the more chemic, darker the color.

WOOLEN GOODS.

CHROME BLACK.—Best in use.—For five pound goods, blue vitriol, six ounces; boil a few minutes, then dip goods three-fourths hour, airing often; take out goods, make a dye with three pounds logwood, boil one-half hour, dip three-fourths hour and air goods, and dip three-fourths hour more. Wash in strong suds. This will not fade by exposure to sun.

WINE COLOR.—For five pound goods, camwood, two pounds; boil fifteen minutes and dip goods one-half hour; boil again and dip one-half hour; then darken with blue vitriol, one and one-half ounces; if not dark enough, add copperas, one-half ounce.

SCARLET.—Very fine.—For 'one pound goods—creamtartar, one-half ounce; cochineal, well pulverized, one-half ounce; muriate of tin, two and one-half ounces; boil up the Gye and enter the goods; work them briskly for ten or fifteen minutes, then boil one and one-half hours, stirring goods slowly while boiling. Wash in clean water and dry in the shade.

PINK.—For three pound goods—alum, three ounces; boil and dip the goods one hour; then add to the dye, creamtartar, four ounces; cochineal, well pulverized, one ounce; boil well and dip the goods while boiling until the color suits.

BLUE.—Quick Process.—For two pound goods—alum, five ounces; cream-tartar, three ounces; boil goods in this one hour, then put goods in to warm water which has more or less extract of indigo in it, according to the depth of color desired, and boil again until it suits, adding more of the blue if needed.

MADDER RED.—To each pound of goods—alum, five ounces; cream-tartar, one ounce. Put in goods and bring kettle to a boil, for one-half hour, then air them and boil one-half hour longer; empty kettle and fill with clean water; put in bran, one peck; make it milk-warm, and let is stand until bran rises, then skim off the bran and put in one-half pound madder; put in goods and heat slowly until it boils and is done. Wash in strong suds.

GREEN.--For each pound of goods-fustic, one pound; with alum, three and one-half ounces; steep until strength is out, and soak goods therein until a good yellow is obtained; then remove the chips and add extract of indigo or chemic, one tablespoon at a time, until color suits.

SNUFF BROWN, DARK,—For five pound goods—camwood, one pound; boil it fifteen minutes, then dip goods three-fourths hour; take out goods, and add to the dye, two and one-half pounds fustic; boil ten minutes and dip goods three-fourths hour; then add blue vitrol, one ounce; copperas, four ounces; dip again one half hour. If not dark enough, add more copperas.

ANOTHER METHOD.—Any shade.—Boil goods in a mordant of alum, two parts; copperas, three parts; then rinse them through a bath of madder. The tint depends on the relative proportions of the copperas and alum; the more copperas, the darker the dye. Joint weight of both should not be more than one-eighth of weight of goods, Mixtures of reds and yellows with blues and blacks, or simple dyes, will make any shade.

ORANGE.—For five pound goods—muriate of tin, six tablespoons; argal, four ounces; boil and dip one hour, and add again to the dye one tea-cup madder; dip again one-half hour. Cochineal, about two ounces, in place of madder, makes a much brighter color.

PURPLE.—For each pound goods—two ounces cudbear; rinse goods well in soap suds, then dissolve cudbear in hot suds—not quite boiling—and soak the goods until of required color. The color is brightened by rinsing in alum water.

YELLOW.—Rich.—Work five pound goods one-half hour in a boiling bath with three ounces bichromate of potassa and two ounces alum; lift and expose till well cooled and drained, then work one-half hour in another bath with five pounds fustic. Wash out and dry.

CRIMSON.—Work for one hour in a bath with one pound cochineal paste; six ounces dry cochineal; one pound tartar, one pint protochloride of tin. Wash out and dry.

SALMON.—For each pound goods—14th pound annotto; one-fourth pound soap; rinse goods in warm water, put them into mixture and boil one-half hour. Shade will be according to amount of annotto.

DOVE and SLATE COLORS—of all shades.—Boil in iron vessel a teacup of black tea with teaspoon of copperas, and sufficient water. Dilute till you get the shade wanted.

COTTON GOODS.

BLACK.—For five pound goods—boil them in a decoction of three pounds sumach one-half hour, and steep twelve hours; dlp in lime water one-half hour; take out and let them drip one hour; run them through the lime water again fifteen minutes. Make a new dye with two and one-half pounds logwood (boiled one hour), and dlp again three hours; add bichromate potash, two ounces to the logwood dye, and dlp one hour. Wash in clear cold water and dry in shade. Only process for permanent black.

SKY BLUE.—For three pound goods—blue vitriol, four ounces; boil few minutes, then dip goods three hours; then pass them through strong lime water. A beautifut BROWN can be obtained by next putting goods through a solution of prussiate of potash.

GREEN.—Dip goods in home-made blue; dye until blue enough is obtained to make the green as dark as required; take out, dry and rinse a little. Make a dye with fustic, three pounds, logwood, three ounces, to each pound goods, by boilling dye one hour; when cooled so as to bear hand, put in goods, move briskly few minutes, and let lie one hour; take out and thoroughly drain; dissolve and add to the dye for each pound of cotton, blue vitriol, one-half ounce, and dip another hour. Wring out and let dry in the shade. By adding or diminishing the logwood and fustic, any shade may be had.

Yellow.—For five pound of goods—seven ounces sugar of lead; dip goods two hours; make new dye with bichromate of potash, four ounces; dip until color suits; wring out and dry. If not yellow enough, repeat.

ORANGE:-For five pound goods-sugar of lead, four

12 to pica

ounces; boil few minutes; when a little cool, put in goods; dip two hours; wring out; make a new dye with bichromate of potash, eight ounces; madder, two ounces; dip until it suits; if color is toored, take small sample and dip into lime water and choose between them.

RED.—Muriate of tin, two-thirds teacup; add water to cover goods; raise to boiling heat; put in goods one hour; stir often; take out, empty kettle, put in clean water with niewood, one pound; steep one-half hour at hand heat; then put in goods and increase heat one hour.—not boiling. Air good and dip one hour as before. Wash without soan.

PRINTING.

1 Point.

EXPLANATION OF POINT SYSTEM.

	OIII			•			12 to picu
2							6 to pica
3	66						4 to pica
31/2	2 " .						Brilliant
4	4.6						3 to pica
41/9	2 "						Diamond
5							Pearl
51/2	2 "						Agate
6	44						Nonpareil
7							Minion
8	66					. "	Brevier
9	66				٠.	-	Bourgeois
10	- 6.						Long Primer
11	66		Dr.				Small Pica
12	- 66			1	-1-		2 line Nonpareil
14	6.6				٠.		2 line Minion or English
16	66					. 2	line Brevier or Columbian
18	46						Nonpareil or Great Primer
20	66						e Long Primer or Paragon
24	**						4 line Nonpareil
30	66	•	-				5 " "
36	66		٠.				` 6 " "
42	٠.	1		-			
48			•	•	•	•	8 " "
60	-66		- "				10 " "
72	66	3					. 12 " "
14		. *					14

SIZES OF PRINTING TYPES.

NAME OR BODY.	Size in dec.of a lin. inch.	ger than	Ems& dec of an em in a lineal foot.	dec. of
Diamond.	.0595	lineal in.	201.587	140.637.46
Pearl.	.0668	.0072	179.593	32,253.97
Agate.	.075	.0081	160.	25,600.
Nonpareil.	.0841	.0091	142.543	20,318.73
Minion.	.0994	.0103	126.992	16,126,98
Brevier.	.1060	.0115	113.137	12,800.
Bourgeois.	.1190	.0129	100.793	10,159.36
Long Primer.	.1336	.0145	89.796	8,063.49
Small Pica.	.15	.0163	80.	6,400.
Pica.	.1683	.0183	71.271	5,031.74
English.	.1889	.0206	63.496	4,031.74
Columbian.	.2121	.0231	56.568	3,200.
Great Primer.	.2381	.0259	50.396	2,539.84
Paragon.	.2672	.0291	44.898	2,015.87
Double Small Pica.	.3	.0327	40.	1,600.
Double Pica.	.3367	.0367	35.635	1,269.92
Double English.	.3779	.0412	31.748	1,007.93
Double Columbian.	.4242	.0462	28.284	,800.

American and British Types are cast 92-100 ths of an inch in height. The European Printing Types are of many different heights.

SIZES AND WEIGHTS OF PAPER.

Owing to the variations in sizes and weight of paper made by different mills, it is almost impossible to give a perfect scale. The following, however, are the sizes and weights most generally used.

NEWS PAPER.

Imperial22>	(32	22, 25 lbs.
Small Double Medium 24"	3625,	28. 30 lbs.
Double Medium24"	38.28, 30, 32, 36,	40, 44, 50.
Double Royal25"	39 and 26×40.36	6, 40, 50, 60.
Double Super Royal28"	42 and 29×43	.36, 40 lbs.
Double Imperial32"	46 and 33×464	15, 50, 53.

	OK PAPER.
+Medium	$19 \times 24 \dots 25, 30, 35 \text{ lbs.}$
†Super Royal	20" 2420, 25, 30, 40 lbs. 22" 2830, 40 lbs.
* "	22" 2835, 40, 50, 60, 70, 80 lbs. 24" 3030, 40 lbs.; unsized.
Medium-and-half	24" 3030, 40 lbs.; unsized.
†Double Medium	24" 38.32, 36, 40, 44, 50, 56, 60.
* - " _ "	24" 3835, 40, 45, 50, 60, 70, 80.
*Double Royal	26° 40 40, 50, 60 lbs.

*Double Super Royal, Double Imperial, *Sized and calendered. $28{\times}42$ $45,\,50,\,60$ lbs- 32``46 $65,\,70$ lbs.; unsized+ $\dagger\text{Sized}$ and unsized.

FLAT PAPER.

lat	Letter,	10×16	7, 8, 9, 10, 12, 14 lbs.
66	Small Cap,	13" 16	12, 14,16 lbs.
66	Cap,	14" 17	10, 12, 14, 16, 18 lbs.
66	Crown,	15" 20	21 lbs.
16.6	Demy,	16" 21	16, 18, 20 22, 24, 28 lbs.
46	Folio.	17" 22	14, 16, 18, 20, 22, 24 lbs.
6.6	Double Cap.	17" 28	24, 28, 32, 36 lbs.
66	Medium,	18" 23	24, 28, 32, 36, 40 lbs.
66	Royal.	19" 24	42 lbs.
66	Super Royal,	20" 28	52 lbs.
66	Imperial	22" 30	65 lbs.

MISCELLANEOUS.

Bond Paper, 14 by 17, 17 by 22, 19 by 23. Blotting Paper, 19 by 24, 60, 80, 100, 120 lbs. Card Sheets, 22 by 28. Cover Papers, 20 by 25. 25, 35 lbs, Glazed, Plated, and Enameled Papers, 20 by 24.

UPPER CASE.

	-			-	_		Carlo A	-	1907.00		-		. 1.4	100
ı	*	+	1	9	1	7	fist		·	• •	2m	ID	18	0
1	1/2	1/4	3/4	1/3	3/3	1/8	3/8	%	1 %	2m	3 m	-	-	-
ı	&	Æ,	Œ	æ	œ	£	8	E	Ξ	2m	3m	Æ	Œ	8
	Λ	В	C	D	E	F	G	Α	В	C	D	E	F	G
1	н	ī	К	L	M	N	0	Н	T	K	L	M	N	ठ
1	P	Q	R	8	Т	v	w	P	Q	R	S	T	V	W
1	Х	Y	7.	J	U.	I)	X	Y	Z	J	U	Ħ	m

LOWER CASE.

血	h:r	5m 4m	'. k		1 2	3 4	5	Q	7	8
j	h	c	d	е	i	s	ſ	0	ff	9
1	Ľ						Ŀ	5	fi	0
1 Z	1	m	n	h	0	ур	w	,	n od	m
X	-	-	-	3m	. ~		;	:	20	Rm
q.	V	u	t	spc	.a	r	-	-	Pia	ds.

Average Daily Performance of Presses,

The estimates of the following table are for miscellaneous work, done in the usual manner, with little making ready, and under the favorable conditions of a brisk season. It is supposed that the presses are at work full ten hours; that feeders and pressmen are expert and diligent; that paper, rollers, steam power, ink, etc., are in perfect order, and that there are no detentions or accidents:

Make Ready Time.	Style of Press.—No. of Forms.	Time of Press Work.	Rate per hour.	Daily perf'r- ance.
Hours.		Hours.		Impr.
	Card Press.			
1	1 form of 7.500 impressions.	9	833	7.500
4	4 " 1.000 "	9 6	666	4.000
$\frac{1}{4}$	4 " 1.000 " 8 " 250 "	4	500	2.000
	Small Machine Press.			
1	1 form of 6.000 impressions.	9	666	6.000
5	5 " 500 "	5	500	2.500
1 5 8	5 " 500 " 10	9 5 2	400	800
	Hand Press.			1. 1.
1	1 form of 1.500 impressions.	9	156	1.500
14	250 "	9	166	1.000
	Medium Cylinder.		0	
1	1 form of 7.500 impressions.	9	833	7.500
5	5 " 750 "	5	750	3.750
1 5 7	5 " 750 " 8 " 250 "	9 5 3	666	2.000
	Double Medium Cylinder.			L
2		8	666	5.000
5	1 form of 5,000 impressions.	5	600	3.000
2 5 7	6 " 250 "	8 5 3	500	1.500
	Mammoth Cylinder.		1	
3	1 form of 4.000 impressions.	7	570	4.000
5	2 '' 1.250 ''	5 3	500	2,500
3 5 7	4 " 250 "	3	333	1.000

MEASURING TYPE OR MATTER.

The measurement is made by multiplying the number of solid ems contained in the length of any body of type, by the number contained in the width of the measure. The gauge for measurement is an em of the type in which the matter calculated is set.

In book offices it is usual to count the matter appearing below the head line in the above manner, counting three ems in addition for the head line with its blank and the foot line, without regard to the size of the type in which they are set. In measuring the subject matter, anything in excess of an em and less than a half em is not counted, while an en, or an excess making less than an em, is counted as a full em.

Chapter heads, blank spaces, or cuts occurring in the dimensions of pages are rated the same as though the space occupied consisted of type. It is also customary to count as type a cut occupying a whole page when backed

by printed matter.

Quotations, poetry, and matter set in smaller type than the body of the work, are always counted according to the size of type in which they are set, distinct from the larger type in the same page or body of matter, commencing at the first line and extending to the first line of the larger type.

Pages set in columns, include all spaces between the columns and bordered pages are measured from outside to outside of border by the ems of the type which they

enclose.

Side and centre notes, in Bibles or law works, are measured by the full width of the note and the full length of the page, in the type of which they are composed.

The mode of acertaining the number of ems in a line is by laying as many of the letter m flatwise in the stick as

will make the measure.

It is customary in many newspaper offices to count the rule set between the advertisements as a line of type, although it may not be of the required depth. This necessitates counting the lines where a number are set together.

COMBINATION LEADS.

The following table shows the combinations that can be formed by leads or slugs of six lengths only, not more than three pieces being required at one time.

LENGTH IN EMS OF THE PIECES EMPLOYED,

			4, 7	, 9, 13,	15, 20.			
4,	4	8 11 12 14 16 17 18 19 21 22 23 24 25	13,	13	26	15,	15, 9	39
7.	4	11	20.	7	27	20,	20	40
4.	4. 4	12	15.	13	28	15.	13, 13	41
7.	7	14	20.	9	29	20,	15, 7	42
9.	7	16	15.	15	30	15,	15, 13	43
13.	4	17	20.	7. 4	31	20.	20, 4	44
9.	9	18	15.	13, 4	32	15,	15, 15	45
15.	4	19 -	20.	13	33	15, 20, 15, 20, 15, 20, 15, 20, 20, 20, 20,	15, 9 20 13, 13 15, 7 15, 18 20, 4 15, 15 13, 13 20, 7 15, 13 20, 9	39 40 41 42 43 44 45 46 47 48 49 50
7.	7. 7	21	15.	15, 4	34	20,	207	47
15.	7	22	20,	15	35	20,	15, 13	48
15.	4. 4	23	20.	9. 7	36	20,	20, 9	49
20.	4	24	15.	15, 7	37 .	20,	15, 15	50
4, 7, 4, 7, 9, 13, 9, 15, 7, 15, 15, 20, 9,	4 4, 4 7 7 4 9 4 7, 7 7 4, 4 9, 7	25	13, 20, 15, 20, -15, 20, 15, 20, 15, 20, 20,	13 7 13 9 15 7, 4 13, 4 15, 4 15, 9, 7 15, 7 9, 9	26 27 28 29 30 31 32 33 34 35 36 37	,	, , ,	-

The printer has also at command the six single pieces used, viz: 4, 7, 9, 13, 15 and 20 ems. By using four, five, or six pieces together, the above combinations may be extended, consecutively to one hundred ems. Fonts of these leads, of suitable proportions, are put up and for sale by the different type founders.

CASTING OFF COPY.

The first step necessary is to take a comprehensive view of the copy, noticing whether it has been written even or has many interlineations, etc., and observing also the number of break-lines, and whether the work be divided into chapters and sub-heads, in order that the allowance may be made for them in the calculation. These observations may be noted on a separate piece of paper, to assist the memory and save the trouble of re-examining the This preparation being made, we ascertain manuscript. the number of words contained in the line by counting several separate lines in various parts of the copy, so that the one we adopt may be a fair average. We then take the number of lines in a page, and multiply by the number of words found in the average line. The quotient we then multiply by the quantity of folios the manuscript copy may contain, and thus we get the amount of words contained in the work, with a tolerable degree of accuracy. The necessary allowances should be made for breaklines chapters, insertions, etc., according to the observations previously made on the memorandum. If information has been furnished as to the size of letter the work is to be done in and the width of the page, we make our measure accordingly, and, by composing a few lines of the manuscript copy, we ascertain what number of words will come into each printed line. We then take the length of our page in lines, and multiply the one by the other, thus getting the number of words in the printed page. The quotient gives the number of pages the manuscript will make. If too many, the page must be enlarged; if too few, the page must be diminished in width and length. For example: We take the number of words in a line of manuscript at 20, the lines in a page at 50; we multiply 50 by 20, which will produce 1,000 words in a page; we then multiply 1,000 by 422, the number of the folios in the manuscript, and we find it contains 422,000 words. The work being printed in Pica octavo, 20 ems measure, and each line containing 10 words, each page 40 lines, the case will stand thus.

Manuscript.	Printed.
50 20	40 10
1000 422	400) 422000 words in MS. 1055 pages.
2000 2000 4000	Divide
422000 words in MS.	16)1055(65 sheets. 15 pages.

HOW TO BEND BRASS RULE.

By taking brass rule and heating it until about to turn red, and then immersing it in cold water, it can be easily bent to any desired shape.

RILEY'S INDISPENSABLE.

No. 1—For Fine Job Work. Dumar Varnish, 6 oz; Bergamot, 2 drachms; Balsam Copaiba, 2 drachms; Balsam of Fir, 3 oz., Creosote, 1 drachm; Copal Varnish one drachm. To enough ink for 1.000 ordinary business cards, add from 8 to 12 drops of the "Indispensable," and to larger quantities in proportion. When used for Bronze, Dry Colors, Diamond Printing, etc., take twice the quantity; and where an extra quick dryer is desired, add a few drops of dissolved Gum Arabic to the ink, after it has mixed with No. 1. In all cases, mix well with the ink before applying to the rollers.

HOW TO ESTIMATE THE QUANTITY OF TYPE.

To ascertain the quantity of Plain Type required for a Newspaper or Magazine, or any other work, find the number of square inches and divide the same by four, the quotient will be the approximate weight of matter: But as it is impossible to set the cases entirely clear it is necessary to add 25 per cent. to large fonts, and 33 per cent. to small fonts for dead matter.

Rule and figure work double price matter.

ROMAN NUMERALS.

Capitals are chiefly employed in designating the order of succession of kings, in chapter headings, and in indicating dates; while lower case are used as folios of a book, or to indicate chapter or verses referred to in the text.

The Following is a Complete System of Roman Enumeration.

1 I.	60 LX. 70 LXX.
2 II. 3 III.	80 LXXX, or XXC.
4 IIII or IV.	90 LXXXX, or XC.
5 V.	100 C.
6 VI.	200 CC.
7 VII.	300 CCC.
8 VIII. or IIX.	400 CCCC.
9 VIIII. or IX.	500 D, or IQ.
10 X.	600 DC, or IQC.
11 XI.	700 DCC, or IQCC.
12 XII.	800 DCCC, or IOCCC.
13 XIII. or XIIV.	900 DCCCC, or IDCCCC.
14 XIIII. or XIV.	1,000 M. or CIO.
15 XV.	2,000 CIOCIOTICIC.
16 XVI.	5,000 IV or 100.
17 XVII.	10,000 X or CCIOO.
18 XVIII. or XIIX.	
19 XVIIII or XIX.	50.000 L or 1000.
20 XX	100,000 C or CCCI
30 XXX	1,000,000 M or CCCCI
40 XXXX or XL.	, , , , , , , , , , , , , , , , , , , ,
50 L.	2,000,000 MM.

As often as a character is repeated, so many times is its value repeated.

A less character before a greater diminishes its value, as IV=V-I, or 1 subtracted from 5=4.

A less character after a greater increases its value, as XI=X+I, or 1 added to 10=11.

For every 3 annexed, the sum is increased 10 times.

For every C and O, placed one at each end, the sum becomes 10 times as many.

A bar thus —, over any number, increases it 1,000 times. Illustration.—1840, MDCCCXL. 18560, XVIIIDLX.

FOLDING PAPER.

FOLIO.—The standard size of this is 25 by 38. The half sheet folded in two leaves, having four pages, makes a book called a folio.

 $\ensuremath{\textit{QVARTO}}.\xspace$ —When the half sheet is folded in four leaves, making eight pages, it forms a quarto.

OCTA VO.—The half sheet folded again, eight leaves, sixteen pages, forms an octavo; or folded in sixteen leaves forms a 16 mo.

DUODECIMO.—By folding the same into twelve leaves, making twenty-four pages, we have a duodecimo. Folded into eighteen leaves, we form an 18 mo., into twenty-four leaves, and we have a 24 mo., etc.

The words, Post, Crown, Demy, Royal, etc., used in connection, as Royal Octavo, designate the size of paper of

which the book is made.

Modern facilities for the manufacture of paper enable publishers to have any desired size made to order,

Marks occasionally found at the bottom of a page are termed signatures (such as a. b, c; or 1, 2, 3; or 1* 2* 3*), and are used for the direction of the pressman and binder in printing, folding and gathering sheets.

Amount of Paper Required for a Book of any Size.

								Amount
No. of		Num		for 1000				
form.								cop's in
	[8 Mo	12 Mo	16 Mo	18 Mo	24 Mo	32 Mo	36 Mo	R. & qr.
1	8	12	16	18	24	32	36	1R 2qr
1 2 3 4 5 6 7 8 9	16	24	32	36	48	64	72	2-4
3	24	36	48	54	72	96	108	3 6
4	32	48	64	72	96	128	144	48
5	40	60	80	90	120	160	180	510
6	48	72	96	108	144	192	216	612
7	56	84	112	126	168	224	252	7-14
8	64	96	128	144	192	256	288	816
9	72	108	144	162	216	288	324	918
10	80	120	160	180	240	320	360	11
11	88	132	176	198	264	352	396	12 2
12	96	144	192	216	288	384	432	13 4
13	104	156	208	234	312	416	468	14 6
14	112	168	224	252	336	448	504	15 8
15	120	180	240	270	360	480		1610
- 16	128	192	256	288	384	512	30.	1712
17	136	204	272	306	408	-		1814
18	144	216	288	324	432			1916
19	152	228	304	342	456		i	2018
20	160	240	320	360	480			22
20 21	168	252	336	378	504			23 2
22	176	264	352	396				24 4
23	184	276	368	414				25 6
24	192	288	384	432				26 8
25	200	300	400	450				2710

EXAMPLE:—How many reams will be required for a 16 mo. book of 320 pages? Find the number of pages (320) in the 16 mo column; and on the same line in the outer column we find 22 reams. For books with a greater number of forms than is given in the table find the quantity for half the forms and multiply by 2. If the forms are odd subtract 1 from its number and find 1/2 multiply by 2 then add the first figures in the outer column (1 R. & 2 qrs).

Y of PAPER REQUIRED for ANY JOB of FROM 50 to 10,000 COPIES.

		HANDI MECHANICAL,
grs stds	48	000000000011114222428 222200000001111422242
shts	36	00000000000000000000000000000000000000
shts	32	126 5 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
spts	24	0000001111112222460851 2000001111112222460851
sids	- 1	20086694469322222222222222222222222222222222
shts	8	211000012410111111111111111111111111111
sprs	91	2000 100 100 100 100 100 100 100 100 100
spre		0 0 4 4 4 4 5 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
shts	11	00000000000000000000000000000000000000
shts	-	0000111123282844400001188888 02524012800021245088828088286 8452898888888888888888888888888888888888
	_	251122422347122222222222222222222222222222
10146	-	$\begin{array}{c} 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 $
S STO	-	E1277244477794447779444
3		012224000000000000000000000000000000000
` T		00101284 101
		12446680214163812288488488888888888888888888888888888
lo səle bəʻr	No. Cop Red	88888888888888888888888888888888888888
	super	210 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2

COMPOSITION ROLLERS, for Summer Use.

Are made of a mixture of the best glue and refined syrup, in the proportion of 10 pounds glue to 5 quarts of syrup. Soften, but not over soak, the glue with water; then melt it; then add the syrup and let the mixture boil briskly for 30 minutes.

WINTER USE.

Composition Rollers for winter use, or for extreme cold weather, are made in the proportions of five pounds of glue to five quarts of syrup. This makes a tender roller, which may be stiffened by adding 2 ounces of tar.

Roller composition should not be over cooked: If it is boiled 40 or 50 minutes, or more, the syrup will candy, and the composition will be spoiled.

How to MIX PRINTING INK (and Paints) FOR TINTS.

Mixing Red and Black makes	Brown.
Lake and White makes	Rose.
Umber and White makes	Drab.
White and Brown makes	Chestnut.
Yellow and Brown makes	Chocolate.
Red with Light Blue makes	Purple.
Carmine with Straw makes	Flesh color.
Blue with Lead color makes	Pearl.
Carmine with White makes	Pink.
Lamp-Black with Indigo makes	Silver Gray.
" " White makes	Lead color.
Paris Green with White makes	Bright Green.
Yellow-Ochre and White makes	Buff.
White tinted with Purple makes	
Black with Chrome Green makes	
Emerald Green with White makes	
Vermillion with Chrome Yellow	
Chrome Yellow and White Lead m	
White tinted with Ded and Veller	akes Strawcorr.
White tinted with Red and Yellov	makes Cream.
Chrome Yellow, Blue, Black and	Red makes Onve.
Chrome Green with White makes	Pea Green.
Yellow and Carmine or Deep Red	makes Scarlet.
Carmine and Blue makes Deep 1	Lilac, Violet Pur-
ple and Plum.	
Blue and Black makes Deep Bl	ue or Blue-Black.

Vermillion and Black makes
Yellow and Black makes
Yellow Blue and Black makes
Orange Mineral and White make beautiful Flesh
Tints.

Violet and White makes pale Lilac or Lavender.

Mixing Yellow and Blue makes bright or a Light Green.
Ultramarine, white and Carmine form the various

tones of Lilac, etc. Red, yellow and black makes Copper. Red, umber and black makes Claret. White, vermillion, blue and yellow makes Dove. White, yellow and red makes Fawn. Red, black, yellow other and white, Free stone. White, Prussian blue and gray, French Gray. White, stone other and red makes Gold. Lemon. White and chrome vellow makes. White, yellow ochre, black and red, Limestone. White and vermillion, makes, White, vermillion and Lake makes, Peach. Pink. White, yellow ocher, black and red. Sandstone. Red, blue and white makes. Violet.

COMBINATION of INK that HARMONIZE WELL.

Two Colors.—Scarlet Red and Deep Green; Orange and Violet; Light Blue and Deep Red; Yellow and Blue; Black and Salmon; Black and Light Green; Dark and Light Blue; Carmine and Emerald; Brown and Carmine; Purple and Green. Three Colors.—Red, Yellow and Blue; Orange. Black and Light Blue; Light Salmon, Dark Green and Scarlet; Brown, Light Orange and Purple; Dark Brown, Orange Yellow and Blue; Crimson Lake, Greenish-Yellow and Black. Four Colors.—Black, Green, Dark Red, and Sienna; Scarlet, Dark Green, Lavender and Black; Ultramarine or Cobalt Blue, Vermillion, Bronze Green, and Lilac; Sienna, Blue, Red and Black.

NEWSPAPER MEASUREMENT.

Table showing number of ems of the different Newspaper Type in a line, the number of lines necessary to make 1.000 ems, and the length in inches. Also the number of ems in the regular length of (13 em Pica wide) columns.

	Aga- te.	Nonp.	Min- ion.	Bre- vier.	Bourg	Long Prim.
No. ems in line. No. lines 1.000 ems. No. In. 1.000 ems.		26 381/2 31/4	221/4 45 43/8	19½ 51⅓ 5⅔	171/3 572/3 71/4	151/2 641/2 9
No. Columns.	No	o. ems	in C	ol. Fo	lio or C	uarto.
4 5 6 7 8	6.505 7.180 7.900	6.160	4.115 4.515 4.970		2.525 2.770 3.050	1.610 2.085 2.290 2.520 2.755
9				4.575		2.970

LEADS FOR NEWSPAPER.

Table showing the number of Leads 13 ems Pica long, contained in one pound and the number required to lead 1.000 ems of matter, together with the number of leads in a single column of matter regular size newspaper.

Size of Body Type to be Leaded with 6-to-Pica Leads.

	Aga- te.	Non- pareil		Bre- vier.		Long Prim
No. Leads to lb. " 1.000 ems.	60 26	60 29	60 34	60 40	60 45	60 52
No. of Columns.	No.	Leads	in Col.	Folio	or Qua	arto.
5	132 170	125 162	108 140	99 128	88 114	108
6	185 206	179	154 169	141 155	125 138	119 131
8 9	224 241	215 233	185 201	169 183	150 163	143 154

STANDARD SIZES OF NEWSPAPERS.

The following are the regular size, adopted by the auxiliary printers. We would advise parties planning new newspaper to adopt one of these sizes. The width of column is 13 ems.

00-11				
No. Col-		FOL10.		
umns.	Size of Paper	Size of Form	Head Rule.	Col.Rule.
5	20 by 26	173/4 by 233/4	111/8	173/4
6	22 " 31	1934 " 2814	133/8	1934
7	24 " 35	2134 " 33	1534	213/4
8	26 " 40	2334 " 371/2	18	233/4
9	28 " 44	253/4 " 42	201/4	253/4
		QUARTO.		
4	22 by 31	1834 by 29	87/8	133/4
5	26 " 40	231/4 " 37	111/8	1734
6	30 ** 44	2734 " 41	133/8	1934
7	35 " 48	321/2 " 45	153/4	213/4

STANDARD NEWSPAPER MEASURE.

The STANDARD newspaper measure, as recognized and now in general use, is 13 Ems PICA. The Standard of Measurement of all sizes of Type is the Em QUAD, not the letter m.

LEADS and SLUGS.

Leads are designated as "—to-Pica," the number being that fraction of a Pica which the lead is, viz: a 6-to-Pica lead is one-sixth of a Pica in thickness, or six 6-to-Picas are equal to one Pica; four 4-to-Picas one Pica, and so with other sizes or thickness of leads.

SLUGS.—Leads of Nonpareil thickness and greater are called Slugs, viz: Nonpareil Slugs, Brevier Slugs, Pica Slugs, etc., a Pica is one-sixth of an inch nearly.

AVERAGE WEIGHT OF MATTER.

A piece of solid matter 13 Ems Pica wide and 6 inches long will weigh *about* 336 pounds, but in order to allow for the sorts usually remaining in the case, 436 pounds of Type would be required to set that amount of solid matter.

When the matter is to be leaded the weight of the Type

may be reduced about one quarter.

A piece of solid matter 12 inches square will weigh about 40 pounds. One pound of Type will therefore, measure 33/s square inches. A piece of leaded matter 12 inches square will contain about 30 pounds of Type.

Leads Required for Newspaper and Book Work.

To lead 1 fb., of Pearl requires 6 ounces of 6-to-Pica leads, Agate 51/2 ounces, Nonpareil 5 ounces, Minion 41/2 ounces, Brevier 4 ounces. Bourgeois 31/2 ounces, Long Primer 3 ounces, Small Pica 23/4 ounces, Pica 21/2 ounces, English 21/4 ounces.

COLORED PRINTING-PAPER.

Are made either by adding coloring-matter to the pulp, or, when peculiarly brilliant colors are required, by painting or staining the paper. By the use of both processes a great variety of shades is produced. In printing on colored papers, it should be remembered that the appearance of the ink is affected by the color of the paper. When black letters appear on a colored surface-ground, they lose the intense hue they have when printed on white paper. On blue they are a failure; on orange (red lead) they are telling and brilliant, and assume a greenish bronze, on violet they are rich, in a Greenish-Yellow tone; the majority of yellows are weakened by black, which is thus rendered more intense. It should be remembered that—

- 1. Black Ink upon Red appears Dark Green.
- 2. Black Ink upon Orange, Bluish-black.
- $\!\!\!\!/$ 3. Black Ink upon Yellow is Black, with a slight tinge of Violet.
 - 4. Black Ink upon Blue is Orange-gray.
 - 5. Black Ink upon Green appears Reddish-gray.
 - 6. Black Ink upon Violet appears Greenish-yellow-gray.

MARKS OR PUNCTUATIONS.

	Comma.	4	Cedilla.
	Semicolon.	Λ	Caret.
	Colon.	44- 27	Quotation Marks.
	Period.		
	Dash.	1	Brace.
?	Interrogation.	(
1	Exclamation.	***	Ellipsis.
0	Parenthesis.		Ellipsis; also leaders.
Ħ	Brackets or Crotchets		Ellipsis.
-	Hyphen.	*	Asterisk.
,	Apostrophe.	†	Dagger, or Obelisk.
1	Acute Accent.	1 1	Double Dagger.
1	Grave Accent.	S	Section.
^	Circumflex Accent.		Parallels.
47	Circumflex or Tilde.	9	Paragraph.
-	The Long or Macron.		Index.
v	The Short or Breve.	*** or ***	Asterism.
••	Diæresis.		

CORRECTIONS OF THE PRESS.

4, or 3, (dele) Delete, take out, or expunge.

Turn a reversed letter.

A space, or more space between words, letters, or lines. Less space, or no space, between words or letters.

L or I carry a word further to the left or to the right.

D Indent.

- Elevate a letter, word, or character that is sunk below

the proper level.

- Sink or depress a letter, word, or character raised above the proper level. Shows that a portion of a paragraph projects laterally

beyond the rest.

L Directs attention to a quadrat or space which improp-

erly appears. x, or + directs attention to a broken or imperfect letter.

Bring a words or words to the beginning of a line; also, make a new paragraph.

Make a new paragraph.

- Change from Italic to Roman, or from Roman to Italic, as the case may be.

= Put in small capitals.

Put in Capitals.

Note.—The other marks are self-explanatory; but the following observations used in correcting proof-sheets,

require explanation:-

wf. Wrong font;-used when a character is of a wrong size or style; tr., Transpose; t.c., Lower-case; i, e., put in small or common letters a word or letter that has been printed in capitals or small capitals; s. caps, or sm. c., Put in small capitals; Qu., Qy., or? Query; Out, s. c. words are wanting, see copy.

FIRST PROOF FROM THE TYPE.

THE CROWNING OF PETRARCH.

Nothing can be conceived more affecting or noble than that ceremony. The superbe palaces and porticos by which had rolled the ivory chariots of Marius and and Caesar had long mouldered into dust. The laureled fasces, the golden eagles, the shouting Legions, the cap tives, and the pictured cities were indeed wanting to his victorious procession. The scep-. tre had passed away from Rome. But she still retained the mightier influence of an empire intellectual and was now to conter the prouder reward of an intellectual trinmph. To the man who had extended the dominion of her ancient language who had erected the trophies of philosophy and imagination in haunts of ignorance and fervency, the whose captives were the he arts of admiring nations; enchained by the influence of his songwhose spoils were the treasures of ancient genius-the Eternal City offered the glorious and just tribute of her gratitude.

Amid the ruined monuments of ancient, and the infant eructions of modern art, he who had restored the broken link between thetwo ages of human civilization was crowned with the wreath which he had deserved from the moderns who owde to him their refinement—from the ancients who owed to him their fame Never was a coronation so august witnessed by westminister or Rheims.

MACAULAY.

A CORRECTED PROOF SHEET.

Caps. THE CROWNING OF PETRARCH. Nothing can be conceived more affecting or a capon that estemony. The superby palnoble than that ceremony. The superbe pal-Nomaces and porticos by which had rolled the ivory chariots of Marius and and Caesar had long at mouldered into dust. The laureled fasces, the golden eagles, the shouting Legions, the cap, Itives, and the pictured cities were indeed want-ing to his victorious procession. The sceptre had passed away from Rome. But she still retained the mightier influence of an emor pire intellectual, and was now to conter the stil prouder reward of an intellectual tripmph. To a the man who had extended the dominion of her ancient language who had erected the trophies of philosophy and imagination in L/L the L haunts of ignorance and fervency, Collead whose captives were the he arts of admiring share bet. nations; enchained by the influence of his songwhose spoils were the treasures of ancient gen-Homi vius-the Eternal City offered the glorious and to just tribute of her gratitude. No Amid the ruined monuments of ancient, and the infant eractions of modern art, he 2/ who had restored the broken link between # [thetwo ages of human civilization was crowned with the wreath which he had deserved from the moderns who owde to him their refinement &. -from the ancients who owed to him their x O tame Never was a coronation so august witnessed by westminister or Rheims. Lexial from obscurty and decay

PROOF SHEET CORRECTED.

THE CROWNING OF PETRARCH.

Nothing can be conceived more affecting or noble than that ceremony. The superb palaces and porticos by which had rolled the ivory chariots of Marius and Cæsar had long mouldered into dust. The laureled fasces, the golden eagles, the shouting legions, the captives, and the pictured cities were indeed wanting to his victorious procession. The scepter had passed away from Rome. But she still retained the mightier influence of an intellectual empire and was now to confer the prouder reward of an intellectual triumph. To the man who had extended the dominion of her ancient language who had erected the trophies of philosophy and imagination in the haunts of ignorance and ferocity, whose captives were the hearts of admiring nations, enchained by the influence of his song-whose spoils were the treasures of ancient genius rescued from obscurity and decay-the "Eternal City" offered the just and glorious tribute of her gratitude. Amid the ruined monuments of ancient, and the infant erections of modern art, he who had restored the broken link between the two ages of human civilization was crowned with the wreath which he had deserved from the moderns , who owed to him their refinement,-from the ancients who owed to him their fame. Never was a coronation so august witnessed by Westminister or Rheims.

COMPLETE TABLE OF SIGNATURES.

EIGHT VO.

	LIGI	11 VO.		7
1 1 2 BC DE 3 BC DE 5	369 377 385 393 391 409 417 425 433 441 449 455 447 505 513 521 529 537 548 551 561 561 562 563 664 665 665 665 677 705 705 713 721	478494505123343333333333333333333344444444444444	729 737 745 745 753 761 769 7785 798 809 817 825 898 897 865 887 888 889 897 905 913 921 929 937 945 953 961 969 1007 1009 1017 1025 1033 1041 1049 1047 1065 1073 1081	92 4 RS 93 4 4 T U V W X Y Z A B C D E F G H I K L M NO P Q R S T U V W X Y Z A B C D E F G H I I I I I I I I I I I I I I I I I I

12 MO AND 18 MO.

-							
1	1 A	301	26	2 A	601	51	3 A
5	1* A2	305	26*	2 A 2	605	51*	3 A2
13	2 B	313	$\frac{27}{27*}$	2 B	613	52	3 B
17	$\overline{2}* \widetilde{\mathbf{B}^2}$	317	27*	2 R2	617	59*	3 D2
$\overline{25}$	3 C	325	90	20	625	52	9 D*
20	3* C2	920	004	0.02	020	93	3 U
29 37	9" U"	329 337	28 28* 29	40"	629	53*	3 B ² 3 C 3 C ² 3 D 3 D ²
37	4 D	337	29	ZD.	637	54	3 D
41	4* D2	341	29*	$2 D^2$	641	54*	$3 D_3$
49	5 E	349	30	$2~\mathrm{E}$	649	55	3 E
$\bar{53}$	5* E ²	353	30*	$2 E^2$	653	55*	$3 E^2$
61	6 F	361	31	$2 \mathrm{F}$	661	56	3 F
65	6* F ²	365	31*	2 F2	665	56*	3 143
73 77	2* B ² 3* C C C C C C C C C C C C C C C C C C	373	32 32*	2 G	673	52 52* 53* 53* 54* 55* 55* 56* 56* 57*	3 E 3 E ² 3 F 3 G 3 G ²
77	7* (+2	377	32*	2 G2	677	57*	3 (12
85	8 H 8* H ²	385	33	2 H	685	58	8 11
89	Q* 112	389	33*	9 112	689	50*	9 112
97	9 T	397	34	9 I	697	50	9 1
101	9 I	401	34*	0.12	701	59	0.12
101	30 17	401	34*	212	701	99*	21.
109	9 I 9* I ² 10 K 10* K ²	409	35	ZK	709	60	3 K
113	10* K2	413	35*	$2 K^2$	713	60*	3 K2
121	11 L	421	36	2 L	721	61	3 L
125	9* 12 10 K 10* K ² 11 L 11* L ² 12 M 12* M ²	425	36*	$2 L^2$	725 733 737	61*	3 H 3 H ² 3 I I 3 K S 3 K S 3 L 3 L ² 3 M
133	12 M	433	37	2 M	733	62	3 M
137	12* M ²	437	37*	2 M ²	737	62*	3 M2
145	13 N	445	38	2 N	745	- 63	3 N
149	12* M² 13 N 13* N² 14 O 14* O² 15 P 16* Q² 17 R 17* R 17* R 18 S 18* S²	449	37 37* 38 38*	2 N2	749	58 58 59 59 60 61 61 62 63 63 64 65 66 67 67 68 69 70 70	3 N2
157	14 0	457	39 39*	20	757	64	3 0
161	14* Ŏ2	461	30*	2 02	761	64*	3 03
160	15 P	160	40	5 D	769	65	9 D
169 173	15* D2	469 473	40*	9 D2	773	65*	9 TD#
181	16. 0	401	41	2 5	781	00.	9 1
185	10 0	481 485	41*	4 0	785	00	5 Q
180	10 V Q2	480	417	Z Q*	780	00*	3 Q ²
193	17 R	493	$\frac{42}{42*}$	Z K	793	67	3 R
197	17* R2	497	42*	$2 R^2$	797	67*	3 R2
205	18 S	505	43 43*	$2 \mathrm{S}$	805	68	3 S
209	18* S ²	509	43*	$2 S^2$	809	68*	$3 S^2$
217	19 T 19* T ² 20 U	517	44 44*	$2 \mathrm{~T}$	817	69	3 T
221	19* T ²	521 529	44*	$2 T^2$	821	69*	3 T2
229	20 U	529	45	2 U	829	70	3 U
229 233 241	20* II2	533	45 45*	2 112	809 817 821 829 833	70*	3 112
241	- 21 V	541	46	$\bar{2}\bar{\mathbf{v}}$	841	71	3 V
$\overline{245}$	21 V 21* V2	545	46*	$\overline{2}$ \mathbf{V}^2	845	71*	3 V2
$\tilde{2}\tilde{5}\tilde{3}$	59 W	553	17	5 W	853	79	3 W
257	22 W 22* W	557	46* 47 47*	2 11/2	857	79*	2 W/2
265	98 A	565	48	2 V	865	71* 72 72* 73 73* 74	9 M Y 2
269	23 X 23* X ²	569	48*	2 X 2		79*	9 V2
	40° X²	509	45*	O W	869 877	75"	0 A
277	24 Y 24* Y ²	577	49	2 Y	877	74	0 X
281	24* Y2	581	49*	ZY²	881	74*	3 Y2
289	21 V 21* V ² 22 W 22* W ² 23 X 23* X ² 24 Y 24* Y ² 25 Z 25* Z ²	589	50	AABBCC°DDEEFFGGHHII'KKLL'MMNNOOPPQQRRSSTTUUVVVWWXXYYZZ	889	75 75*	AABBCCODDEEFFGGHII'KKLLIMMNNOOPPQGRRSSTTUUVVWWXXYYZZ
293	25* Z ²	593	50*	2 Z2	893	75*	3 Zz

16MO AND 24MO.

	16	MO		MO.			
16	MO.		24 1	ИO.			
		9	1 A	401		$\frac{\mathbf{R}^2}{\mathbf{S}}$	
17	1 A 2 B 3 C 4 D 5 E 6 F 7 G	9	1*	409	18 18*	·S	
33	3 C	17	A2	417	18*	~	
49	4 D	-25	2 B	425	10	S^{2}	
65	5 E	33	2 B	433	19	T	
00	0 5	41	B2	441	19*	1	
81 97 113	6 F 7 G	41	B-	441	19*	mx	
97	7 6	49	3 C	449	-	$\mathbf{U}^{\mathbf{z}}$	
113	8 H I	57	3*	457	20	U	
129	9 I	65	C ²	465	20*		
145	10 K	73	4 D	473		U^{2}	
161	11 L	81	4*	481	$-rac{21}{21}*$	V	
177 193	12 M	89	D^2	489	21*		
193	13 N	97	5 E	497		VZ	
209	14 0	105	5 E 5*	505	22	w	-
225	15 - P	113	E ²	513	$\frac{22}{22*}$	**	
241	15 P 16 Q	121	6 F	521	44.	W₹	
	16 Q 17 R	129	6*	529	90		
257	17 K	129		529	23 23*	X	
273	18 S 19 T	137	_ F2	537	23*		
289	19 T	145	7 G	545		XZ	
305	$\tilde{20}$ $\tilde{\mathbf{U}}$	153	7*	553	24	Y	
321	20 U 21 V	161	G2	561	24*		
337	22 W	169	8 H	569 577		\mathbf{Z}^{2}	
353	23 X	177	8*	577	25	7.	
369	23 X 24 Y	185	H ²	585	25 25*		
385	24 Y 25 Z	185 193	9 I	593	20	$\mathbf{Z}_{\mathbf{\bar{2}}}$	
401	26 2 A	201	9 I 9*	601	26	2 A	
417	26 2 A 27 2 B	209	I2	609	26*	a A	
433	28 2 C	217	10 K	617	40"	0 40	
440	40 4 U		10 K		0=	2 A ² 2 B	
449	29 2 D 30 2 E	225		625	27 27*	2 B	
465 481	30 Z E	233	K ²	633 641	27*	_	
481	31 2 F	241	11 L	641		2 B ²	
497	32 2 G	249	11*	649	28 28*	$2\overline{ extbf{c}}$	
513 529	33 2 H	257	L^2	657	28*		
529	34 2 I	265	12 M	665		2 C2	
545 561	35 2 K	273	12 M 12*	665 673	29	2 D	
561	36 2 L	281	M2	681	29 29*		
577 593 609 625 641	37 2 M	289	13 N	689	40	$2 D^2$	
502	38 2 N	297	13 N 13*	689 697	30	2 E	
600	39 2 0	305	N^2	705	30*	4 E	
009	40 2 P		14 0	700	50°	0.770	
020	40 4 P	313	14 0	713		2 E ² 2 F	
041	41 2 Q	321	14*	721	31 31*	2 F	
00.4	42 2 R	329	O2	729	31*		
673	43 2 S	337	15 P 15*	729 737		2 F ²	
689 705 721	26 2 A B C 27 A B C 27 A B C 28 A B C 2	345	15*,	745	32	2 G	
705	45 2 U	353	P^{2}	753	32*		
721	46 2 V	361	16 Q	761		2 G2	
737	47 2 W	369	16 Q 16*	769	33	$\tilde{2}\tilde{\mathrm{H}}$	
753	47 2 W 48 2 X	377	OF	777	-33 33*	- 11	
769	46 2 V 47 2 W 48 2 X 49 2 Y 50 2 Z	385	17 R	785	90.	2 H ²	
785	50 2 Z	393	17*	793	34	2 I	
100	00 4 L	1 000	11.	1 130	16	41	

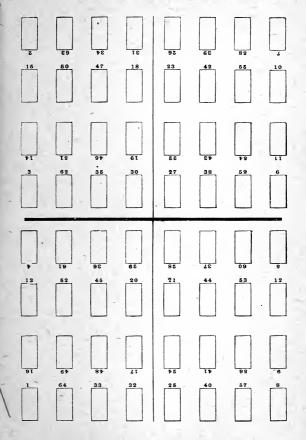
IMPOSITION OF FORMS.

A HALF-SHEET OF SEVENTY-TWCS, WITH THREE SIGNATURES. 4 51 28 38 33 42

POCKET COMPANION.

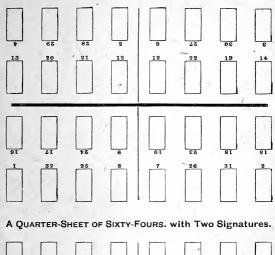
121

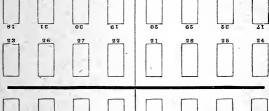
A HALF-SHEET of SIXTY-FOURS.

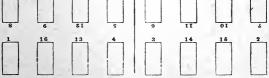


IIII I DIDOMITICALI,							
A HALF-SHEET of FORTY-EIGHTS, with Two Signatures.							
				*			
2	23	22	3	50	4.9	9#	22
7	18	19	6	31	42	43	30
		. '					
11	14	15	.10	35	38	39	34
	-					-	-
13	13	91	9				33
13	81	91	9	98	37	01	88
8	21	20	9	35	TF	**	62
1	24	21	4	25	48	45	28
							-
	L						`
A HALF-SHEET of TWENTY-FOURS, without Cutting.							
В	20	17	8	7	18	19	6
						Ш.	
-	12	91	6	OI	91	22	3
1	24	13	12	11	14	23	2
				2			
			_				-

A COMMON QUARTER-SHEET of SIXTY-FOURS,



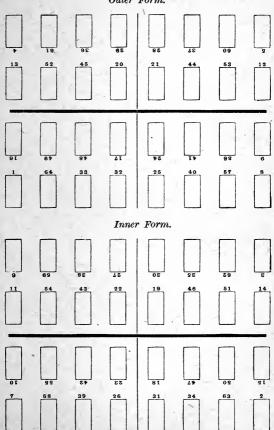




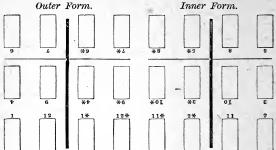
124 HANDI MECHANICAL,							
A HALF-SHEET of FORTY-EIGHTS, with Three Signatures.							
				- \			
34	47	97	38	36	46	81	33
39	42	43	38	37	44	41	40
ī							
						-	
81	1 5	30	61	02	62	35	41
23	26	27	22	21	28	25	24
	-						
8	6	13	9	9	II	01	1
	16	13		3	14	15	Ť
A HALF-SHEET of TWENTY-FOURS, without Inset.							
81	23	2.2	61	20	2.1	78	11
		_			-		
8	6	21	9	9	TT	01	
1	16	13	4	3	14	15	2
	ΓŤ						
						1.	

A SHEET of THIRTY-TWOS.

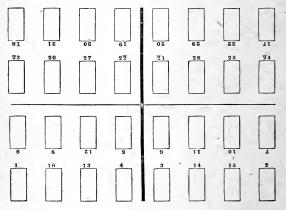
Outer Form.



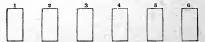
Two Half-Sheets of Twelves Worked Together.



A HALF-SHEET of THIRTY-Twos with Two Signatures.



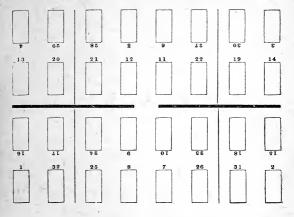
Six Page Leaflet. First Page to the Left.



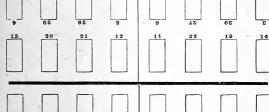
A SHEET OF SIXTEENS, With one Signature.

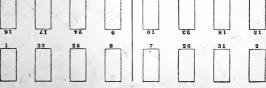
Outer Form.

Inner Form.

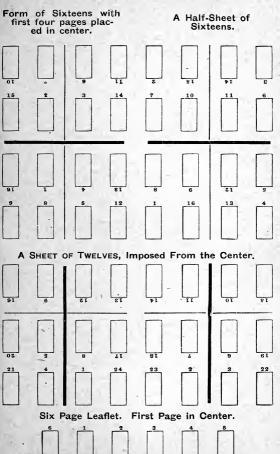


A HALF-SHEET of THIRTY-TWOS.





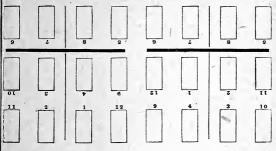
128 A HALF-SHEET of TWENTY-FOURS. A HALF-SHEET OF FORTIES. Six Page Leaflet. First Page to the Right.



9 .

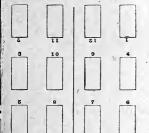
Out	er Form of Tw	of a S velves.	Sheet	Inner	Form of Tw	of a Shelves.	eet
21	ετ	Į.	6	ot	31	14	TT
8	21	20	3	9	61	8t	4
1	24	21		3	22	23	2
	L '						
	A SHEET OF TWENTIES.						
	Outer 1	Form.			Inner .	Form.	
02	IZ	84	21	st .	£3	22	61
5	36	33	8	7	34	35	6
I g	93	82	13			92	st
9	32	29	12	11	30	31	10
	40	37	4	3	38	39	2

Different Method of Imposing Half-Sheets of Twelves, from the Center.

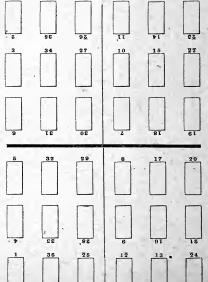


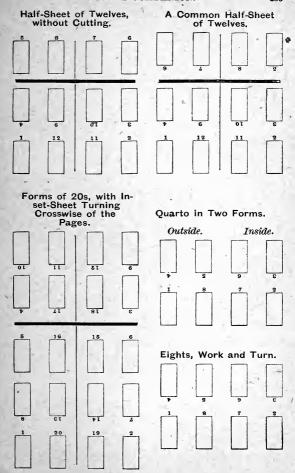
A Half-Sheet of Twenties, with Two Signatures.





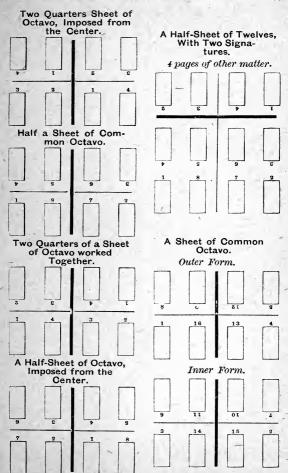
	Inner	With Two Signatures. Inner Form.			
02 13 20	1 81 82	22 61			
8 6 51		01			
1 16 13	3 14	15 2			
A HALF-SHEET OF TH	IRTY-Sixes, Without	ut Cutting.			





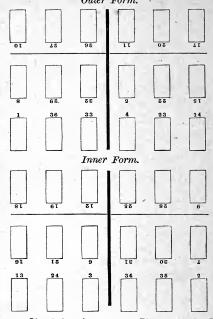
HANDY MECHANICAL,

A SHEET OF TWELVES Without Cutting. Outer Form. Inner Form. A HALF-SHEET OF THIRTY-SIXES. ₹8



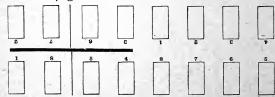
A SHEET OF EIGHTEENS, with One Signature.

Outer Form.

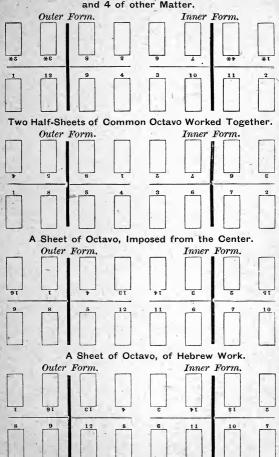


OCTAVO.—Sheet turning lengthwise of the pages.

Eight page leaflet. First page to the left.

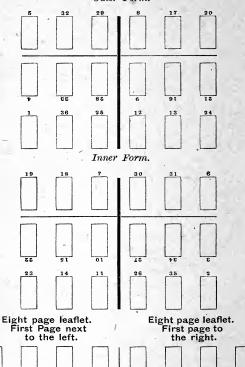


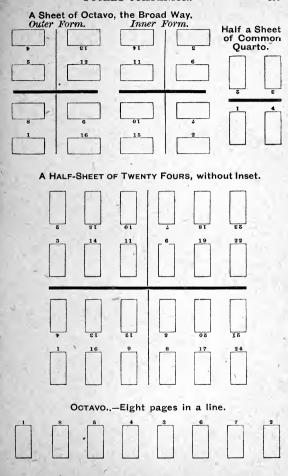
A Sheet of Octavo, 12 of the Work and 4 of other Matter.



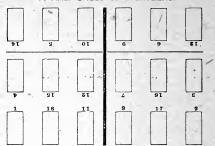
A SHEET OF EIGHTEENS to be Folded Together.

Outer Form.



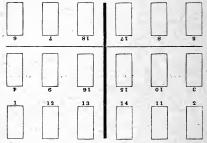


A HALF-SHEET OF EIGHTEENS.



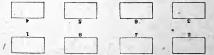
When the paper is worked off, transpose the pages 11 and 8 in the place of 7 and 12, and pages 7 and 12 in place of 11 and 8.

A Half-Sheet of Eighteens, without Transposition.



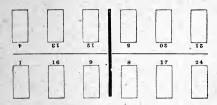
This form of imposition will give three single leaves when the sheet is cut, and should therefore be avoided where possible.

Broad Eights, in Two Forms. Outside. Inside.

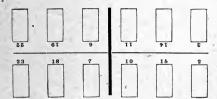


A SHEET OF LONG TWELVES.

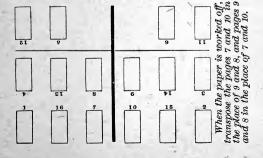
Outer Form.



Inner Form.



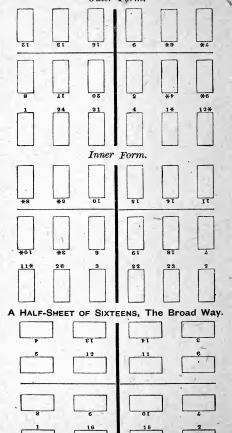
A HALF-SHEET OF EIGHTEENS, (Containing 16 pages).



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A SHEET OF EIGHTEENS, with Two Signatures.

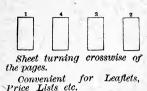
Outer Form.



QUARTO.
Sheet turning lengthwise of the page.



QUARTO.



AMERICAN AND GERMAN TYPE.

ij oţ GERMAN NAME. AMERICAN NAME. ES. 811 855 1 1/2 petit American 1/8 cicero German 14 541 570 1/4 petit Saxon 2 405 427 $\tilde{3}$ Brilliant 270 285 14 cicero 4 203 202 Diamant Diamond 56 Perl 162 160 Agate Nonpareille Nonpariel 135 143 115 7 Colonel Brevier 113 101 8 Petit Bourgeois 101 Borgis 9 90 90 Long-primer Garmond Small-pica 10 81 80 Cicero Pica 12 68 71 58 Mittel English 14 57 Tertia 51 Great-primer 16 50 Doppelborgis Paragon 18 45 45 Double S. pica Text 20 41 40 Double pica Doppelcicero 34 36 28 29 Doppelmittel Columbian Kleine canon Gr't Primer 32 $\frac{23}{20}$ Canon or dreicicero Paragon 36 20 Grobe canon 40 Meridian $\bar{4}2$ 19 19 31/2 cicero 3 line Columbian Kleine missal or viercicero 48 17 18 Canon 41/2 cicero 3 line Paragon 54 15 15 "S. pica $\bar{1}\bar{3}$ Grosse missal 60 14 " Paragon Kleine sabon 72 11 11

DECIMAL APPROXIMATIONS FOR FACILI-TATING CALCULATIONS.

Avoirdupo	is pounds	multipl	ied by	.009	equals	Cwts.	
44	- 44		4.4	.3045	-66	Tons.	
Lineal fee	t	+ 4	44	.00019	44	Miles.	
" yaı		44		.000568	44		
Square In	ches.	• 6		.007	"Squ	are feet.	
	et.	**	44	.111	- "	" Yds.	
	rds.	6.6	- 16	.000206	7 ''	" Acres	
Circular I	nches	4.6		.00546	66	" Feet.	
Cylindrica		44		.0004546		ubic "	
**	Feet	66		.02909	66	" yds.	
Cubic Incl	nes	"		.00058	66	" Feet.	
" Feet	ī	4.6		.03704	66	" Yds.	
"		66		.6232		per'l g'ls.	
" Incl		***		003607	- 66	" "	
Cylindrica		* *	4.8	395	66	" "	
"	Inches	44		002832			
Cubic	66	6.6	66 9	263		os. Avoir.	
					(0	ast-Iron.	
44	66	44		81	" W:	r'gt Iron.	
	**	**		83	"	Steel.	
44	44	66		225	"	Copper.	
46	"	44		037	"	Brass.	
66		44	".2		"	Zinc.	
**	**		. 1	103	• • • • • • • • • • • • • • • • • • • •	Lead.	
**	"			636		Tin.	
66		**		908		Mercury.	
Cylindrica				065	- (ast-Iron.	
- "	- 1 46	44		168	W	r'gt Iron.	
		- "	.4	223	**	Steel.	
44	- 66		.4	533	"	Copper.	
		٧.		385	"	Brass.	
.,		"	4	042	66	Zinc.	
- 44		"		223	46	Lead.	
- 66	"		• 4	07	"	Tin.	
				854		Mercury.	
Diameter	ora ç mu	ltiplied		416		Circum.	
66	166			8862	510	le of=sq.	
- 11		66				scribed".	
46	Sphere		.0	UU		f = Cube.	
				667 " L	ength of	f=cyl'der	
Square of	f a Girolo		7854	• 6		a Circle.	
Circum. o		66	.31831			Diameter.	
Side of a		66	1.128		mam of	= Circle.	
Sq. Root of			1.1283	70		Square.	
Sq. of the		**	9 1410	66	Conve	e arrefo ac	
Cube. d	a sphere.	66 .	3.1416	66	Convex	surface.	
	o. do. rcular inc		.5236	66	1 000	Solidity.	
100.010 (1	iculai ilic	nes			r adi	nare foot.	

2.200 Cylindrical inches	•	equals :	Cubic foot.
Acres	\times .4840	" Sc	quare yards.
Links	.44	4.4	Yards.
_"	.66	66	Feet.
Feet	" 1.5 -	4.6	Links.
Width in chains	0.	" Acı	es per Mile.
Cubic feet	1.45		. S. gallons.
" Inches	.004348	, (J. S. "
Cylindrical feet.	0.014	(J. S. ''
" Inches	.0034	"	J. D.
U. S. gallons	.13367		Cubic feet.
U. S. gallons Cubic feet	" 231. " 8036	- 0	bic Inches.
" Inches	" .000466	U.	S. Bushels.
U. S. Bushels	" .0495	υ.	S. Bushels.
U. S. "	" 1.2446	44	Cubic yards.
Ŭ. S. "	"2150.42	44	" feet. " inches.
Cylindrical feet of water	:" 6.	44 T	. S. gallons.
Cubic feet of water.	" 62.5		avoirdupois.
· " inches	" .03617	"	avoiruupois.
Cylindrical feet.	" 49.11	"	
" inches.	.02842	66 66	66
13.44 U. S. gal.	101011	66	1 Cwt.
268.8 U. S. "		66	1 Ton.
1.8 Cubic feet.	-	"	1 Cwt.
35.88 " "		"	1 Ton.
Square Inches	" 1.273	" Circ	ular Inches.
STEAM	AND W		
Pounds of water, at 62°	F. × 0.01608	7 equal	Cubic feet.
1 11 11 11 11 11	0.1199	· cquai	Gallons.
66 66 66	" 1.2	" In	perial gals.
Tons o" ·"	** 35.90	"	Cubic feet.
Gallons per second X		qual Cu. fe	et per hour.
Gallons per minute "	7.9	***	6 76 6
Cu. feet per second "	2,222	"Cu. yds.	per minute.
	133.333		" hour.
Cu. feet per minute "	2.222		66 66
Feet of water at 52.3°	$\mathbf{F.} imes 0.8823$ (equals inc	hes of mer-
cury at 32° F.			
Atmospheres \times 14.7	06 equals po		quare inch.
" 2105.6			quare foot.
· · · · · · · · 8.5			square yard.
49.9	44		of mercury.
" 33.9	5 '' Te	eet of water	er at 52.3° F.
TO CONVE		IGHT OF	
TO CONVER Wrought-Iron into Cas		EIGHT OF multiplied	
	t-Iron	multiplied	by 0.928 1.014
Wrought-Iron into Cas Stee Zinc	t-Iron el. c.	multiplied	by 0.928 1.014 0.918
Wrought-Iron into Cas Stee Zinc Bra	t-Iron el. e. ss.	multiplied	by 0.928 '' 1.014 '' 0.918 '' 1.082
Wrought-Iron into Cas Stee Zinc Bra	t-Iron el. c. ss. per.	multiplied	by 0.928 1.014 0.918

-	9167	9193	9219	9245	9271	9297	.9323	.9349	9375	.9401	.9427	.9453	.9479	9202	.9531	.9557	.9583	6096	.9635	1996	8896	9714	9740	9926	9792	.9818
INCH.	.8333	8359	.8385	.8411	.8438	.8464	.8490	.8516	.8542	.8568	8594	.8620	.8646	.8672	8698	.8724	.8750	9278.	.8802	.8828	.8854	0888	9068	8932	8958	8984
AN IN	7500	.7526	.7552	.7578	.7604	.7630	.7656	.7682	.7708	.7734	.7760	.7786	.7813	.7839	.7865	.7891	.7917	.7943	6962	.7995	.8021	8047	8073	6608	.8125	1918.
1-32 OF	1.0999	6699	.6719	.6745	.6771	.6797	.6823	.6849	.6875	1069	.6927	.6953	6269.	.7005	.7031	.7057	.7083	.7109	.7135	.7161	.7188	.7214	.7240	.7266	.7292	.7318
EACH 7	5833	.5859	.5885	.5911	.5938	.5964	.5990	9109.	.6042	8909	.6094	.6120	.6146	.6172	.6198	.6224	.6250	.6276	.6302	.6328	.6354	.6380	.6406	.6432	.6458	.6484
T FOR	2000	9709	.5052	.5078	5104	.5130	.5156	.5182	.5208	5234	.5260	.5286	.5313	.5339	.5365	.5391	.5417	.5443	.5469	.5495	.5521	.5547	.5573	5599	.5625	.5651
A FOOT	.4167	.4193	.4219	.4245	.4271	.4297	4323	.4349	.4375	.4401	.4427	.4453	.4479	4505	.4531	.4557	.4583	.4609	.4635	.4661	.4688	4714	.4740	.4766	.4792	.4818
STS OF	.3333	3329	.3385	.3411	.3438	.3464	.3490	.3516	.3542	3568	.3594	.3620	.3646	.3672	3698	.3724	.3750	.3776	.3802	.3828	.3854	3880	3906	.3932	3958	.3984
_	.2500	.2526	.2552	.2578	7907	.2630	.2656	7897	.2708	.2734	.2760	.2786	.2813	.2839	.2865	.2891	.2917	.2943	.2969	.2995	3021	.3047	.3073	.3099	.3125	.3151
DECIMA	.1667	.1693	.1719	.1745	.1772	.1797	.1823	.1849	.1875	1901	.1927	.1953	.1979	2002	.2031	.2057	.2083	.2109	.2135	.2161	.2188	.2214	.2240	.2266	.2592	.2318
E OF	.0833	.0859	.0885	.0911	.0938	.0964	0660	1016	.1042	.1068	.1094	.1120	.1146	.1172	.1198	.1224	1720	.1276	.1302	.1328	.1354	1380	.1406	.1432	.1458	.1484
TABLE	0000	.0026	.0052	.0078	.0104	.0130	.0156	.0182	.0208	.0234	0970	.0286	.0313	.0339	.0365	.0391	.0417	.0443	.0469	.0495	.0521	.0547	.0573	.0599	.0625	1090.
Inch		1-32	1-16	3-37	1/8	5-37	3-16	7-32	1/4	9-32	5-16	11-32	×	13-32	7-16	15-32	1/2	17-32	9-16	19-32	2%	21-32	11-16	23-37	34	25-32

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(Continued	
ŏ	
7.	
INCI	
1N 1	
OF,	
TABLE OF DECIMAL PARTS OF A FOOT FOR EACH 1-32 OF AN INCH.	
CH	
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PA	
CAL	
SOIL	
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E O	
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T	

Continued).	0 . 11		89		Decimals of an Inch.	75 765625 78125 78125 88125 8825 88375 88375 89625 99025 99187 977 9875 9871 9871 9871 983125 983125
	9 10	•	.8255 .9089 .8281 .9115 .8307 .9141	an INCH.	Fractions of an Inch.	25,28 25,28 25,28 25,28 25,28 25,28 25,28 25,28 25,28 25,28 31,28 31,28 31,28 31,28
1-32 OF AN INCH	&	.7344 .7370 .7396	7422	64ths of	Decimals of an Inch.	15 15 15 15 15 15 15 16 16 16 16 16 16 16 16 16 16 16 16 16
1-32 O	4	.6510 .6536 .6563		and		
EACH	9	.5677 .5703	.5755 .5781 .5807	hs, 32ds,	Fractions of an Inch.	21.35 17
I FUIE	9	.4844 .4870 .4896	4922 4948 4974	hs, 16ths,		
DECIMAL PARTS OF A FOOT FOR EACH	4	.4010 .4036 .4063	.4089 .4115 .4141	S of 8ths,	Decimals of an Inch.	25.25625 286525 28125 28125 3126 323125 34375 375 375 390625 400625 400626 4315 48315 483125
ינוא חו	3	.3203 .3203 .3229	.3255 .3281 .3367	EQUIVALENTS		
AL FA	7	2344 2370 2396	2448 2474 2474	EQUIV	Fractions of an Inch.	25-64 25-64
DECLM	1	.1510 .1536 .1563	.1589 .1615 .1641	DECIMAL	Decimals of an inch.	015625 03125 046875 046875 0625 1078125 11406275 1140625 1171875 1171875 1171875 1171875 1171875 1171875 1171875 1171875 1171875
TABLE OF	0	.0570 .0708	.0755 .0781 .0807	DE	Dec of ar	
TABL	Inch.	13-16 27-32 7%	29-32 15-16 31-32		Fract- ions of an Inch.	49-1-1-2-2-2-1-2-2-2-2-2-2-2-2-2-2-2-2-2-

DECIMAL PARTS OF A POUND (16 oz) REDUCED TO THEIR VALUE IN OUNCES.

Oun-	100th Parts.	Ounces.	100th Parts	Ounces	100th Parts	Ounces	100th. Parts
16 151/2 15 141/2 14 131/2 13 121/2	1.00 .96 .94 .90 .87 .84 .81	111/ ₂ 111/ ₂ 11 101/ ₂ 10 91/ ₂ 9 81/ ₃	.75 .72 .69 .65 .62 .59 .56	8 71/2 7 61/2 6 51/2 5 41/2	.50 .46 .43 .40 .37 .34 .31	4 31/2 3 21/2 2 11/2 1	.25 .22 .19 .15 .12 .09 .06

Equivalents of Carats in Decimal parts, unity being Twenty-Four Carats.

Carats.	Decimals.	Carats.	Decimals.	Carats.	Decimals
1	0.042	9	0.375	17	0.707
2	0.033	10	0.417	18	0.750
3	0.125	11	0.459	19	0.792
4	0.167	12	0.500	20	0.833
5	0.208	13	0.542	21	0.875
6	0.250	14	0.583	22	0.917
7	0.292	15	0.625	23	0.958
8	0.333	16	0.666	24	1.000

DECIMAL EQUIVALENTS TO FRACTIONAL PARTS OF LINEAL MEASURES.

One Inch	the Integer	or whole Number.	
Inch. Dec.	Inch.	Dec. Inch.	Dec.
$\begin{array}{c} 78 + 3-32 = .96875 \\ 78 & 1-16 & .9375 \\ 78 & 1-32 & .90625 \\ 78 & .875 \\ 34 & .875 \\ 34 & .16 & .8125 \\ 34 & .16 & .8125 \\ 34 & .132 & .78125 \\ 34 & .75 \\ 58 & .3-32 & .71875 \\ 58 & .1-16 & .6875 \\ \end{array}$	1/2 " 1-16 " 1/2 " 1-32 " 1/2 " 1-32 " 3/8 " 3-32 " 3/8 " 1-16 3/8 " 1-32 "	.040 14 1-1	6 " .3125 2 " .28124 " .25 2 " .21875 6 " .1875 2 " .15625 " .125 2 " .09375

ONE FOOT OF 12 INCHES.

Inch. De	ec. Inch. Dec.	Inch. Dec.	Inch. Dec.
11 = .91 10 " .63 9 " .75 8 " .66 7 " .58	38 5 " .4166 4 " .3333	$\begin{array}{c} 1 = .0833 \\ 7_8 \text{ " .07291} \\ 34 \text{ " .0625} \\ 56 \text{ " .05208} \\ 1/2 \text{ " .04166} \end{array}$	3/8 = .03125 1/4 " .02083 1/8 " .01041

SAW-LOGS REDUCED TO INCH BOARD MEASURE.

		· · · · · · · · · · · · · · · · · · ·	
Length in Feet.		DIAMETER IN INCHES.	1000
H.	12 13 1	14 15 16 17 18 19 20 21 22 23 24 2	5 26
10 11 12 13 14 15 16 17 18 19 20 21	49 61 7 54 67 7 59 73 8 64 79 8 69 85 10 74 91 10 79 97 11 84 103 12 89 109 12 93 116 18 98 122 14 103 128 15	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	87 313 15 344 44 375 73 408 01 439 80 469 59 500 87 531 16 562 45 594 73 625 03 656
-	108 134 15 113 140 16 118 146 17 123 152 17		59 719 88 750
Length in Feet	07 1 00 1 0	DIAMETER IN INCHES.	1 90
HH	27 28 2		38
10 11 12 13 14 15 16 17 18	342 363 38 377 400 41 411 436 45 445 473 49 479 509 53 514 545 57 548 582 60 582 618 64	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	669 734 801 868 934 1001 1068 1134

To find the amount of lumber any log will make—First, find the length of the log in the first or left-hand column; then, on the top of the page, to the right, find the diameter and under the same will be found the quantity of lumber your log will make; calculated for any length from 10 to 25 feet, and for any diameter from 12 to 38 inches.

Table to Facilitate the Mensuration of Timber, Flat or Board Measure

			. O. Dou	i di mica.	sui c.		
Brea- dth in Ins.	Area of a lin.ft.	Breadth in Ins.		Breadth in Ins.	Area of a lin.ft.	Breadth in Ins.	Area of a lin.ft.
1/4 1/2 3/4 1 11/4 11/2 13/4 2 1/2 21/4 21/2 23/4	.0208 .0417 .0625 .0834 .1042 .1250 .1459 .1667 .1875 .2084	31/2 31/2 33/4 41/4 41/2 43/4 51/2 53/4	.2708 .2916 .3125 .3334 .3542 .3750 .3958 .4167 .4375 .4583 .4792	61/4 61/2 63/4 71/4 71/2 73/4 8 81/4 81/2 83/4	.5208 .5416 .5625 .5833 .6042 .6250 .6458 .6667 .6875 .7084	914 91/2 93/4 10 101/4 101/2 103/4 11 111/4 111/2 113/4	.7708 .7917 .8125 .8334 .8542 .8750 .8959 .9167 .9375 .9583 .9792
3	.2500	6	.5000	9	.7500		

RULE.--Multiply the length by the number in the table

corresponding to any given number.

EXAMPLE.—Given a board 161/2 feet in length and 934 inches in breadth.

The number in the table opposite 934 inches = .8125 \times 16½ = 13.4 square feet.

Contents (Board Measure) of I lineal foot of Timber.

		-				- / -						_
Br'th in Ins				TH	ICI	KNES	SIN	INCI	IES.			
HH	2	3	4	5	6	7	8	9	10	11	12	13
18	3.	4.5	6.	7.5	9.	10.5	12.	13. 5	15.	16. 5		
17	2.83			7.08			11.32			15.58		
16	2.67			6.67		9.33	10.67	12.	13.33	14.67	16.	17.33
15		3.75		6.25	7.5		10.00					
14	2.33	3.5	4.67	5.83		8.17		10.5	11.67	12.83	14.	15.17
13		3.25	4.33					9.75		11.92		14.08
12	2.	3.	4.	5.	6.	7.	8.	9.	10.	11.	12.	
11	1.83			4.58		6.42	7.33			10.08		
10	1.67	2.5	3.33	4.17	5.	5.83	6.67	7.5	8.33	-		
9		2.25		3.75		5.25	6.	6.75				
8	1.33			3.33		4.67	5.33					
7	1.17	1.75		3.92		4.08			. "	1		
6	1.	1.5		2.50	3.							
5	.83	1.25	1.67	2.08								
1 4	.67		1.33									
3 2	.50	.75								. 1		
2	.33											2
								- 0			71	-

To ascertain the contents of a piece of timber. Find in the table the contents of one foot and multiply by the

length in feet of piece.

EXAMPLE:—What is the contents of a piece of timber 10×11 . 20 feet long? $9.17 \times 20 = 183.4$ feet. B. M.

TABLE TO FACILITATE THE MENSURATION OF

	- THE	SOLIDIT	Y OF TIL	MBER.	
1 qr girth in inches.	Feet.	1 qr girth in Inches.	Area in Feet,	1 qr girth in Inches.	Area in Feet.
6	.250	121/4	1.042	19	2.506
61/4	.272	121/2	1.085	191/2	2.640
61/2	.294	123/4	1.129	20	2.777
634	.317	13	1.174	201/2	2.917
7'1	.340	131/4	1.219	21	3.062
71/4	.364	131/2	1.265	211/2	3.209
71/2	.390	133/4	1.313	$\begin{array}{c c} 211/2 \\ 22 \end{array}$	3 362
73/4 8	.417	14	1.361	221/2	3.516
8	.444	141/4	1.410	23	3.673
81/4	.472	141/2	1.460	231/2	3.835
81/2	.501	1434	1.511	24	4.000
83/4	.531	15	1.562	241/2	4.168
9	.562	151/4	-1.615	1 25	4.340
91/4	.594	151/2	1.668	251/2	4.516
91/2	.626	15¾ 16	1.722	26	4.694
93/4	.659	16	1.777	261/2	4.876
10	.694	161/4	1.833	27	5.062
101/4	.730	161/2	1.890	271/2	5.252
101/2	.766	163/4	1.948	28	5.444
103/4	.803	17	2.006	281/2	5.640
11	.840	171/4	2.066	29	5.840
111/4	.878	171/2	2.126	291/2	6,044
111/2	.918	1734	2.187	30	6.250
113/4	.959	18	2.250		
12	1.000	181/2	2.376		

RULE:-Multiply the area corresponding to the quarter girth in inches by the length in feet.

EXAMPLE:—Given a piece of timber 20 feet long and 12 inches square.

The number opposite 12 inches = $1.000 \times 20 = 20$ Cubic feet.

The following table of scantling measure gives the number of feet in a scantling from 1 foot to 13 feet and from 2×2 to 11×12 .

EXAMPLE:—How many feet in a 5×6 scantling 10 feet long? First find 10 feet under the column marked "Length in Feet" and opposite the number under the column marked 5×6 will be found 25 feet, the number of feet, the scantling contains.

If your scantling is longer than that given in the table

take two lengths and add them together.

EXAMPLE:—How many feet in a 3×4 scantling 21 feet long? Opposite 10 feet and under 3×4 is 10 feet. Opposite 11 feet and under 3×4 is 11 feet. Then 10+11=21 feet, the number of feet the scantling contains.

HANDY MECHANICAL,

SCANTLING MEASURE.

Length in Feet.			,		_ 1	NC	н	ES.				
in Feet.	2	$\times 2$	2	$\times 3$	1 5	2×4		$\times 5$		$\times 6$		$\times 7$
1 2 3 4 5 6 7 8 9 10 11 12 13	ft. 0 0 1 1 2 2 3 3 4 4	in. 4 8 0 4 8 0 4 8 0	ft. 0 1 1 2 2 3 4 4 5 5 6	in. 6 0 6 0 6 0 6 0 6	ft. 0 1223445666788	in. 8 4 0 8 4 0 8 4	1 ft. 0 1 2 3 4 5 5 6 6 7 8 9	in. 10 8 6 4 2 0 10 8 6	ft. 1 2 3 4 5 6 7 8 9 10 11 12	in. 0 0 0 0 0 0	1 2 3 4 5 7 8 9	in. 2 4 6 8 10 0 2 4
10 11 12 13		$ \begin{array}{c} 0 \\ 4 \\ 8 \\ 0 \\ 4 \\ 2 \times 3 \end{array} $	6	$\begin{array}{c} 6 \\ 0 \\ 6 \\ 0 \\ 6 \\ \hline 2 \times 4 \end{array}$		$ \begin{array}{c} 0 \\ 8 \\ 4 \\ 0 \\ 8 \end{array} $ 2×5	10 10	0 10 2×6	13	0 0 0 0 0 2×7	10 11 12 14 15	0 2 4 6 8 10 0 2 2×8
1 1	0	Q	0	10	1 1					6	1 44	
1 2 3 4 5 6 7 8 9 10 11 12 13	1 1 2 3 3 4 5 5 6 6 7 8	3 11 6 2 9 5 0 8 3 11 6 2	1 2 3 4 5 5 6 7 8 9 10 10	10 8 6 4 2 0 10 8 6 4 2 0 10 8 6 4 2 0	1 2 3 4 5 6 7 8 9 10 11 12 13	1 1 1 2 3 3 4 4 5 5 6 6 6 7 ×5 5	1 2 3 5 6 7 8 10 11 12 13 15 16	3 6 9 0 3 6 9 0 3 6 9 0 3 6 9	1 2 4 5 7 8 10 11 13 14 16 17 19	6 11 5 10 4 9 3 8 2 7 1 6 0	1 3 5 6 8 10 11 13 15 16 18 20 21	8 4 0 8 4 0 8 4 0 8 4 0 8
1 1	0	9	·	0		$\frac{3}{\sqrt{3}}$		6				
1 2 3 4 5 6 7 8 9 10 11 12 13	123345667899	630963096309	1 3 4 5 6 7 8 9 10 11 12 13	000000000000000000000000000000000000000	1 2 3 5 6 7 8 10 11 12 13 15 16	3690369036903	1 3 4 6 7 9 10 12 13 15 16 18 19	0606060606	1 3 5 7 8 10 12 14 15 17 19 21 22	9630963096309	2 4 6 8 10 12 14 16 18 20 22 24 26	000000000000000000000000000000000000000

SCANTLING MEASURE.

Length in Feet.				13	N C	нЕ	s.		_		
n Feet.	4×4	4×		4>	<6	4>		4>	<8	4>	
1 2 3 4 5 6 7 8 9 10 11 12 13	5 6 8 9 10 12 13 14 16 16	1. ft. 1. 3 1. 6 1. 3 1. 6 1. 8 1. 1 1. 1	in. 84 0 8 4 0 8 4 0 8 4 0 8	ft. 2 4 6 8 10 12 14 16 18 20 22 24 26	in. 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	ft. 2 4 7 9 11 14 16 18 21 23 25 30	in. 4 8 0 4 8 0 4 8 0 4 8 0 4 8 0	ft. 2 5 8 10 13 16 18 21 24 26 29 32 34	in. 8 4 0 8 4 0 8 4 0 8	15 12 15 18 21 24 27 30 33 36 39	in 0
	5×5	5×	(6	5×		5×	(8	5 >	9		(10
1 2 3 4 5 6 7 8 9 10 11 12 13	8 10 12 14 16 18 20 1 22 1 25 27	$egin{array}{c c} 1 & 27 \\ 0 & 30 \\ 1 & 32 \\ \end{array}$	6 0 6 0 6 0 6 0 6 0 6 0 6	2 5 8 11 14 17 20 23 26 29 32 35 37		40 43	48 04 80 48 04 80 4	3 7 11 15 18 22 26 30 33 37 41 45 48	9 6 3 0 9 6 3 0 9 6 3 0 9	8 12 16 20 25 29 33 37 41 45 50	2 4 10 0 2 4 6 8 10 0 0 2 10 0 0 0 0 0 0 0 0 0 0 0 0 0 0
	6×6	6×		6×4	$\frac{8}{0}$	6> 4	<9 6	$\frac{6\times}{5}$	$\frac{10}{0}$	6>	<11
1 2 3 4 5 6 7 8 9 10 11 12 13	6 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	7 10 114 117 117 117 119 121 122 128 131 135 135 138 142	6 0 6 0 6 0 6 0 6 0 6 0 6 0 6 0 6 0 6 0	8 12 16 20 24 28 32 36 40 44 48 52	000000000000000000000000000000000000000	9 13 18 22 27 31 36 40 45 49 54 58	6 0 6 0 6 0 6 0 6	10 15 20 25 30 35 40 45 50 55 60 65	000000000000000000000000000000000000000	11 16 22 27 33 38 44 49 55 60 66 71	60 60 60 60 60 60 60 60 60

HANDY MECHANICAL,

SCANTLING MEASURE.

Length in Feet.						N C		s.				
in Feet.	7>	<7	$ $ $7 \times$	(8	7>		7>	(10	, ,	<11		₹12
	ft.	in	ft.	in.	ft.	in.	ft.	in.	ft.	in.	ft.	in.
1 2 3 4 5 6 7 8 9	4	1	4	8	5	3	5	10	6	5	7	0
2	8	2	9	4	10	6	11	8	12	10	14	0
3	12	$\frac{2}{3}$	14	0	15	9	17	6	19	3	21	0
4	116	4	18	8	21	0	23	4	25	10 3 8	21 28	0
5	20	5	23	4	26	3	29	2	32	1	35	0
6	24	6	28	Õ	31	6	35	Õ	38	6	42	Õ
7	28	4 5 6 7	23 28 32	8	36	9	40	10	44	11	49	ŏ
Ř	$3\tilde{2}$	- 8	37	4	42	ŏ	46	- 8	51	11 4 9 2 7	56	ŏ
ğ	36	8 9	42	Ô	47	š	$\tilde{52}$	6	57	ĝ	63	ŏ
10	40	10	46	8	52	6	58	4	64	2	70	ŏ
11	44	11	46 51	4	52 57	ğ	64	. 2	70	7	77	ŏ
19	49	0	56	ō	63	ŏ	70	ő	77	~ 0	84	_ 0
12 13	53	ĭ	60		68	3	75		83	5	91	0
10		. 8			8×		1	(11	_	(12		×9
		<u> </u>	8>				<u> </u>					
1 2 3 4 5 6 7 8 9	5	4	16 12	0	6	8	7	4	18 16	0	6	9
2	10	8	12	0	13	4	14	8	16	.0	13	6
3	16	0	18	0	20	0	22	0	24	0	20 27	3
4	21	8	24	0	26	8 4 0	29	4	32	0	27	Ü
5	26	- 8	30	0	33	4	36	8	40	0	33	9 6 9 6 9 6 9 6 9 6
6	32	0	36	. 0	40	0	44	0	48	0	40	6
7	37	4	42	0	46	8	51	4	56	, 0	47	3
8	42	8	48	0	53	4	58	8	64	. 0	54	C
9	48	Ō	54	0	60	. 0	66	0	72	0	60	9
10	53	4	60	0	66	8	73	4	80	0	67	•
10 11	58	8	66	0	73	4	80	8	88	. 0	74	3
12	64	0	72	Õ	80	Õ	88	Ō	96	0	81	Ō
13	69	4	78	Õ	86	8	95	4	104	Ŏ	87	9
	9>	<10	9×	11		<12	10	$\times 10$		×11	10>	<12
1	17	6	8	3	18	(4	9 18	2	10	0
$\frac{2}{3}$	15	0	16	6	18	(16		18	4	20	0
3	22	6	24	9	27	(25	0	27	. 6	30	0
4	30	0	33	0	36	(4	36	8	40	0
5	37	6	41	3 6	45	(41	8	45	10	50	0
. 6	45	0	49	6	54	(0	55	0	60	0
7	52	6	57	9	63	(58	4	64	2	70	0
- 8	60	0	66	0	72	(8	73	4	80	0
5 6 7 8 9 10	67	6	74	3 6	81	- (75	Ó	82	6	90	0
10	75	ŏ	82	6	90	Č	83	4	91	8	100	Ŏ
11	82	- ĕ		· ğ	99	Č		8	100	10	110	Ŏ
12 13	90	ŏ		ŏ	108	Č		ŏ	110	0	120	ŏ
											130	

BOARD MEASURE, (I inch thick).

-	Ņ-		W	DTI		I I		s.			
4	1		5		j				8	1	9 .
ft. 0 0 1 1 1 2 2 3 3 4 4	in 480 480 480 448	ft. 00 1 1 2 2 2 3 3 4 4 5 5	5 10 3 8 1 6 11 4 9	0 1 1 2 2 3 3 4 4 5 5	in. 60 60 60 60 60 60 60 60 60 60 60 60 60	ft. 0 1 1 2 2 3 4 4 5 6 7	in. 7 2 9 4 111 6 1 8 3 10 5 0 7	ft. 0 122344566788	in. 8 4 4 0 8 4 4 0 8 4 4 0 8	ft 0 1 2 3 3 4 5 6 6 7 8 9 9	. in. 9 6 3 0 9 6 3 0 9 6 3 0 9
				15	2						15
$ {f 10} $	4 2 0 10	11 11	10 9 8 7 6 5 4 3 2 1 0 11	8 9 10 11 12 13		11 13 14	$\begin{array}{c} 11 \\ 0 \\ 1 \end{array}$	8 9 10 11 14 15	10 0 2 4 6 8 10 0 2	10 11 12 13 15 16	3 6 9 0 3 6 9 0 3 6 9 0 3 6 9
1											21
1 2 4 5 6 8 9 10 12 13 14 16 17	8 0 4 8 0 4 8 0 4 8 0 4	2 4 5 7 8 9 11 12 14 15 17 18	10 3 8 1 6 11 4 9 2 7 0 5	3 4 6 7 9 10 12 13 15 16 18 19	0 6 0 6 0 6 0 6 0 6	3 4 6 7 9 11 12 14 15 17 19 20	2 9 4 11 6 1 8 3 10 5	3 5 6 8 10 11 13 15 16 18 20	4	17 19 21	9630963096309
	ft. 0 0 1 1 2 2 2 3 3 3 4 4 4 5 5 6 6 7 7 8 9 10 10 10 12 13 4 15 14 16 16 16	0	ft. in ft. 0 4 0 1 1 1 4 1 1 2 8 2 2 4 3 3 4 4 4 0 5 5 10 6 8 8 7 8 4 9 10 8 11 2 0 12 12 12 12 12 12 12 12 12 12 12 12 12	4 5 5 10 6 10 11 1 10 10 11 11	4 5 6 6 6 10 11 12 12 10 10 11 12 10 10	4 5 6 6 6 6 6 6 6 6 6	4 5 6 ft. im ft. im. ft. im. ft. 0 4 0 5 0 6 0 1 0 1 3 1 6 1 1 0 1 3 1 6 1 1 4 1 8 2 0 2 6 3 0 3 9 2 4 2 11 3 6 4 4 3 4 4 0 4 3 4 4 2 5 0 6 6 7 4 4 5 5 6 6 7 6 6 6 7 4 4 5 5 6 6 7 7 6 6 6 7 10 11 12 1 1 1 1 1 1 <th< td=""><td>4 5 6 7 ft. im ft. im. ft.</td><td>4 5 6 7 I ft. im ft. im. ft. <th< td=""><td>4 5 6 7 8 ft. im ft. in. in. ft. in. in. in. <th< td=""><td>4 5 6 7 8 ft. im ft. in. ft. <th< td=""></th<></td></th<></td></th<></td></th<>	4 5 6 7 ft. im ft. im. ft.	4 5 6 7 I ft. im ft. im. ft. <th< td=""><td>4 5 6 7 8 ft. im ft. in. in. ft. in. in. in. <th< td=""><td>4 5 6 7 8 ft. im ft. in. ft. <th< td=""></th<></td></th<></td></th<>	4 5 6 7 8 ft. im ft. in. in. ft. in. in. in. <th< td=""><td>4 5 6 7 8 ft. im ft. in. ft. <th< td=""></th<></td></th<>	4 5 6 7 8 ft. im ft. in. ft. <th< td=""></th<>

NOTE:—The rule for this table is worked in the same manner as the rule for scantling measure, on page 151.

BOARD MEASURE, (2 inch thick).

Length			VIDTI		INC	HE	S.			
in Feet.	6	7	1 8		9		10	0	1	1
8 9 10 11 12 13 14 15 16 17 18	ft. 1r 8 9 10 11 12 13 14 15 16 17 18	1 ft. in 9 44 10 66 11 8 12 10 14 0 15 2 16 44 17 8 18 19 10 21 0	10 12 13 14 16 17 18 20 21 22	in. 8 0 4 8 0 4 8 0	ft. 12 13 15 16 18 19 21 22 24 25 27	in. 0 6 0 6 0 6 0 6 0 6	ft. 13 15 16 18 20 21 23 25 26 28 30	in. 4 0 8 4 0 8 4 0 8 4	ft. 14 16 18 20 22 23 25 27 29 31 33	in. 8 6 4 2 0 10 8 6 4 2 0 10
19 20	19 20	$\begin{vmatrix} 22 & 2 \\ 23 & 4 \end{vmatrix}$	$\begin{array}{c} 25 \\ 26 \end{array}$	4 8	28 30	6	31 33	8	34 36	10
	12	13	1		1	5	1	6 ;	1	7
8 9 10 11 12 13 14 15 16 17 18 19 20	16 18 20 22 24 26 28 30 32 34 36 38 40	19 6 21 8 22 10 26 28 3 32 34 8 36 10 39 41 43	28 2 30 42 35 35 37 39 42 44 46	8 0 4 8 0 4 8 0 4 8 0 4 8 0 4 8	20 22 25 27 30 32 35 37 40 42 45 47 50	0 6 0 6 0 6 0 6 0 6 0 6	21 24 26 29 32 34 37 40 42 45 48 50 53	4 0 8 4 0 8 4 0 8 4 0 8 4	22 25 28 31 34 36 39 42 45 48 51 53 56	1
	18	19		20	2		22			23
8 9 10 11 12 13 14 15 16 17 18 19 20	24 27 30 33 36 39 42 45 48 51 57 60	28 31 34 1 38 41 44 47 50 53 1 57 60	0 40 2 43 4 46 6 50 8 53	8048048048048	28 31 35 38 42 45 49 52 56 66 70	0 6 0 6 0 6 0 6 0 6 0 6 0 6	29 33 36 40 44 47 51 55 62 66 69 73	4 0 8 4 0 8 4 0 8 4 0 8 4	30 34 38 42 46 49 53 57 61 65 69 72 76	1

Note:—The rule for this table is worked in the same manner as the rule for scantling measure, on page 151.

CUBIC CONTENTS of SQUARE TIMBER.

Length in Feet.				HES.		
m reet.	6×6	6×7	6×8	6×9	6×10	6×11
10 11 12 13 14 15 16 17 18 19 20 21	ft. in 2 9 9 3 0 0 3 6 8 9 4 0 9 4 6 9 5 5 6	ft. in. 2 11 3 3 3 6 3 10 4 1 4 5 4 8 5 0 5 7 5 10 6 5 5	ft. in. 3 8 4 0 4 4 4 8 5 0 5 4 6 6 8 7 0 4	ft. in. 3 9 4 2 6 4 11 5 3 5 8 6 0 6 5 6 9 7 2 7 8 7 11 8 3	ft. in. 4	4 7 5 1 5 6 6 0 6 5 6 11 7 4 7 10 8 3 8 9 9 2 9 8 10 1
	1 7×7	7×8.	7×9	7×10	7×11	7×12
10 11 12 13 14 15 16 17 18 19 20 21 22	3 5 3 1 4 5 5 5 5 6 6 10 7 6	3		1 4 10 5 4 5 10 6 4 7 4 7 9 8 3 8 9 9 3 9 9 10 3 10 8	5 4 5 11 6 5 6 11 7 6 8 7 9 1 9 8 10 8 11 3 11 9	5 10 6 5 7 0 7 7 8 2 8 9 9 4 9 11 10 6 11 1 11 8 12 3 12 10
* 1	8×8	8×9	8×10	8×11	8×12	8×13
10 11 12 13 14 15 16 17 18 19 20 21 22	4 5 4 11 5 4 5 9 6 3 6 8 7 1 7 7 8 5 8 5 8 11 9 9	5 0 5 6 6 0 6 6 7 6 8 0 8 6 9 0 10 0 10 6 11 0	5 7 6 1 6 8 7 3 7 9 8 4 8 11 9 5 10 0 10 7 11 1 11 8 12 3	$ \begin{vmatrix} 6 & 1 \\ 6 & 9 \\ 7 & 4 \\ 7 & 11 \\ 8 & 7 \\ 9 & 2 \\ 9 & 9 \\ 10 & 5 \\ 11 & 0 \\ 111 & 7 \\ 112 & 3 \\ 12 & 10 \\ 13 & 5 \\ \end{vmatrix} $	6 8 7 4 8 0 8 8 8 9 4 10 0 10 8 11 4 12 0 12 8 13 4 14 0 14 8	7 3 7 11 8 8 9 5 10 1 10 10 11 7 12 3 13 0 13 9 14 5 15 2 15 11

Note:—The rule for this table is worked in the same manner as the rule for scantling measure, on page 151.

CUBIC CONTENTS of ROUND TIMBER.

Length in Feet.					MET			INCI				
m reet.	10)	1.	1	12	2		13		14	1	5
13 14 15 16 17 18 19 20 21 22	ft. 7 7 8 8 9 9 10	in 1 8 2 9 3 10 4 11	ft. 8 9 10 11 11 12 13 13	in. 7 3 11 7 3 11 7 2 10	ft. 10 11 11 12 13 14 14 15	in. 3 0 9 7 4 2 11 9 6	ft. 12 12 13 14 15 16 17	in. 0 11 10 9 8 7 6 5	ft. 13 15 16 17 18 19 20 21	in. 11 11 12 34 56 66 78	ft. 15 17 18 19 20 22 23 24	in 11 2 5 8 10 1 4
21 22 23 24 25	11 12 12 13 13	6 0 7 1 8	13 14 15 15 16	$\begin{array}{c} {\bf 6} \\ {\bf 2} \\ {\bf 10} \\ {\bf 6} \end{array}$	15 16 17 18 18 19	3 1 10 8	19	5 4 3 3 2 1	21 22 23 24 25 26	6 6 7 8 9	20 22 23 24 25 27 28 29 30	1 4 7 9 0 3 6 8
13 14 15 16 17 18 19 20 21 22 23 24 25	18 19 20 22 23 25 26 27 29 30 32 33 34	2 7 11 4 9 2 6 11 4 9 2 6 11	20 22 23 25 26 28 30 31 33 34 36 37 39	6 1 8 3 10 5 0 6 1 8 3 10 5 5	23 24 26 28 30 31 35 37 38 40 42 44	0 9 6 3 1 10 7 4 2 11 8 5	25 27 29 31 33 35 37 39 41 43 45 47	77 77 66 55 54 44 43 33	28 30 32 34 37 39 41 43 45 48 50 52 54	4 7 9 11 1 3 6 8 10 0 2 5 7	31 33 36 38 40 43 45 48 50 52 55 67	3 8 1 6 11 4 9 2 6 11 4 9 2 6
13 14 15 16 17 18 19 20 21 22 23 24 25	34 37 39 42 44 47 50 52 55 58 60 63 66	11 6 2 10 6 1 9 5 0	37 40 43 46 49 51 54 57 60 63 66 69 72	6 5 4 2 1 11 10 9 7 6 5 3 2	40 44 47 50 53 56 59 62 66 69 72 75 78	10 0 0 2 3 5 7 9 10 0 0 2 3 5 7 9	51 54 58 61 64 68	25 4 99 27 70 05 10 27 0 05 10 3	47 51 55 59 62 66 70 73 77 84 88 92	26 11 8 4 0 8 5 1 9 6 2 10 6 3	51 55 59 63 67 75 79 83 87 91 95	27 9 8 8 7 7 7 6 6 6 6

Note:—The rule for this table is worked in the same manner as the rule for scantling measure, on page 151.

CUBIC CONTENTS OF ROUND TIMBER WHEN SQUARED.

Length			_	DIA	ME	rer	IN	INCI	IES	S.		
n Feet.	1	.0		11	1	2		13		14		15
13 14	ft.		ft. 4 5	in. 11 4	ft. 5 6	in. 10 4	ft. 6	in. 10 5	ft. 8 8	in. 0 7	ft. 9 9	in 2
15	4444555566667	1 5 8	5	8	6	9	7	11	9	- 2	10	2 10 7 3 11 8 4 1 9 6 2 11
15 16 17 18 19 20	5	0	6	1 5	7	2 8 1	8 9	5	9 10	10 5	11 11	11
18	5	8	6	10	8	1	9	6	11 11	0	12 13	8
19 20	5	8 11 3 7	6 7 7	2 7	8	7	10 10	0	11	8	13 14	4
21	6	7	7	11	.9	5 11	11	7 1 7	12 12 13	10	14 14	ģ
22	6	11 2	8	8	9 10	11	$\frac{11}{12}$	$\frac{7}{2}$	$\frac{13}{14}$	6	15 16 16	. 6
23 24 25	7	6	8	1	10	10	12	8	14 15	8	16	1
20	7	10 16	9	$\frac{5}{17}$	11	8	13	19	119	20	17	21
13	110	5	111		13		114	8	16		17	
14	11	2	12 13	9 8 7	14	-	15	10 11	17	3 6	19	4
16	12 12		14	5	15 16		2 16 2 18	11	18 20	0	$\frac{20}{22}$	1
14 15 16 17 18 19 20	12 13 14 15	9 7 5 2	15 16 17	$\frac{4}{3} \\ \frac{2}{1}$	17 18		3 19 3 20	1 2 4 5 7 8	21	9 0 3 6 9	23	10
19	15	2	17	2	19		21	5	22 23	9	24 26	1
20 21	16 16	0	18 19	$\frac{1}{0}$	20 21		$\frac{1}{2}$	7 8	$\frac{25}{26}$	- 3	27 28	11 8 10 10 11 11
22 23	17 18	97	19	10	22		3 24	10	97	3	30	4
23 24	18 19	5	20 21	9 8	23 24			11 1	28 30 31	9	31 33	1
24 25	20	0	$\begin{array}{c} 21 \\ 22 \end{array}$	8 7	25	= 4	1 28	2	31		33 34	
	•	22		23		24	<u> </u>	25		26		27
13 14	$\frac{19}{21}$	8	$\frac{21}{23}$	6 2 10	23 25		5 25 2 27 3 29	5 4	27 29 31	67	29 31	1
15	22	8	24	10	27	- (29	4	31	8	34	- 2
17	24 25	9	26 28 29	5 1	28 30	1	7 33	2	33 35	10 11	36 38	
13 14 15 16 17 18 19 20	27 28	82829393939	29	9 5 1	32 34		35 2 37	4 4 3 2 2 1	38 40	0	141	. (
20	30	3	31 33	1	36	1	0 39	1	42	3 4	43 45	
21	31 33	9	134	$\frac{\bar{9}}{4}$	37	1		0	44 46	6	47 50	10
22 23	34	9	36 38	- 0	41		5 44	11	48	7	52	-
24 25	36 37	4 10	39 41	8	43			11 10	50 52	- 8 10	54 56	

NOTE:—The rule for this table is worked in the same manner as the rule for scantling measure, on page 151.

STANDARD CONTENTS OF LOGS.

Length		DI.	AMETER	R IN INC	HES.	
in Feet.	10	11	12	13	14	15
10	.21	.26	.31	.36	.42	.48
11	.23	.28	.34	.40	.46	.53
12	.26	.31	.37	.43	.50	.58
13	.28	.34	.40	.47	.54	.62
14	.30	.36	.43	.50	.58	.67
15 16	.32	.39	.46	.54	.63	.72
16	.34	.41	.49	.58	.67	.77
17	.36	.44	.52	.61	.71	.81
18	.38	.46	.55	.64	.75	.86
19	.40	.49	.58	.68	.79	.91
20	.43	.52	.61	.72	.84	.96
21	.45	.54	.64	.76	.88	1.01
22	.47	.57	.67	.79	.92	1.05
	16	17	18	19	20	21
10	.55	.62	.69	.77	.85	.94
11	.60	.68 .74	.76	.85	.94	1.03
$\overline{12}$.65	.74	.83	.92	1.02	1.13
13	.71	.80	.90	1.00	1.11	1.22
14	.76	.86	.97	1.08	1.19	1.32
15	.82	.92	1.04	1.15	1.28	1.41
16	.87	.99	1.10	1.23	1.36	1.50
17	.93	1.05	1.17	1.31	1.45	1.60
18	,98	1.11	1.24	1.38	1.53	1.69
19	1.04	1.17	1.31	1.46	1.62	1.79
20	1.09	1.23	1.38	1.54	1.70	1.88
21	1.15	1.29	1.45	1.62	1.79	1.97
22	1.20	1.35	1.52	1.69	1.88	2.07
	22	23	24	25	26	27
10	1.03	1.13	1.23	1.33	1.44	1.55
11	1.13	1.24	1.35	1.46	1.58	1.71
12	1.24	1.35	1.47	1.60	1.73	1.86
13	1.34	1.47	1.60	1.73	1.86	2.02
14	1.44	1.58	1.72	1.86	2.02	2.17
15	1.55	1.69	1.84	2.60	2.16	2.33
16	1.65	1.80	1.96	2.13	2.30	2.49
17	1.75	1.92	2 09	2.26	2.45	2.64
18	1.86	2.03	2.21	2.40	2.59	2.80
19	1.96	2.14	2.33	2.53	2.74	2.95
20	2.06	2.25	2.46	2.66	2.88	3.11
21	2.17	2.37	2.58	2.80	3.02	3.26
22	2.27	2.48	2.70	2.93	3.17	3.42

Note:—A log 13 feet long and 19 inches in diameter is the standard. The table shows the comparison of logs with this standard.

Table showing the Temperature of Steam at different pressures, from 1 lb., to 240 lbs., per square inch, and the quantity of Steam produced from a cubic inch of water, according to pressure.

		nen or w	ater,	accor	ding to p	11655	ure.	
re In	Corresp'd'g Temp. of S. to pressure.	C. Ins. of S. 108261 68261 782621 782	Pressure er Sq. In.	Corresp'd'g Temp. of S. to pressure.	C. Ins. of S. from a C.In of water accord'g to P.	essure Sq. In.	Corresp'd'g Temp. of S. to pressure.	C. Ins. of S. from a C.In of water accord'g to P.
Pressure er Sq. Ir	Corresp'd Temp. of to pressur	C. Ins. of from a C. of water a cord'g to	ssm Sq.	o SS	C. Ins. of from a C. of water a cord'g to	Pressure er Sq. II	p'q o ssu	C. Ins. of from a C. of water a cord'g to
S. X	e de	rat 2	SS	g d g	at s		es res	ata
Pr	買り	13 × 5 1	Pre	算算型	11 6 ≥ 21	Pr	計算品	Ta va
Q	245	15.#g81	1,0		S##2	ΙÃ	243	S 5 # C
1	102.9 126.1	20868	39	267.5	695 679 666	77 78	313.1 314.0 314.9	374 370
2 3 4 4 5 6 6 7 7 8 9 10 11 12 13 14 15 16 17 18 19 200 21 22 23 24 25 26	126.1	10874	40	269.1	679	78	314.0	370
- 3	141.0	1401	41	270.6	666	79	314.9	366
4	152.3 161.4 169.2 175.9 182.0 187.4 192.4 197.0	5685	42	272.1	649 635 622 610	80	1 315.8	362
5	161.4	4617	43	273.6	635	81	316.7	358
6	169.2	3897 3376	44	275.0	622	82	317.6	354
7	175.9	3376	45	276.4	610	83	318.4 319.3	350
- 8	107.4	2983 2674	46	277.8	589 586	84 85	320.1	346 342
10	102.4	2426	48	279.2 280.5	575	86	321.0	339
11	197.0	2221	49	281.9	564	87	321.8	335
12	201.3	2050	50	283.2	554	88	322.6	332
13	201.3 205.3	1904	51	284.4	544	89	322.6 323.5	332 328
14	209.1	2050 1904 1778	52	285.7	534	90	324.3	325
15	212.8	1 1669 1	53	286.9	525	91	325.1	322
16	216.3	1573 1488 1411	54	288.1	516	92 93	1 325.9	319
17	219.6 222.7	1488	55	289.3 290.5	508	93	326.7 327.5	316
18	222.7	1411	56	290.5	500	94	327.5	313
19	225.6	1343	57	291.7	492	95	328.2	310
20	228.5	1281 1225 1174 1127 1084 1044	58	292.9	484 477	96	329.0 329.8	307
21	231.2 233.8	1225	59 60	294.2	470	97	329.8	304 301
99	233.0	11/4	61	295.6	470	98	331.3	298
24	236.3 238.7	1084	62	296.9 298.1	463 456	99 100	332.0	295
25	241.0	1044	63	299.2	449	110	339.2	295 271
26	243.3	1007	64	300.3	449 443	120	345.8	251
27 28 29	245.5	973	65	301.3	437	120 130	352.1	233
28	247.6	941	66	302.4	437 431	140	357.9	218 205
29	249.6	911	67	303.4	425	150	363.4	205
30	251.6	883	68	304.4	419	160	368.7	193
31	253.6	857	69	305.4	414	170	373.6	183
32	255.5	833	70	306.4	408	180	378.4	174
30 31 32 33 34 35 36 37	257.3	810	71	307.4	403	190	382.9	193 183 174 166 158 151 145
34	259.1	788 767	72	308.4	398 393	200 210	387.3 391.5	151
50 90	260.9 262.6	767	73 74	309.3	393	210	391.5	145
27	264.3	729	75	311.2	383	230	399.4	140
38	265.9	712	76	312.2	379	230 240	403.1	140 134
00	1 200.0	114	10	1 014.4	1 010	1 410	1 100.1	. 101

Note:—Add the pressure of the atmosphere 15 fbs to the pressure on the Steam gauge, to correspond with the table.

Table showing the average Pressure of the Steam upon the Piston throughout the Stroke When, cut-off in the Cylinder, from 1-3 to 11-12 commencing with 10 lbs., and advancing in 5 lbs., up to 135 lbs., Pressure.

	135 lbs., Pressure.
Cut- the ler.	Pressure in 1bs., at the Commencement of the Stroke.
in ind	10 15 20 25 30 35 40 45 50 55 60 65 70 75
Steam off ir Cylin	Average Pressure in Ibs. upon the Piston.
	7 101 141 171 21 1241 28 1211 35 1381 42 1451 49 1591
133424555566677777788888999 1234151234561357 12341561357	$\begin{array}{c} 7 & 104 & 144 & 174 & 21 & 244 & 28 & 814 & 85 & 385 & 42 & 464 & 615 & 656 & 704 \\ 94 & 14 & 184 & 234 & 234 & 234 & 324 & 372 & 42 & 464 & 514 & 564 & 616 & 657 & 704 \\ 85 & 123 & 17 & 21 & 254 & 294 & 232 & 262 & 292 & 292 & 392 & 393 & 384 & 414 & 444 \\ 95 & 144 & 194 & 24 & 284 & 333 & 333 & 343 & 424 & 464 & 502 & 555 & 594 & 634 \\ 94 & 144 & 194 & 24 & 284 & 333 & 333 & 434 & 484 & 53 & 577 & 624 & 677 & 724 \\ 77 & 124 & 13 & 154 & 154 & 152 & 294 & 234 & 225 & 284 & 313 & 364 & 394 \\ 97 & 13 & 18 & 224 & 27 & 314 & 364 & 404 & 451 & 494 & 554 & 568 & 684 & 673 & 444 & 494 & 544 & 494 & 544 & 684 & 684 & 733 & 444 & 494 & 544 & 494 & 544 & 684 & 684 & 733 & 444 & 644 $
4-9	8 112 116 120 124 128 132 136 1401/441/481/521/561/601
5-9 7-9 8-9	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
1-11 2-11 3-11	44 74 94 121 144 174 195 22 245 27 295 314 344 364
4-11 5-11 6-11	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
7-11 8-11 9-11	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
10-11 1-12	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
7-12 11-12	$\begin{array}{c} 8\frac{1}{4} & 12\frac{1}{4} & 16\frac{3}{4} & 21^{2} & 25\frac{1}{4} & 29\frac{1}{4} & 33\frac{3}{4} & 38 & 42\frac{1}{4} & 46\frac{1}{4} & 50\frac{3}{4} & 59\frac{1}{4} & 69\frac{3}{4} $

Table showing the average Pressure of the Steam upon the Piston throughout the Stroke when cut-off in the Cylinder, from 1-3 to 11-12 commencing with 10 lbs., and advancing in 5 lbs., up to 135 lbs., Pressure, (Continued).

Cut- the	Pressure in Ibs., at the Commencement of the Stroke.	
Hind	80 85 90 95 100 105 110 115 120 125 130 135	5
Steam off ir Cylin	Average Pressure in Ibs. upon the Piston.	-
1/ ₃ 2/ ₃ 1/ ₄ 1/ ₂ 3/ ₄ 1-5	$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	
2/3 1/4		
1/6	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	
3/4	$77\frac{4}{4}82$ 87 $91\frac{3}{4}$ $96\frac{4}{2}$ $101\frac{1}{4}$ $106\frac{4}{4}$ 111 $115\frac{3}{4}$ $120\frac{4}{4}$ $125\frac{1}{2}$ $130\frac{1}{2}$	
1-5	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	į
2-5	1 6 1 5 160 1 169 17 2 2 7 6 5 1 80 5 1 84 5 1 8 1 9 1 2 1 9 5 2 1 9 5 1 10 3	ĭ
3-5		1
4-5	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	_
1-6	$\begin{array}{c} 37\frac{1}{4}39\frac{1}{2}41\frac{1}{4}44\frac{1}{4}46\frac{1}{2}48\frac{1}{4}&48\frac{1}{4}&51\frac{1}{4}&53\frac{1}{4}&55\frac{1}{4}&58\frac{1}{4}&60\frac{1}{2}&62\\ 78\frac{3}{4}83\frac{3}{4}88\frac{3}{4}99\frac{1}{2}98\frac{1}{2}108\frac{1}{2}108\frac{1}{4}112\frac{1}{4}118\frac{1}{4}123\frac{1}{4}128&133 \end{array}$	4
5-6 1-7		3
2-7	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	
3-7	$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	
4-7	$71\frac{1}{4}65\frac{1}{4}80^484\frac{1}{2}89 93\frac{1}{4}98 102\frac{1}{4}106\frac{1}{4}111\frac{1}{4}115\frac{1}{4}120$	1
5-7	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	3
6-7	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	
1/8 3/8 5/8 7/8	002 042 046 006 006 406 422 446 402 40 60 64	
3/8	1 005 00 (007 105 177 10 017 005 00 027 005 100	1
5/8	$73\frac{7}{2}78$ $82\frac{1}{2}87\frac{7}{4}91\frac{7}{4}91\frac{7}{4}91\frac{7}{4}101\frac{1}{2}101\frac{1}{2}110\frac{1}{4}114\frac{7}{4}119\frac{7}{4}12\frac{1}{4}12\frac{1}{4}119\frac{7}{4}12\frac{1}{4$	
1/8	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	
1-9 2-9	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	
4-9	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	
5-9	$ 70\frac{1}{2} 74\frac{3}{4} 79\frac{1}{4} 83\frac{3}{4} 88^2 92\frac{1}{2} 97^2 101\frac{1}{4} 105\frac{3}{4} 110\frac{1}{4} 114\frac{1}{2} 119$	2
7-9	1 779 829 874 924 974 H OZ 1107 H H I 19 H 16 9 H Z L # H Z 0 # H Z 1	14
8-9	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	
1-11	1 245 204 274 294 304 524 554 555 57 566 40 41	ž
2-11	291 413 441 463 49 511 54 561 59 611 633 66	
3-11 4-11	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	
5-11	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	23
6-11	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	1
7-11	731 781 83 873 921 97 1011 1061 1103 1151 120 1124	3
8-11	1 76월 81월 86월 91 195월 1101월 1105월 1110월 1115 1119월 124월 1129	1
9-11	+781831881931981103 + 108 + 1123117312231271132	
10-11	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	4
1-12		
7-12 11-12	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1

CONDENSING ENGINE.

EXAMPLE:— 15 pounds pressure on the piston above atmosphere, cut-off at one-fourth the piston's traverse, will be thus; 15 pounds steam and 15 pounds that atmosphere pressure equals 30; then look for 30 pounds at the head of the table, and down the first column for 14; trace that 14 under 30 and you will find the average to be 1734 pounds throughout the stroke.

NON-CONDENSING ENGINE.

EXAMPLE:—45 pounds steam above atmosphere upon the piston, cut-off at one quarter the length of stroke. Thus 45 pounds of steam cut-off at one-fourth the stroke

with 15 pounds added make 60 pounds.

Look for 60 on the top line and 14 on the side, trace that 14 to the figures under 60 and the average will be found to be 3534 pounds. Take 16 pounds from 3534 pounds, for friction (1 fb)., and atmosphere pressure, and there remains 1934 pounds, the available pressure on the piston.

STEAM.

A cubic inch of water evaporated under an ordinary atmospheric pressure is converted into 1 cubic *foot* of steam (approximately).

The specific gravity of steam (at atmospheric pressure) is .411 that of air at 34° Fahrenheit, and .0006 that of water

at same temperature.

27.222 cubic feet of steam weigh 1 pound; 13.817 cubic feet of air weigh 1 pound.

Locomotives average a consumption of 3000 gallons of

water per 100 miles run.

The best designed boilers, well set with good draft and skillful firing, will evaporate from 7 to 10 pounds of water per pound of first-class coal. The average result is from 25 to 60 per cent. below this.

In calculating horse-power of Tubular or Flue boilers, consider 15 square feet of heating surface equivalent to

one nominal horse-power.

Steam engines in economy, vary from 20 to 60 pounds of feed water, and from 2 to 7 pounds of coal per hour per

indicated horse-power.

Condensing engines require from 20 to 30 gallons of water to condense the steam represented by every gallon of water evaporated—approximately for most engines, we say, from 1 to 1½ gallons per minute per I. H. P. Jet condensers do not require quite as much water for condensing as surface condensers.

Surface condensers should have about 2 square feet of tube (cooling) surface per horse-power of steam engine.

RATIO OF VACUUM TO TEMPERATURE (Fahrenheit) OF FEED WATER.

0	Inches.	Vacuum	212°	171/2	Inches,	Vacuum,	112°
11	66	66	190°	281/2	6.	44	92°
18	66	66	170°	29	66	66	72°
221	6 66	66	150°	291/2	6.6	6.6	52°
*25	- "	66	135°	/2			

*Usually considered the standard point of efficiency--condenser and air pump being well proportioned.

A TABLE OF MULTIPLIERS TO FIND THE LAP AND LEAD, WHEN THE STEAM IS TO BE CUT OFF AT 14 TO 76ths OF STROKE.

			11 1		/80H3	OI C	TILOI	X.13.	
H	alf-	Five-e		Thi	ee-	Sev	en-		100
	olza	0		fourth	s of	eight	hs of		
Sur	one.	the st	roke.	the St	roke.	theS	troke		
1	2	1	2	1	2	1	2		
lap.	lead.	lap.	lead.	lap.	lead.	lap.	lead	nee of the Piston from the troke when steam is read- the return stroke being If the stroke multiplied by	
2.41	.000	1.58	.000	1.000	.000	.540	.000	3.3 t	.00000
2.16	.145	1.41	.124	.893	.105	.477	.089	8223	.00208
2.06		1.35	.170	.851	.146	.450	.123	28 0 2	.00416
1.94	.268	1.27	.231	.795	.200	.413	.170	2 5 6	.00833
1.84	.318	1.21	.276	.754	.240	.385	.204	2833	.01250
1.97	.358	1.16	.312	.723	.271	.363	.232	2882	.01666
1.71	.391	1.12	.342	.691	.299	.344	.257	6282	.02083
1.65	.420	1.08	.368	.668	.322	.327	.277	2230	.02500
1.60	.444	1.05	4.391	.644	.343	.313	.296	3.5 E	.02916
1.56	.467	1.02	.412	.623	.362	.298	.313	3 2 8	.03333
1.48	.505	.968	.449	586	.396	.273	.343	2882	.04166
1.41	.540	.921	.480	.554	.425	.251	.370	£ 45 6	.05000
1.35	.570	.881	.508	.526	.451	.232	.393	distance of its stroke for the to half the	.05833
1.30	.595	.844	.532	.500	.473	.215	.414	its fo fo	.06666
1.25	.617	.810	.554	.476	.495	.198	.434	2 2 3	.07500
1.21	.638	.779	.572	.454	.514	.183	.452	2828	.08333
1.17	657	.751	.592	.434	.532	.160	.468	itt ua	.09166
1.13	.674	.724	.607	.415	.548	.156	.483	The cend of mitted equal t	1.00000

The lap must be equal to the width of the Steam port multiplied by col 1. The lead must be equal to the width of the Steam port multiplied by col 2.

of the Steam port multiplied by col. 2.

EXAMPLE:—Stroke 36 inches; width of port 2 inches; Steam to be cut off at half-stroke; distance of the piston from the end of its stroke when Steam is readmitted for

the return stroke, 1.5 inches. $1.5 \div 18 = .0838$ Find that number or the one nearest to it, in the right hand or last column, and take out the multipliers on the same line under the head half-stroke.

Then $2 \times 1.21 = 2.42$ inches = the lap. And $2 \times .638 = 1.276$ " = the lead. Table showing the amount of "LAP" required for slide valves, when the Steam is to be worked expansively.

Traverse	Tra	verse	of the	e Pist	on wh	nen th	e Ste	am is c	ut-off.
of the Valve in	1/4	1/3	5-12	1/2	7-12	2/3	3/4	10-12	11-12
Inches.		, , , ,		The	requ		ap.		
2 21/ ₂ 3	$1_{16}^{7/8}$	13/4	11 16 78	5/8 13 16	9 16 11 16 51	1/2 16 3/4	1/2 1/2 5/8 7/8	3/8	. 5g
31/2	11/4 11/2	$1\frac{3}{16}$ $1\frac{5}{16}$	$\frac{11/8}{116}$	11/8	1_{16}^{16}	1	5/8 7/8	916 3/4 136 7/8	1/2 1/5
$\frac{4}{41/2}$	13/4 2	$1\frac{9}{16} \\ 1\frac{13}{16} \\ 2$	1_{16}^{16} 1_{16}^{16} 1_{16}^{13}	1 16 11/2	13/8	11/4	11/8	78	5/8 3/4
51/2 6	$2\frac{1}{8}$ $2\frac{5}{16}$ $2\frac{1}{2}$	2_{16} 2_{16}	$\frac{113}{2}$ $\frac{2}{216}$	1_{16}^{9} 1_{16}^{13} 2	11/2 15/8 113	13/8 11/2 15/8	13/8 11/2	11/8 13/6	78 15 16
6½ 7	$egin{array}{c} 23\overline{4} \ 3 \end{array}$	$\frac{2^{9}_{16}}{2^{11}_{16}}$	$\frac{2_{16}}{2_{16}}$	$\frac{2^{3}}{2^{32}}$	$\frac{2}{23}$	$\frac{1}{16}$	15/8 13/4	114	11/8
71/ ₂ 8	$3^{\frac{3}{16}}_{16}$	$\frac{3}{3}$	$\frac{211}{6}$	21/2 25/8	$2\frac{3}{8}$ $2\frac{1}{2}$	$\frac{2\frac{3}{32}}{238}$	27/8 2	11/2 15/8	$\frac{1\frac{3}{16}}{1\frac{1}{4}}$
81/2 9	$\begin{vmatrix} 35/8 \\ 3\frac{13}{16} \end{vmatrix}$	$\frac{3\frac{5}{16}}{35/8}$	3^{3}_{16} 3^{5}_{16}	213 3	$2^{11}_{16} \\ 2^{13}_{16}$	$\begin{array}{c c} 21/2 \\ 2\frac{11}{16} \\ 2\frac{13}{16} \end{array}$	21/8 21/4	$\begin{vmatrix} 134 \\ 178 \end{vmatrix}$	$\frac{1\frac{5}{16}}{13/8}$
91/2 10	41/4	313 4	35/8 313	3 5 5 91/2	3 3 3 5 5 5 5	3	23/8 21/2	2 216	11/2
101/2 11 $111/2$	$4\frac{7}{16}$ $4\frac{9}{16}$ $4\frac{13}{16}$	41/4 47/6	4 41/4 476	31/2 35/8 37/8	31/2 31/8	31/8 31/8 33/8	25/8 23/4 27/8	$ \begin{array}{c c} 2\frac{3}{16} \\ 2\frac{1}{4} \\ 2\frac{3}{8} \end{array} $	15/8
12 12	413 5	1_{16}^{9} 1_{16}^{13}	49	41/8	4	35/8	3 3	21/2	17/8

Note:—The traverse of the valves being ascertained, and also the amount of cut-off desired, the above table shows the amount of "LAP" required.

TABLE OF CONSTANT NUMBERS, by which to ascertain the AVERAGE PRESSURE of the STEAM against the PISTON for DIFFERENT PRESSURE and POINTS OF CUT-OFF, from 1-4 to 7-8 of the stroke.

Point of Cut-off.	Constant Number.	Point of Cut-off.	Constant Number.
1/4 1/5	.5965 .6995	5/8	.9188 .9370
3/8 1/2	.7428 .8465	3/4 7/9	.9657 .9919

Multiply the pressure in pounds, as shown by the gauge, by the constant number opposite the point of cut-off in the left column. The product is the average.

Table showing usual consumption of coarse anthracite coal and soft wood by different sized engines, 12 hours per day.

Horse- Power.	Pounds of Coal.	- of Wood.	Horse- power.	Pounds of Coal.	Cords of Wood.
4 6 8 10 12 14 16 18 20 25 30 35 40	168 252 336 420 504 588 672 756 840 1066 1260 1458 1680 1896	1/2 34 1 11/4 11/2 13/4 2 21/4 21/2 3 31/2 41/4 43/4 51/2	50 55 60 65 70 75 80 85 90 95 100	2100 2300 2520 2780 2940 3150 3360 3560 3780 3990 4200	6 61/2 71/4 81/2 91/4 98/4 101/2 11 113/4 121/2

Table showing the effluent velocity with which Steam at different pressures, will flow into the atmosphere, or into steam at a lower pressure

	enco sceum ac	a cower pressur	6	
Pressure above the atmosphere.	Velocity of escape per Sec.	Pressure above the atmosphere.	Velocity of escape per Sec.	
lbs.	feet.	il ibs.	feet.	_
1	540	. 50	1736	
. 2	698	60	1777	
3	814	70	1810	
4	905	80	1835	
5	981	90	1857	
10	1232	100	1874	
20	1476	110	1889	
30	1601	120	1900	
40	1681	130	1909	

TABLE Of AREAS of CYLINDERS from I to 36 ins. DIAM. Diam. | Area | Diam. | Area | Diam. | Area || Diam | in Ins. .78 51/2 283 78 10 19 11/2 1.7 28.2 20 314 11 95 21/2 3.1 61/2 33.1 12 113 21 346 4.9 38.4 $\overline{13}$ 132 380 3 7. 71/9 153 23 415 44.1 14 31/2 9.6 50.215 176 24 452 12.5 $\tilde{28}$ 81/2 56.7 615 16 201

To find the area—Multiply the square of the diameter in inches by .7854—For other Areas see page 73.

17

 $\bar{18}$

226

254

63.6

70.8

9

91/9

30

36

706

1017

41/2 | 15.9

19.6

Table showing length of stroke and number of revolutions for different piston speeds in feet per minute.

Stroke in Ins.		Spe	ed of	Pisto	n in f	eet pe	r min	ute.	
51	200	210	220	230	240	250	260	270	! 280
E.St				Re	voluti	ons.	7 - 1		- 1
2	600	630	660	690	720	750	780	810	840
3	400	420	440	460	480	500	520	540	560
4	300	315	330	345	360	375	390	405	420
5 .	240	252	264	276	288	300	312	324	336
3 4 5 6 7	200	210	220	230	240	250	_260	270	280
7	179	180	188	197	206	214	223	231	240
8	150	107	165	172	180	187	195	202	210
9	133	140	147	153	160	166	173	180	187
10	120	126	132	138	144	150	156	162	168
11	109	114	120	125	131	136	142	147	153
12	100	105	110	115	120	125	130	135	140
13	92	97	101	106	111	115	120	125	129
14	86	90	94	98	103	107	111	116	120
$\tilde{1}\tilde{5}$	80	84	88	92	96	100	104	108	112
16	75	79	82	87	90	94	97	101	105
17	70	74	78	8i	85	88	92	95	99
18	67	70	73	76	80	83	86	90	93
	1 01	1 10	1 .0	1 10	1 00	1 00	1 00	1 00	1 00

TABLE of Units of H. P. for DIFFERENT PISTON SPEEDS. Indicated Horse-Power for each pound average pressure per square inch, with different Diam, and speed of piston.

Diam.					feet p			4
linder	240	300	350	400	450	500	550	600
lns.								'
4	.091	.114	.133	.152	.171	.19	.209	.228
5	.144	.18	.21	.24	.27	.3	.33	.36
6	.205	.256	.299	.34	.385	.428	.471	.513
7	.279	.348	.408	.466	.524	.583	.641	.699
- 8	.365	456	.532	.608	.685	.761	.837	.912
9	.462	.577	.674	.77	.866	.963	1.059	1.154
10 .	.571	.714	.833	.952	1.071	1.39	1.409	1.428
- 11	.691	.864	1.008	1.152	1.296	1.44	1.58	1.728
12 -	.820	1.025	1.195	1.366	1.54	1.708	1.884	2.05
13	.964	1.206	1.407	1.608	1.809	2.01	2.211	2.412
14	1.119	1.398	1.631	1.864	2.097	2.331	2.564	2.797
15	1.285	1.606	1.873	2.131	2.409	2.677	2.945	3.212
16	1.461	1.827	2.131	2.436	2.741	3.045	3,349	3.654
17	1.643	2.054	2.396	2.739	3.081	3.424	3.766	4.108
18	1.849	2.312	2.697	3.083	3.468	3.854	4.239	4.264
19	2.061	2.577	3.006	3.436	3.865	4.295	4.724	5.154
20 21	2.292	2.855	3.331	3.807	4.265	4.759	5.234	5.731
22	2.518	3.148	3.672	4.197	4.722	5.247	5.771	6.296
22	2.764	3.455	4.031	4.607	5.183	5.759	6.334	6.911

Applebys Table showing the number of gallons discharged per minute by single-acting pumps of a grobebys Technique.

											- P	in													
		15	075.	099.	.945	1.29	1.695	2.64	3.81	5.19	6.78	8.57	10.5	12.75	15.15	20.77	27.13	34.33	42.40	61.02	95.41	137.37	169.6	244.23	oumps at 10
		14	392	919.	.882	1.204	1.582	2.464	3.55	4.84	6.32	8.0	8.6	11.9	14.14	19.38	25.32	32.04	39.56	56.94	89.04	128.2	158.3	227.9	-
		12	338											10.2	12.12	16.62	21.7	27.46	32.92	48.08	76.32	109.88	135.68	195.4	single-acting
F	HES.	10	.280												_		18.09							162.82	for sing
TATAT	INCI	6	.252								4.06	5.14	6.3	7.65	9.09	12.06	16.28	20.60	25.44	36.61	57.24	82.42	101.76	146.53	calculated
	NI.	8	.224																			73.26	90.45	130.25	are calc
1	KOKE	7	961.									4.20	4.9	5.95	7.07	69.6	12.66	16.02	19.78	28.47	44.52	64.10	79.15	113.97	and
E CO	Z Z	9	168									3 43	4.2	5.10	90.9	8.31	10.85			24.40	38.16	54.94	67.84	69,66	gallons,
	H OF	9						088				2.86	3.5	4.25	5.05	6.92	9.04	11.44	14-13	20.34	31.80	45.79	56.53	81.41	1
3	5	4	ļ					8 .704				9.29	8	3.40	4.04	5.54	7.23	9.15	11.30	16.27	25.44	36.63	45.23	65.12	given in the table are in
year	Z Z Z	e 						528			_	1 71	2.1	2.55	3.03	4.15	5.42	98.9	8 48	12.20	19.08	27.47	33.92	48.48	in the
		2											7 1.4		1 2.02		0 3.6	89 4.5	27 5 4	000	61 12.75	58 18 3	07 22 6	82 32.56	s given
4	hl.	9S. 1	-	_	_	_		_	_					_	_		28	2.2	000	4.6	60	6	1	16.2	antitie
Diom	plant. or	in inches.	-	11/4	971	100	2.2	21%	. 00	31%	4	41%	5,42	6/19	9	2	00	6	2	25	15	<u>x</u>	06	121	The quantities

strokes per minute; if required for double-acting pumps the number found in the table should be doubled. The quantity for any other number of strokes may be found by multiplying or dividing the number found in the table.

Table showing the power to raise water to different altitudes, varying from I foot to 10.000 feet.

What a	H. P.	2 H. I	. will	3 H. I	P. will	4 H. P	wifi	
will rais		raise		raise		raise per		
minu		min		min	ute.	minute.		
gals.	feet	gals.	feet		gals. feet		feet	
or	or	or				gals.		
			or	or	or	or	or	
feet.	gals.	feet.	gals.	feet.	gals.	feet.	gals.	
2.500	1	5.000	1	7.500	Ţ	10.000	1	
1.250	2.	2.500	2	3.750	2	5.000	2	
833	3	1.666	3	2.500	3	3.333	3	
625	4	1.250	4	1.875	4	2.500	4	
500	5	1.000	2 3 4 5	1.500	5	2.000	5	
416	6	833	-6	1.250	2 3 4 5 6 7	1.666	6	
357	2 • 4 5 6 7	714	7	1.070	7	1.428	7 1	
312	8	625	8	937	8	1.250	2 3 4 5 6 7 8	
277	9	555	ğ	833	9	1.111	9	
250	1 0	500	10	750	10	1.000	10	
125	$\tilde{20}$	250	20	375	20	500	20	
83	30	166	30	250	30	333	30	
62	40	125	40	187	40	250	40	
50	50	100	50	150	50	200	50	
41	60	83	60	125	60	166	60	
35	70	72	70	107	70	142	70	
31					80	125	10	
31	80	62	80	93			80	
27	60	55	90	83	90	111	90	
25	100	50	100	75	100	100	100	

To find what an 8 Horse-Power will raise, multiply gals. or feet column under 4 Horse-Power by 2 the product will be the number of gals, or feet.

To find what any H. P. will raise, multiply gals. or feet in first column, by the H. P. you have, and the product will be the number of gals. or feet.

CAPACITY OF CISTERNS.—IN U.S. GALLONS, (2.31 Cubic Inches) FOR EACH 10 INCHES IN DEPTH.

Feet in Diam.	Gallons.	Feet in Diam.	Gallons.	Feet in Diam.	Gallons.
2	19.5	6	176.25	10	489.20
21/2 3	30.5 44.06	61/2	$206.85 \\ 239.88$	11 12	592.40 705.
31/2	59.97 78.33	71/2	275.40 313.33	13	807.4 959.6
41/2	99.44	81/2	353.72	15	1101.6
5 51/2	$122.40 \\ 148.10$	91/2	396.56 461.40	20 25	1958.6 3059.9

TABLE SHOWING THE CAPACITY OF CISTERNS AND TANKS, COMPUTED IN BARRELS OF 311/2 GALLONS.

Depth		D	AM	ET	ER	IN F	EET	٠.	1
in feet.	5	6	7	8	9-1	10	11	12	13
5	23.3	33.6	45.7	59.7	75.5	93.2	112.8	134.3	157.6
5 6 7	28.0	40.3	54.8		90.6	111.9	135.4	161.1	189.1
7	32.7	47.0	64.0		105.7	130.6	158.0	188 0	220.6
8 9	37.3	53.7	73.1	95.5	120.1	149.2	180.5	214.8	252.1
9	42.0	60.4	82.2	107.4	136.0	167.9	203.1	241.7	283.7
10	46.7	67.1		119.4		186.5	225.7	268.6	315.2
11	51.3	73.9	100.5	131.3	166.2	205.1	248.2	295.4	346.7
12	56.0			143.2		223.8	270.8	322.3	378.2
13	60.7			155.2		242.4	293.4	349.1	409.7
14	65.3	94.0	127.9	167.1	211.5	261.1	315.9	376.0	441.3
15	70.0			179.0		279.8	338.5	402.8	472.8
16	74.7	107.4	146.2	191.0	241.7	298.4	361.1	429.7	504.3
17	79.3	114.1	155.4	202.9	256.8	317.0	383.6	456.6	535.8
18	84.0	120.9	164.5	214.8	272.0	-335.7	406.2	483.4	567.3
19	88.7				287.0	354.3	428.8	510.3	598.0
20	93.3	134.3	182.8	238.7	302.1	373.0	451.3	537.1	630.4

For cisterns larger in diameter multiply the barrels of half the diameter by four and the product will be the number of barrels which it will contain. Thus 10 feet deep by 20 feet in diameter, $\frac{1}{2}$ of 20 feet is 10 feet, look opposite 10 feet in first column and under 10 feet we find $186.5 \times 4 = 746$ barrels.

Table showing the power in foot pounds, required to raise a given quantity of water a given height.

Height	. 1	Number of gallons raised per minute.									
in feet.	1	2	3	4	5	10	20	30	40	50	
1	20	40		80	100	175	300		5 50	675	
2	30	60	90	120	150	275	500	750	950	1175	
3	40	80	120	160	200	375	700	1025	1350		
5	50	100	150	200	250	475	900	1325	1750	2175	
5	60	120	180	240		575	1100		2150		
10	110	220		440					4154		
20	210		630		1050	2076	4102			10180	
30	310	620			1550	3076			12154		
40	410				2050	4076			16154		
50					2550				20154		
100	11010	2020	13030	14040	19090	10076	20102	30128	40104	190190	

The numbers given in the table are in foot lbs. including allowance for friction.

A foot pound = 1 lb. raised 1 foot high in 1 minute.

A man is capable of exerting 6.000 foot pounds for 10 hours a day, 33,000 ft. fbs. = 1 Horse-Power,

Table showing quantity of water per lineal foot in pumps verticle pipes of different diameters.

	verticie	pipes of	umerent	ulamete	15.
Diam. of			Diam. of		
Pump in		Cu. ft. per			Cu. ft. per
Inches.	lin. ft.	lineal foot	Inches.	lin. ft.	lineal foo
2	.136	.0218	8	2.176	.3490
21/4	.172	.0276	81/4	2.314	.3712
21/2	.212	.0340	81/2	2.456	.3940
$\frac{2\sqrt[3]{4}}{3}$.257	.0412	83/4	2.603	.4175
3	.306	.0490	9 1	2.754	.4417
31/4	.359	.0576	91/4	2.909	.4666
31/2	.416	.0688	91/2	3.068	.4923
33/4	.478	.0766	$93\sqrt{4}$	3.232	.5184
3¾ -	.544	.0872	10	3,400	.5454
41/4	.614	.0985	101/4	3.572	.5730
41/2	.688	.1104	101/2	3.748	.6013
43/4	.767	.1230	103/4	3.929	.6302
43/4 5	.850	.1363	11	4.114	.6599
51/4	.937	.1503	111/4	4.303	.6902
51/2	1.028 -	.1649	111/2	4.496	.7212
53/4	- 1.124	.1803	1134	4.694	.7529
5¾ 6	1.224	.1963	12	4.896	.7853
61/4	1.328	.2130	121/2	5.312	.8521
61/2	1.436	.2304	13	5.746	.9217
63/4	1.549	.2489	131/2	6.196	.9934
6¾ 7	1.666	.2672	14	6.664	1:0689
71/4	1.787	.2866	15	7.650	1.2271
71/2	1.912	.3067	16	8.704	1.3962
73/4	2.042 -	.3275	18	11.016	-1.7670

AIR IN MOTION.

Velocity of the wind.		Force or]			
Miles per Hour.	Feet per Sec.	pressure per sq. ft. in lbs. avoir.	Common applications of the Force Wind.			
1	1.47	.005	Hardly preceptible.			
$\frac{2}{3}$	2.93 4.40	.020 }	Just " -			
4 5	5.87 7.33	.079 {	Gentle pleasant winds.			
10 15	14.67 22.00	.492 { 1.107 }	Pleasant brisk gale.			
20 25	29.34 36.37	1.968 2	Very brisk.			
30 35	44.01 51.34	4.429 } 6.027 \$	High winds.			
40 45	58.68 66.01	7.873 } 9.963 \	Very high.			
50	73.35	12.300	A Storm or Tempest.			
60	88.02	17.715	A great storm.			
80	117.36	31,400	A hurricane.			

TABLE SHOWING NUMBER OF FEET IN SQUARE FRAMES OF DIFFERENT SIZES AND WIDTHS.

Leng- th in		Wi	dth o	f Mo	uldin	gs in	Inche	es.	
Ins.	1	11/2	2	21/2	3	31/2	4	41/2	5
8 10 12 14 16 18 20 22	2 1323 1323 4 1323 1323 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	223 33534 4455 5556 6667 7778 8889 990 10488	2 ² / ₃ 3 3 ¹ / ₃ 3 ² / ₃	3 3 3 3 3 3 3	3334 435 555 6 667	32	4 4 4 4 5 5 5 5 6 6 6 6 7 7 7 7 8 8 8 8 9 9 9 9 1 10 10 1 11 11 11 11 11 11 11 11 11 11	4 ¹ 323 5 556 6 6323 7	42
10	21	$2\frac{2}{3}$	3	31	33	4 13283 13283 15283 6 6 6 6 6 6	41	42	5
- 12	23	3	31	33	4	41	42	5	51
14	3	34	32	4 413 423 5 5 5 5 5 5 5 5 5	44	42	5	51	5
16	31	32	4 1525 5 1525 6 1525 7	41	42	5	51	53	6
18	32	4	41	42	5	54	52	6	61
20	4	41	43	5	54	5%	6	61	62
22	41	42	5	54	5%	6	61	62	7
24	42	5	54	5%	6	61	62	7	71
26	5	51	52	6	61	62	73	71	72
28 -	51	52	6	61 62 7	62	73	71	$\frac{7_{3}^{1}}{7_{3}^{2}}$	8
30	52	63	61	62	73	71	72	8	81
32	63	61	63	7	71	72	83	81	82
34	61	62	73	71	72	83	81	82	0,3
36	62	73	71	7½ 7½ 8	83	81	82	03	01
38	73	71	72	83	81	82	03	01	0.2
40	71	72	23	91	Q2	03	01	02	103
49	72	23	81	81 82 83	03	01	02	103	101
11	03	Q1	7 ¹ / ₃ 7 ² / ₃ 8 8 ¹ / ₃ 8 ² / ₃ 9	I 0. I	01	02	103	101	103
44	01	03	03	01	02	103	101	103	1103
40	03	03	01	02	10	101	103	103	111
40	03	01	03	91 92 10	101	103	113	111	119
50	01	03	103	101	103	113	11,	113	103
04	93	103	101	10½ 10¾	113	111,	113	113	101
04	193	10	91 92 10 101 102 103	103	71525 8 88 8 9 1525 10 1525 10 1525 11 1525 11 1525	113	113	12	123
00	10	104	103	11	113	113	12	123	123
98	71323 81323 91323 101023	103	11	113	113	12	123	123	13
60	103	11	113	113	12	718 8 88 88 9 15 88 10 10 13 25 11 12 12 12 13 25 12 12 13 25 12 13 25 12 13 25 12 13 25 12 13 25 12 13 25 12 13 25 13 2	123	13	13
62	11	11½ 11½	113	12	121	123	13	131	133
24 26 28 32 34 38 40 42 44 46 50 52 54 56 66 66 66	11½ 11½	112 12	$\begin{vmatrix} 11_{\frac{1}{3}} \\ 11_{\frac{2}{3}} \\ 12 \\ 12_{\frac{1}{3}} \end{vmatrix}$	$11\frac{1}{3}$ $11\frac{2}{3}$ $12\frac{1}{3}$ $12\frac{1}{3}$	12 12 ₁ 12 ₃ 12 ₃ 13	13° 13¹	12^{1} 12^{1} 12^{2} 13^{1} 13^{1} 13^{2}	81923 91223 10 101223 11123 1123 1124 1123 11323 11323 11323 11323 11323 11323 11323 11323 11323 11323 11323 11323 11323 11323	10 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
66	112	12	121	$12\frac{2}{3}$	13	133	$ 13_{3}^{2}$	114	143

RULE.—Take the number of inches in half the size of a frame, (thus; a frame 22×28 added, making 50 inches), find 50 in the first column, select your width, and you have the number of feet desired.

SURFACE OF BOILER TUBES.

Diam.	Length.	Surface.	Diam.	Length.	Surface.
Ins.	ft. in.	sq. ft.	Ins.	ft. in.	sq. in.
21/2	5 0	3.27	3	6 0	4.70
"	5 3	3.42	6.6	6 3	4.90
66	5 6	3.60	6.6	6 6	5.10
4/4	5 9	3.75	66	7 0	5.50
- 66	6 0	3.90	44	7 6	5.89
66	6 3	4.05	66	8 0	6.28
44	6 6	4.20	"	8 6	6.67

VALUE OF IRON PER TON OF 2.240 POUNDS AT FROM 2c. TO 13c. PER LB.

per lb.	₩ Ton	per lb	P Ton.	per lb	₩ Ton	per lb	P Ton.
2	\$14.80	43/4	\$106.401	71/2	168.00	101/4	\$229.60
21/8	47.60	47/8	109.20	75/8	170.80	103/8	232.40
21/4	50.40	5	112.00	73/4	173.60	101/2	235.20
23/8	53.20	51/8	114.80	77/8	176.40	105/8	238.00
21/2	56.00	51/4	117,60	8	179.20	103/4	240.80
23/4	85.80	53/8	120.40	81/8	182.09	107/8	243.60
25/8	61.60	51/2	123.20	81/4	184.80	11	246.40
27/8 3	64.40	55/8	126.00	83/8	187.60	111/8	249.20
3	67.20	53/4	128.80	81/2	190.40	111/4	252.00
31/8	70.00	5%	131.60	85/8	193.20	113/8	254.80
314	72.80	6	134.40	83/4	196.00	111/2	257.60
33/8	75.60	61/8	137.20	87/8	198.80	115/8	260.40
31/9	78.40	61/4	147.00	9	201.60	113/4	263.20
35/8	81.20	63/8	142.80	91/8	204.40	117/8	266.00
33/4	84.00	61/2	145.60	91/4	207.20	12	268.80
37/8	86.80	63/8	148.40	93/8	210.00	121/8	271.60
4 .	89.60	63/4	151.20	91/2	212.80	121/4	274.40
41/8	92.40	67/8	154.00	95/8	215.60	123/8	277.20
41/4	95.20	7	156.80	93/4	218.40	121/2	280.00
43/8	98.00	71/8	159 60	97/8	221.20	125/8	282.80
41/2	100.80	71/4	162.40	10	224.00	123/4	285.60
45/8	103.60	$73/\hat{8}$	165.2C'l	101/8	226.80	13	291.20

DEPRECIATION OF MACHINERY.

Per Annum on first Cost.	Depre		ar and Tear.	To	tal.	
Engines. Boilers. Machinery tools. Mill work, shafti'g & gear.	6 pe 10 71/2	1 21/2	per ¢	9 1 13 11 6½ 45	per "	¢

REGULAR POLYGONS.

No. sid's	Name.	Numbers	s en squar	e for mi	itre.
4 5 6 7 8	Square, Pentagon. Hexagon. Heptagon.	12½ and 7¼, Any two equa 7¼ and 10, m 7¼ and 12½, 6 " 12½, 2 and 5; or 7 & 6½ and 20.	al number: ark along """	S.	

Regular polygons are plain figures whose sides are *equal* straight lines. A regular polygon of six sides is often called a six-square, and one of eight sides an eight-square, etc.

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Sec., 4.934 U. S. Rev. Stat. reads:	The :	following
shall be rates for patent fees;		
On application for patent, except in design	cases	. \$15.
In design cases for 3 y'rs and 6 mo.		10.
In design cases for 7 years.		15.
In "" " 14 "		30.
Filing caveat.		10.
" disclaimer.		10.
Re-issue application.		30.
On appeal from primary examiners.		10.
On appeal to Commissioner.		20.

CEMENTS.

Cast-Iron Slowly Setting.—Two ounces of sal-ammoniac, 1 cunce sulphur, and 16 cunces of borings or filings of cast-iron, to be mixed well in a mortar, and kept dry. When required for use, take one part of this powder to 20 parts of clear iron borings or filings, mix thoroughly in a mortar; make the mixture into a stiff paste with a little water, and then it is ready for use. A little fine grindstone sand improves the cement.

Cast-Iron Quickly Setting.—One ounce sal-ammoniac, 2 ounces of sulphur, and 80 ounces of iron filings or boring. Mix the same as for "slowly setting."

RED LEAD CEMENT FOR FACE JOINTS.—Equal parts of white and red lead, mixed with linseed-oil to the proper consistency.

For Leather.—By dissolving in a mixture of 10 parts; of bisulphide of carbon and 1 part of oil of turpentine enough gutta-percha to thicken the composition. The leather must be free from grease, which may be done by placing a cloth between the leather and a hot iron.

The pieces cemented must be pressed together until the cement is dry.

For Brass and Glass.—Boil 3 parts of resin with 1 part of caustic soda and 5 parts of water. Add 5 times its weight of plaster of Paris. It sets finely in from ½ to ¾ of an hour. Zinc, white lead, or percipitated chalk may be substituted for plaster, but hardens more slowly.

FOR STONE OR MARBLE.—The best cement for mending marble or any kind of stone, is made by mixing 20 parts of litharge and one part of freshly-burned lime in fine dry powder. This is made into a putty by the addition of linseed-oil. It sets in a few hours, having the appearance of light stone.

FIRE AND WATER-PROOF CEMENT.—To ½ pint of milk, put an equal quantity of vinegar, in order to curdle it; then separate the curd from the whey, and mix the whey with 4 or 5 eggs, beating the whole well together. When it is well mixed, add a little quick lime through a sleve, until it has acquired the consistency of thick paste. With this cement, broken vessels and cracks of all kinds may be mended. It dries quickly, and resists the action of water as well as considerable degree of fire.

FOR FASTENING LEATHER TO IRON, CHINA, OR GLASS.— To 1 quart of glue dissolved in good cider vinegar; add 1 ounce of good Venice turpentine. It should be allowed to simmer about ½ day.

How to Mix a Good Adhesive Cement.—Mix pulverized Gum-Arabic with its weight of finely powdered calcined alum. When mixed with a small quantity of water, it forms a cement which unites wood, paper, porcelain, glass, and crockery very finely. It must be kept dry in powder and moistened only as needed.

FOR CISTERNS AND WATER CASES.—Melted glue 8 parts; linseed-oil, 4 parts; boiled into varnish with litharge.

This cement hardens in about 48 hours, and renders the joints of wooden eisterns and casks air and water tight.

RUBBER BELTING.—Take 16 parts of Gutta-Percha or India-Rubber; 2 parts common pitch, and 1 part linseedoil. Melt together, and use hot. This cement will unite leather or rubber that has not been vulcanized.

For Steam Joints.—Take 2 parts powdered litharge, very fine sand, 2 parts; slacked quick-lime, 1 part. Mix all together. So use. Mix the proper quantity with boiled linseed-oil, and apply quickly. It gets hard very soon.

or 10 pounds of ground litharge; 4 pounds of ground Paris-white; 1½ pound of yellow ochre and 1½ ounce of hemp: Cut into lengths of 1½ inch: Mix all together with bolled linseed-oil to the consistency of a stiff putty. This cement resists fire and will set in water.

AMMONIA SHELLAC CEMENT.—As rubber plates and rings are now-a-days used almost exclusively for making connections between steam and other pipes and apparatus, much annoyance is often experienced by the impossibility or imperfection of an air-tight connection. This is obviated entirely by employing a cement which fastens alike well to the rubber and to the metal or wood. Such cement is prepared by a solution of shellac in ammonia. This is best made by soaking pulverized gum-shellac in 10 times its weight of strong ammonia, when a slimy mass is obtained which in three to four weeks, will become liquid without the use of hot water. This softens the rubber and becomes after volatilization of the ammonia, hard and impermeable to gases and fluids.

CEMENTS FOR BELTS.—The cements used for belts may be made by melting together; 1 part shellae; 2 parts pitch; 2 parts linseed-oil; 4 parts India-rubber; 16 parts guttapercha, until thoroughly incorporated. It is applied warm, in a thin coating, very quickly, and the 2 parts of the belt are properly and firmly clamped together and left until completely set.

CEMENT FOR BELTS.—Of common glue and American isinglass, take equal parts; place in a kettle, add sufficient water to cover the whole. Let them soak 10 hours; then bring the mixture to the boiling point, and add tannin, until the whole becomes soapy or appears like the white of eggs; apply it warm. Buff the grain off the leather where it is to be cemented; rub the joint surfaces solidly together, and let it dry for a few hours.

Transparent.—A transparent cement may be made by dissolving 75 parts of India-rubber (not vuncanized) in 60 parts of chloroform, and adding to this solution 15 parts of gum mastich. Balsam of fir will also serve the purpose, as it is a strong cement when not exposed to heat. Both the cement and the edges of the article to which it is applied should be previously warmed before joining.

FOR LEATHER, WOOD, ETC.—A cement resisting the action of water both hot and cold, and most of the acids and alkalies. Three parts, by weight, of shellac and 1 part of caoutchouc are to be dissolved in separate vessels, in ether free from alcohol, applying a gentle heat. When fairly dissolved, the 2 solutions are to be mixed. If the glue be thinned by the admixture of ether, and applied as varnish to leather, it renders a joint or seam water-tight.

VARNISHES.

LAC VARNISH.—Five parts of lac, 1 of turpentine, dissolve in 5 times its weight of alcohol; keep warm until fluid, then strain.

SPAR VARNISH.—Boiled oil and resin.

GOLD VARNISH.—Turmeric, 1 drachm; gamboge, 1 dr; oil of turpentine, 1 quart; shellac, 5 ounces: sandarach. 5 ounces; dragons-blood, 7 drachms; with occasional shaking, for 14 days in a warm place, set it aside to fine and pour off the clear.

VARNISH FOR IRON.—Dissolve in 2 pounds of tar-oil 1/2 pound asphaltum, 1/2 pound of powdered resin, mix hot and apply cold.

Varnish for Metals.—Dissolve 1 part of bruised copal in 2 parts of strong alcohol. It dries very quickly.

OIL VARNISH.—Dissolve resin in turpentine to about the consistency of treacle; add 2 pints of linseed-oil to 1 of resin and turpentine.

VARNISH FOR WOOD PATTERNS.—Gum-shellac, 3 ounces; and resin, 1½ ounce; dissolved in a pint of wood naphtha.

Varnish for Plaster Casts.—A quarter of an ounce of soap is dissolved in a pint of water, and an equal quantity of wax afterwards incorporated. The cast is dipped in this liquid, and after drying a week is polished by rubbing with soft linen. The surface produced in this manner approaches the polish of marble. When intended to resemble bronze, a soap is used, made of linseed-oil and soda colored by the sulphates of Copper and Iron.

VARNISH FOR IRON AND STEEL.—Clear grains of mastic, 10 parts; camphor, 5 parts; sandarach. 15 parts; and eleni, 5 parts; dissolved in a sufficient quantity of alcohol, and apply without heat. This varnish will retain its transparency, and the metallic brilliancy of the articles will not be obscured.

BLACK VARNISH.—Heat to boiling, 10 parts of linseed-oil varnish with burnt umber, 2 parts, and powdered asphaltum, 1 part. When cooled, dilute with spirits of turpentine as required.

A VARNISH TO GILD WITH, WITHOUT GOLD—Take half a pint of spirits of wine, in which you dissolve 1 drachm of saffron, and half a drachm of dragon's-blood, both previously well pulverized together. Add this to a quantity of Shell-lac varnish, and get it on fire with 2 drachms of aloes.

A VARNISH FOR FASTENING THE LEATHER ON TOP ROLLERS IN FACTORIES.—Dissolve 234 ounces of Gum Arabic in water, and so much isinglass dissolved in brandy and it is fit for use.

IMITATION GOLD VARNISH.—As a substitute for the expensive "gold varnish" 1/2 gallon of turpentine, 1/2 a gill of aspaltum, 2 ounces of yellow aniline, 4 ounces of umber, 1 gallon of turpentine varnish, and 1/2 pound of gamboge, mixed and boiled for ten hours. This is said to have as good an effect as the gold varnish and is very cheap.

ENAMELS.

WHITE ENAMEL.—Potash 25 parts; arsenic, 14 parts; glass, 13 parts; salt-petre, 12 parts; flint 5 parts; and lith-arge, 3 parts.

BLACK ENAMEL.—Clay, 2 parts; protoxide of Iron 1 part.

BLUE ENAMEL.—Fine paste, 10 parts; Nitre, 3 parts; color with cobalt.

GREEN ENAMEL.—Frit, 1 pound; oxide of Copper, 1/2 ounce; red oxide of Iron, 12 grains.

YELLOW ENAMEL.—White lead, 2 parts; alum, white oxide of Antimony, and sal-ammoniac, each 1 part.

GELATINE GLUE.—If gelatine which has been swelled in cold water, be immersed in linseed-oil and heated, it dissolves and forms a glue of remarkable tenacity which when once dry perfectly resists dampness, and two pieces of wood joined by it will separate any where else rather than at the joint, ordinary glue may be thus dissolved, and sometimes a small quantity of red-lead in powder is added.

MARINE GLUE.—India-Rubber, 1 part; coal-tar naphtha 8 to 10 parts; shellac, 15 to 20 parts; melted together. Use hot. Glue dissolved in skimmed milk will resist the action of moisture; also glue softened with boiled oil or resin, and its weight of Iron oxide added.

WATER-PROOF GLUE.—Boil 8 parts of common glue with about 30 parts of water, until a strong solution is obtained, add 4½ parts of boiled linseed-oil and let the mixture boil 2 or 3 minutes, stirring it constantly.

ETHER GLUE.—An excellent glue is made by dissolving le in nitric ether; this fluid will only dissolve a certain amount of glue, consequently the solution cannot be made too thick. The glue solution obtained has about the consistency of molasses, and is doubly as tenacious as that made by hot water. If a few pieces of caoutchouc cut into scraps the size of buck-shot be added and the solution be allowed to stand a few days, being frequently stirred, it will be all the better, and will resist dampness twice as well as glue made with water.

LIQUID GLUE.—Glue, water, and vinegar, each 2 parts. Dissolve in a water bath, then add alcohol, 1 part.

PARCHMENT.—Parchment shavings, 1 pound; water, 6 quarts. Boil until dissolved, then strain and evaporate slowly to the proper consistency.

POLISHING COMPOUNDS.

PASTE FOR CLEANING METALS.—Oxalic acid, 1 part; rotten stone, 6 parts. Mix with equal parts of train-oil

and spirits of turpentine.

To CLEAN BRASS.—Brass that has not been gilt or lacquered may be cleaned by washing with alum boiled in strong lye, in proportion of an ounce to a pint; afterwards rub with strong tripoil.

Polish for Silver, Gold, Brass and Glass.—Take 5 pounds of the best Spanish whiting, and with it, mix 3 ounces of alcohol, and then wet to the consistency of dough, make into cakes and dry.

CLEANING SILVER, GLASS, ETC.—Emersons compound for polishing and cleaning glass, silver-plate, tinware and surfaces that permit only slight friction and but little action, consists of water 4 onuces; carbonate of ammonia 1 ounce. When dissolved add 16 ounces of Paris white, with

aniline for coloring. This forms a solid, as the Paris white consists of white lead, all who purchase this compound should beware of using it upon the inside of culinary vessels.

TO FRENCH POLISH FURNITURE.—For the polish take 1 pint of spirits of wine, add 1/2 ounce gum shellac, 1/2 ounce seed lac, 14 ounce gum sandarac; submit the whole to a gentle heat, frequently shaking it until the gums are dissolved, when it is fit for use. Make a roller of list, put a little of the polish upon it, and cover that with soft linen rags which must be lightly touched in cold-drawn linseedoil. Rub the wood in a circular direction (not covering too large a piece at one time) until the pores of the wood are filled up; after this rub in the same manner spirits of wine with a little of the polish added to it.

Patent Leather Polish. —A splendid polish for patent leather, which is used as a blacking in the ordinary way and requires no brushes for polishing; is made by boiling well together 1/2 pound brown sugar, 1 ounce gum-arabic and 2 pounds of ivory black. Allow this mixture to cool and become settled and then bottle it.

For Holes in Castings. -Sal-ammoniac, 2 parts; sulphur in powder, 1 part; powdered iron turnings, 80 parts. Make into a thick paste. The ingredents composing this cement should be kept separate and not mixed until required for use.

'TO KILL KNOTS.—Cover them with fresh slacked lime for 24 hours; scrape lime off and lay on a coat of red and white lead mixed with glue-size. Pumice-stone when dry and lay on some paint.

FILES (RECUTTING).—Lay dull files in diluted sulphuric acid until they are bit in deep enough.

WATCH-MAKERS OIL, WHICH NEVER CORRODES OR THICKENS -Place coils of thin sheet lead in a bottle of olive-oil, expose it to the sun for a few weeks, and pour off the clear

French Polish.—Five ounces of naphtha, 1 ounce of shellac, 1 drachm of myrrh, 10 grains of isinglass, 6

drachms of olive-oil.

BRONZING, OR BRONZING LIQUID. - Sulphate of Copper, 1 ounce; sweet spirits of nitre, 1 ounce; water, 1 pint. Mix

In four or five days it will be fit for use. well.

Brown Tint for Iron and Steel. - Dissolve, in 4 parts; of water, 2 parts of crystallized chloride of iron, 2 parts of chloride of antimony, and 1 part of gallic acid, and apply the solution with a sponge or cloth to the article, and dry it in the air. Repeat this any number of times, according to the depth it is desired to produce. Wash with water and dry, and finally rub the article over with boiled linseedoil. The metal thus receives a brown tint and resists moisture. The chloride of antimony should be as little acid as possible.

Browning for Gun Barrels.—Tincture of muriate of iron, 1 ounce; nitric ether, 1 ounce; sulphate of copper; 4 scruples; rain water, 1 pint. If the process is to be hurried, add 2 or 3 grains of oxymuriate of mercury. When the barrel is finished, let it remain a short time in lime water, to neutralize any acid which may have penetrated; then rub it well with an iron wire scratch-brush.

Bronzing Fluid for Guns.—Nitric acid, sp. gr. 1, 2; pure nutric ether, alcohol, muriate of iron, each 1 part. Mix, then add sulphate of copper 2 parts, dissolved in water 10 parts.

PATINA ANTIQUA BRONZE.—Bronze of a good quality acquires, by oxidation, a fine green tint. Corinthian brass receives, in this way, a beautiful clear, green color. This appearance is imitated by an artificial process, called bronzing. A solution of sal-ammoniac and salt of sorrel in vinegar is used for bronzing metals, any number of layers may be applied, and the shade becomes deeper in proportion to the number applied. For bronzing sculptures of wood, plaster figures, etc. etc., a composition of yellow ochre, Prussian blue, and lamp-black, dissolved in water is employed.

NON-CONDUCTING COVERING FOR STEAM-BOILERS AND PIPES.—Make a thin paste of boiling water and flour, then stir in as much sawdust as it can hold together. After drying it will adhere to iron when slightly warmed, after which several coats may be applied in succession. It may be made water-proof by painting with coal-tar.

FLOUR PASTE.—To make paste that will keep a long time mix with each 100 pounds of flour; 5 pounds of alum, 8 ounces of sulphate of lime, and 2 ounces of oil of sassafras.

Parting Sand.—Burnt sand scraped from the surface of castings.

LOAM. - Mixture of brick, clay, and old foundry sand.

BLACKENING FOR MOULDS.—Charcoal powder; or, in some instances, fine coal-dust.

BLACK-WASH. - Charcoal, plumbago, and size.

To Soften Horn.—Take 1 pound, of wood-ashes, add 2 pounds of quick-lime, put them into a quart of water, let the whole boil until reduced to 1-3, then dip a feather into it. if the plume comes off on drawing it out, then it is boiled enough; when settled filter it off, and in the liquor, add shavings of horn, let them soak for 3 days, then rubbing oil on your hands work the horn into a mass, and print or mould it in what ever shape you want.

EASY WAY OF CLEANING THE HANDS FROM DYES ETC.— Take a small quantity of pot-ash or pearl-ash in your hand, pour into it a small quantity of water, rub it well all over your hands with a little sand, then wash it off, take in your hands a small quantily of chemic (chloride of lime), pour a little water into it, and rub it well on the hands in a semi-liquid state; wash the hands well in water, and they will be clean. If not perfectly clean, repeat the operation.

PRESERVATIVE FOR STEEL.—Caoutchouc, 1 part; turpentine, 16 parts; and boiled oil, 8 parts; well mixed and boiled together, caoutchouc should first be dissolved in the turpentine by gentle heat, and the boiled oil added, it should be applied with a brush, and may be removed by turpentine.

To Prevent Iron from Rusting.—Warm it, then rub with white wax; warm again to allow the wax to prevade the entire surface, or immerse the iron in boiled linseed-oil, and allow it to dry upon the metal.

BRAZING.—The edges filed or scraped clean and bright, covered with spelter and powdered borax, and exposed in a clear fire to a heat sufficient to melt the solder.

MIXTURE FOR WELDING STEEL.—One part of sal-ammoniae and 10 parts of borax, pounded together and fused until clear, when it is poured out, and when cool reduce to powder.

ETCHING SOLUTION FOR IRON AND STEEL.—Take 4 of nitric acid, 2 of sal-ammoniac, 1 of sulphate of copper, and 72 parts water. This is by weight.

WATER ANNEALING.—Heat the steel to a red heat, and let it lie a few minutes, until nearly black hot, then throw it into soap suds. Steel in this way, may be annealed softer than by putting in the ashes on the forge.

EVERLASTING PASTE.—Dissolve half a teaspoonful of alum in a pint of water; when it is cold, for it should be heated when the alum is mixed with it, stir in flour enough to make it about as thick as rich cream; do not leave a lump in it; stir in as much powdered rosin as will lie on a cent piece. Put a saucepan on the stove, put a teacupful of boiling water in it, then stir in the mixture; stir it constantly to keep it from burning. Add a few drops of winter-green. When it is about as thick as mush take it from the fire, put it in a jar or glass can and set it where it will be cool. It will become hard, and when needed for use take out a little and soften it with warm water; it will only take a minute or two to do this. This paste will keep a year at least.

STAINING WOODS.

Rosewood.—Boil 8 ources of logwood in 3 pints of water until reduced to 1/2; apply it boiling hot 2 or 3 times, let-

ting it dry each time. Put in the streaks with a camel's hair brush dipped in a solution of copperas and verdigris in a decoction of logwood.

LIGHT MAHOGANY.—Brush over the surface with diluted nitrous acid, and when dry apply with a soft brush the following: Four ounces of dragon's blood, 1 ounce of carbonate of soda, 3 pints of alcohol. Let it stand in a warm place, shake it frequently and then strain.

To STAIN MUSICAL INSTRUMENTS.—Boil 1 pound of ground Brazil wood in 3 quarts of water for 1 hour; strain it, then add $\frac{1}{2}$ an ounce of cochineal; boil $\frac{1}{2}$ hour longer. This makes a crimson stain.

EBONY.—Wash the wood several times with a solution of sulphate of iron; let it dry, then apply a hot decoction of logwood and nutgalls. When dry wipe it with a wet sponge; and when dry again polish it with linseed-oil.

PURPLE.—Boil a pound of chip logwood in 3 quarts of water for an hour; then add 4 ounces of alum.

BLUE.—Boil 4 parts of alum with 85 parts of water.

To IMITATE EBONY.—Infuse gall-nuts in vinegar wherein you have soaked rusty nails; then rub your wood with this; let it dry, polish and burnish.

TO PREVENT LOGS AND PLANKS FROM SPLITTING.—Logs and planks split at ends because the exposed surface dries faster than the inside. Saturate muriatic acid with lime, and apply like whitewash to the ends. The chloride of calcium formed attracts moisture from the air, and prevents the spliting.

TURNING OR CUTTING METAL WITH PETROLEUM.—A machinist has discovered that by keeping his turning tools constantly wetted with petroleum, he was able to cut metals and alloys with them, although when the tools were used without the oil, their edges were turned and dulled. The hardest steel can be turned easily if the tools be thus wet with a mixture of 2 parts of petroleum with 1 part of turpentine.

WATER-PROOF BOOTS.—The following is said to have been used by the New England fishermen for over a century: Tallow 4 ounces; rosin and bees-wax, of each 1 ounce; melt together in a gentle heat, and add an equal bulk of neats-foot oil. This is first melted and applied to the boots, rubbing it in before the fire; it will make them soft, and at the same time water-proof.

TRACING PAPER.—Nut-oil, 4 parts; turpentine, 5 parts; mix and apply to the paper, then rub dry with flour and brush it over with ox gall.

TRACING PAPER.—A very good tracing-paper may be made by saturating with a camel-hair pencil the finest tis-

sue paper with the following mixture:-Half an ounce of the balsam of Canada, to one ounce of the spirits of turpentine, shaken well together in a two ounce bottle, it requires no heat, When covered with the mixture, hang the paper on a line to dry; then wash in like manner the other side.

Paper for Draughtsmen etc.—Powdered tragacanth, 1 part; water 10 parts. Dissolve and strain through clean gauze, then lay it smothly upon the paper, previously stretched upon a board. This paper will take either oil or water color.

Transferring Paper.-Take half a sheet of very fine bank post paper, lay it on a clean place and rub it well with the scrapings of red chalk; a small bit of sponge is good for this purpose. Apply the chalk, until the paper is all one color, then with a piece of clean old muslin, rub the greater part of the color from the surface. The color may be renewed occasionally as the marking becomes faint.

BLUE PRINTS FOR COPYING MECHANICAL DRAWINGS ETC.

Take 1% ounces pure Ammonia Citrate of Iron, 8 ounces distilled water or pure rain water. Pure Ferricyanide (Red Prussiate of Potash), 114 ounces, 8 ounces distilled water. Mix separately and unite. Keep in yellow bottle or in the dark.

To sensitize paper, moisten it uniformly with the liquid by means of a soft clean camel hair brush and suspend in a dark room to dry. Keep from light.

To print the design or drawing put the sensitized paper on a flat surface and then lay the drawing over it and cover with a pane of glass. Expose to the Sun for 15 to 30 minutes (according to the brightness of the Sun) and then rinse thoroughly with pure rain or distilled water.

FACTS FOR FARMERS.

Table Showing the Quantity of Garden Seeds Required to Plant a Given space.

DESIGNATION. Asparagus.

Roots.

French Beans, pole, large. 1 " small. 1 "

Beets.

SPACE AND QUANTITY OF SEEDS. 1 oz. produces 1000 plants and requires a

bed 12 feet square. 1000 plant a bed 4 ft. wide, 225 feet long. Eng.dwarf beans. 1 qt. plants from 100 to 150 feet of row. 250 or 350 of row. 1

66 100 hills.

300 " or 250 feet of row. 10 lbs. to the acre: 1 oz. plants 150 feet of row.

Broccoli and Kale 1 oz. gives 2500 plants, and requires 40 square feet of ground.

Early sorts same as broccoli, and requires Cabbage. 60 square feet of ground. Canliflower. The same as cabbage. 1 oz. to 150 of row. Carrot. 7000 plants, and requires 8 1 oz. gives Celery. square feet of ground. 1 oz. for 150 hills. Cucumber. 1 oz. sows a bed 16 feet square. Cress. 1 oz. gives 2000 plants. Egg Plant Endive. 1 oz. 3000 " rea'i'es 80 ft. of ground 46 Leek. 1 oz. 2000 60 .. " seed bed of 120 ft. Lettuce. 1 oz. 7000 1 oz. for 120 hills. Melon. Nasturtium 1 oz. sows 25 feet of row. 200 Onion. 1 oz. 66 Okra. ٠. 200 1 oz. Parsley. 1 oz. • • 200 Parsnip. 1 02. .. 250 1 oz. gives 2500 plants. Penners. 1 quart sows 120 feet of row. Peas. 1 oz. to 50 hills. Pumpkin. Radish. 1 oz. to 100 feet. Salsify. 1 oz. to 150 " of row. 1 oz. to 200 Spinage. Squash. 1 oz. to 75 hills 1 oz. gives 2500 plants, requiring seed bed of Tomato. 80 feet. 1 oz. to 2000 feet. Turnip. Water melon, 1 oz. to 50 hills.

Table Showing the Number of Plants, Hills, or Trees Contained in an Acre at Epual Distances Apart. From 3 Inches up to 66 Feet.

	Distan apar				No. of plants.		stance	e			No. of olants.
3 1	inches.	by.	3 iı	iches.	696,960	4	feet.	by	1	foot	10.890
4	6.6		4	4.6	392.040	4	+ 4		$2 \cdot$	feet	5.445
6	4.4	16	$\bar{6}$	6.6	174.240	4	6.	••	3		3.630
9	4.6		9	4.4	77.440	4	6.6	4.6	4	+ 4	2.722
1 :	foot	٠.	1	foot	43.560	41	/2 "	4.4	41/2	4.6	2.151
11/	2 feet	• •	11/9	feet	19.360	5	- • •	66	1	foot	8.712
2	• • • •	• •	1	foot	21.780	5	6.	4.6	2	feet	4.356
2	**	• •	2	feet	10.890	5	+ 6	4.6	3	• •	2.904
21	5	• •	215		6.960	5	4.6		4	• •	2.178
3	• • •	• •	1 -	foot	14.520	5		••	5	• •	1.742
3	+ 4		2	feet	7.260	51	/9	4.4	51/2		1.417
3	4.6		3	**	4.840	6		6.4	6	6.	1.210
31	6 "		315	4.0	3.555	61	6	• •	61/2		1.031

Distance . apart.	No. of plants.	Distance apart.	No. of plants.
7 feet by 7 feet	881	17 feet by 17	150
8 " " 8 "	680	18 " " 18	134
9 9	537	19 19	120
10 " " 10 "	435	20 20	108
11 " " 11 "	361	25 25	69
12 12	302	30 30	48
13 " " 13 "	257	33 33	40
14 " " 14 "	222	40 40	27
15 " " 15 "	193	50 50	17
16 " " 16 "	170	60 60	12
161/2" " 161/2"	160	66 66	10

Table Showing the Numtber of Seeds in one Pound, and Weight per Bushel.

NAME.	No. of seeds	No. of lbs.,
	per pound.	per bushel.
Wheat.	10,500	58 to 64
Barley.	15,400	48 to 56
Oats.	20,000	38 to 42
Rye.	23,000	56 to 60
Vetches.	8,500	60 to 63
Lentils.	8,200	58 to 60
Beans.	600 to 1,300	60 to 65
Peas,	1.800 to 2,000	60 to 65
Flax seed.	108,000	50 to 60
Turnip seed.	155,000	50 to 56
Rape seed.	118,000	50 to 56
Mustard (white).	75,000	57
Cabbage seed.	128,000	52
Mangel-wurzel.	24,600	20 to 24
Parsnip seed.	97,000	14
Carrot-seed.	257,000	9
Lucern-seed.	205,000	58 to 60
Clover (red).	249,600	60 to 63
" (white).	686,400	
Dra arroad (sevennich)		59 to 62
Rye-grass (perennial)	334,000	20 to 28
" (Italian).	272,000	13 to 18
Sweet vernal grass.	923,000	8
Buck-wheat.	25,000	42 to 52

Table Showing Quantity per Acre when Planted in Rows or Drills.

Broom Corn.	1	to 11/2	bushel.	Onions.	4 to 5	pounds
Beans.		to 2		Carrots.	2 to 210	4.6
Peas.	11/0	to 2	4.6	Parsnips.	4 to 5	• •
Pen-nuts	1 -	to 2	44	Reets	4 10 6	

Table showing the quantity of seed required to the acre.

Designation.	Quantity of Seed.	Designation.		ant	
Wheat.	11/4 to 2 bu.	Broom Corn.	1 to		bus.
Barley.	11/2 " 21/2 "	Potatoes.	5 "	10"	66
Oats.	2 " 4 " "	Timothy.	12 "	24	qts.
Rye.	1 " 2 "	Mustard.	8 "	20	***
Buckwheat.	34 " 11/3 "	Herd Grass.	12 "	16	66
Millet.	1 " 11/3 "	Flat Turnip.	2 "	3	lbs.
Corn.	14 " 1 "	Red Clover.	10 "	16	66
Beans.	1 " 2 "	White Clover.	3 "	4	6.6
Peas.	21/2 " 31/2 "	Blue ,Grass.	10 "	15	66
Hemp.	1 " 11/0 "	Orchard "	20 "	30	66
Flax.	1/2 " 2" "	Carrots.	4 "	5	4.6
Rice.	2" " 21/2 "	Parsnips.	6 "	8	"

NUMBER OF YEARS SEEDS RETAIN THEIR VITALTY.

Vegetables.	У	ears	8.	Vegetables.		years	١.
Cucumber.	8	to	10	Asparagus.	2	to	3
Melon.	8	4.4	10	Beans.	2		3
Pumkin.	8	6.6	10	Carrots.	$\bar{2}$	4.6	3
Squash.		6+	10	Celery.	$\bar{2}$	**	3
Brocoli.	855555	6.6	6	Corn (on cob).	2	**	
Cauliflower.	5	6.6	6	Leek.	2		3
Artichoke.	5	6.6	6	Onion.	2	••	3
Endive.	5	44	6	Parsley.	2	++	3
Pea.	5	6.6		Parsnip.	$\frac{2}{2}$	6.6	3
Radish.	4	6.6	6 5	Pepper.	2	66	3
Beets.	3	44	4	Tomato.	2	••	3
Cress	3	6.6	.4	Egg Plant.	1	••	2
Lettuce.	4 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6		4	HEDD	2		
Mustard.	3	4.6	4	HERB	٠.		
Okra.	3	64	4	Anise.	3	to	4
Rhubarb.	3	4.4	4	Caraway.	2		
Spinach	3	6.6	4	Summer Savory.	1	4.4	2
Turnips.	3	4.	5	Sage.	$\bar{2}$	**	3

Amount of Seeds, Bulbs, etc., Required to Plant One Agre.

Barley, Beans, bunch, in drills 21/2 feet	21/2 bus.
Beans, poles, lima, 4×4 feet	20 ats.
Beets, drills 21/2 feet	9 lbs.
Broom-corn in drills	121/2 "
Cabbage in beds	12 oz.
Cabbage in frames	4 "
Clover, large, red	16 lbs.
Clover, large, with timothy	12 "
Corn, sugar	10 qts.

Corn, field			8	
Cucumbers in hills			. 8	
Grass, timothy with clover .			. 6	41
Grass, timothy without cloves	г.		. 10) "
Grass, orchard			25 to 30	
Grass, red-top			20 to 25	
Grass, blue		•	. 28	
	•		. 20	
Grass, rye				
Lawn grass			. 25	
Melons, water, 8×8 feet .			. §	
Oats			. 2	
Onions in beds for sets .			. 50	lbs.
Onions in rows for large bulb	os .		. 7	**
Pumpkins in hills 8×8 feet			,	ats.
Peas in drills, low varieties			5	bus.
Peas in drills, tall varieties			1 to 1	1/2 ''
Peas, broadcast		. •		
				66
Potatoes			. 9	10/
Rye, broadcast				3/4
Rye, drilled				1/2 "
Turnips in drills 2 feet .			. :	
Turnips, broadcast			. :	3 "
Wheat in drills			. 1	14 bus.
Wheat broadcast				,

Table showing the number of hills or plants on an acre of land, for any distance apart, from 10 inches to 6 feet—the lateral and longitudinal distances being unequal,

	10 in.	12 in.	15 in	18 in	20 in.	2 ft.	2½ ft.	3 ft.	3½ ft	4 ft.
	62626							Ī		
	52272									
15 "	41817	34848	27878							
18 "	34848	29040	23232	19360						
	31363									
	26136									
21/2"	20908	16424	13939	11616	10454		6969			
3 "	17424	14520	11616	9680	8711		5808			
31/2"	14935 13068	12446	9953				4976			
4 "							4356			
5 "	11616						3872			
5 "	10454						3484			
51/2" 6 "	9504					3960	3168	2640	2263	1980
6 "	8712	7260	5808	4840	4356	3630	2904	2420	2074	1865

TO PROTECT NEWLY PLANTED CORN.

To prevent the corn from being destroyed and eaten by chickens, birds, or insects before it grows through the surface of the soil, prepare the seed before pianting by sprinkling a sufficient portion of coal tar, (procured at the gas manufactory), through it, stirring so that a portion

will adhere to each grain; then mix among the corn some ground plaster-of-Paris, which will prevent the tar from sticking to the fingers of those who drop the corn, and vegetation will be promoted thereby. The tar and plaster will not injure the corn so as to prevent its growing, by being kept some days after it is so mixed together.

TO PROTECT CORN STALKS FROM MICE.

Sprinkle from four to six bushels of dry white sand upon the root of the stalk before the thatch is put on. The sand is no detriment of the corn, and stacks thus dressed have remained without injury. So very effective is the remedy, that nests of dead young mice have been been found where the sand have been used, but not a live mouse could be seen.

MEASURE OF AN ACRE PLOT.

Either of the following measure include about an acre plot.

3	by	531/8	Rods.	1 8	by	20	Rods.
4	66	40	44	9	"	177/2	4.6
5	66	32	4.6	10	16	16	16
6	6.4	262/3	4.4	11	+4	14 6-11	4.6
7	6.6	22 6-7	4.6	12	6.6	131/2	6.6
	12 R	ods 10 ft.	and 81/2 in	square	make	an Acre	

Square Feet and Feet Square in Fractions of an Acre.

Fractions of an Acre.		Ft. Sq.	Fractions of an Acre.	Sq. Ft.	Ft. Sq.
1-16 1/8 1/4 1/3	27221/2 5445 10890 14520	521/ ₂ 733/ ₄ 1041/ ₂ 1201/ ₂	1/2	21780 43560 87120 130680	1471/2 2081/4 2951/4

HILLS IN AN ACRE OF LAND.

			Hills.		Hills.
40	feet	apart.	27	8 feet apart.	680
35	4.4	~ "	35	6 " "	1210
30	66	66	48	5	1742
35 30 25	6.6	4.4	69	31/2"	3556
20	44	44	108	3 4 4	4840
. 15	6.6	66	193	21/2"	6969
12	66	6.6	302	2'-". "	10890
10	66	66	435	ī " "	43560

TO ESTIMATE GRAIN CROPS PER ACRE.

Frame together four light sticks, measuring exactly a foot square inside, and with this in one hand, walk into the field and select a spot of fair average yield, and lower the frame square over as many heads as it will inclose, and

shell out the heads thus enclosed carefully, and weigh the grain. It is fair to presume that the proportion will be the 43560th part of an acre's produce. To prove it go through the field and make ten or twenty similar calculations, and estimate by the mean of the whole number of results. It will certainly enable a farmer to make a closer calculation of what a field will produce than he can by guessing.

Comparative Yield of Various Grains, Vegetables and Fruits.

	Lbs		Lbs.,
	per Acre.		per Acre.
Hops.	,442	Grass.	7,000
Wheat.	1,260	Carrots.	6,800
Barley.	1,600	Potatoes.	7.500
Oats.	1,840	Apples.	8,000
Peas.	1.920	Turnips.	8,420
Beans.	2,000	Cinque foil grass.	9,600
Plums.	2,000	Vetches, green.	9,800
Cherries.	2,000	Cabbage.	10,900
Onions.	2,800	Parsnips.	11,200
Hay.	4,000	Mangel Wurzel.	22,000
Pears.	5,000		

CONTENTS OF FIELDS AND LOTS.

To assist farmers in making an estimate of the amount of land in different fields.

220	feet	by	198		land		
440	6.6	6.6	99	**	**	" 1	- 4 4
110	+6	66	369	4.6	"	" 1	
60	6.6	6 .	726	44	"	" 1	4.6
120	6.6	6.	363	4.6	"	1	٠.
240	6.6	44	1811/2	44	"	. 1	6.6
200	44	66	108,9	44	44	1/9	44
100	6.	6.6	145 %	44		. 1/9	
100	44	66	108_{12}^{9}	4.6	"	1/4	

A PRACTICAL RULE FOR LAYING PIPE

FOR DR	AINING	ì L	AND.	Dist	ance.
Soils.	Depth	of	f Pipe.		art.
Coarse, Gravel Sand.	4 feet	6	inches,	 60	feet.
Light Sand with Gravel.	4 "				64
Light Loam.	3 "	6	6.	 33	6 6
Loam with Clay.	3 "	2	66	 21	• •
. " Gravel.	3 "	3	**	 27	• 6
Sandy Loam.	3 "	9	• •	 40	6.
Soft Clay.	2 "	9	44	 21	
Stiff Clay.	2 "	6	**	 15	• •

Greatest Fall of Rain is 2 inches per hour—54308.6 gallons per acre.

Showing Number of Acres drained by different sizes of tile, the rainfall being considered as equal to one-half inch in depth each 24 hours.

Rat	e of	Inclin	ation	1	1	ACRE	S DR.	AINE	D.	
Fee	et to	one of	rise.	2-in. Tile.	3-in. Tile.	4-in. Tile.	6-in. Tile.	8-in. Tile.	10-in. Tile.	12-in Tile.
1 for 11 11 11 11 11 11 11 11 11 11 11 11 11	oot	in 10 20 25 30 40 40 50 60 70 80 96 100 150 200 225 300 400 600 800 1.00 1.00 1.00	feet. "" "" "" "" "" "" "" "" "" "" "" "" ""	$\begin{vmatrix} 6.6 \\ 4.7 \\ 4.2 \end{vmatrix}$	18.9 13.0 11.4 10.9 9.4 7.6 6.9 6.5 5.7 4.5 3.9 3.5	26.8 24.0 21.9 19.0 17.0 15.6 14.5 13.4 12.6 11.9 9.5 8.2	66.22 61.55 53.3 47.7 43.4 39.9 37.2 35.0 26.6 22.8 20.4 18.4 16.5 14.8 13.3	126.4 109.6 98.0 90.0 83.0 77.0 72.5 69.2 56.0 48.0 43.4 38.2 34.6 30.1 28.0 24.0 21.2	190.5	269.0 246.0 228.1 213.0 200.5 154.4 132.5 117.0 90.7 81.6 74.0 65.0 47.0

Showing carrying capacity of different sizes of tile in Gals.

	Carrying Capacity—Gallons per Minute.											
	ze of ipes.	11/2 in. fall per 100 ft.	3 inch fall per 100 ft.	6 inch fall per 100 ft.	9 inch fall per 100 ft.	1 foot fall per 100 ft.	11/2 ft. fall per 100 ft.	2 foot fall per 100 ft.	3 foot fall per 100 ft.			
21/	2 in.	14	20	28	34	40	49	55	68			
3		21	30	42	52	60	74	85	104			
4 5	4.6	36	52	76	92	108	132	148	184			
5	• 6	54	78	111	134	159	192	219	269			
6	_ 64	84	120	169	206	240	294	338	414			
8	44	144	208	304	368	432	528	592	736			
9	4.	232	330	470	570	660	810	930	1140			
10	6.6	267	378	563	655	803	926	1340	1613			
12	6.6	470	680	960	1160	1360	1670	1920	2350			
15	66	830	1180	1680	2040	2370	2920	3340	4100			
18	44 .	1300	1850	2630					6470			
					3200	3740	4600	5270				
20		1760	2450	3450	4180	4860	5980	6850	8410			
24		13000	4152	5871	7202	8303	10021	11743	14466			

THE NUMBER OF RAILS, RIDERS AND STAKES REQUIRED FOR EVERY TEN RODS OF ZIGZAG FENCE.

t of	ght	of el.	Number	r of Ra h 10 Ro	ils for ds.	of	of ste).
Length Rail.	Deflect from ri line.	Length	Rails righ.	Rails nigh.	en Rails high.	mber Stakes.	umber ers (sing
Ft.	Ft.	Ft.	Five	Six	Seve	Num	Ride
12 14 161/ ₂	6 7 8	8 10 12	103 83 69	123 99 84	144 116 95	42 34 28	21 17 14

For longer distances than 10 rods the proper number of rails, etc., may be computed by multiplying. For instance: If 50 rods of fence, multiply the above number by 5; if for 100, multiply by 10, etc. The like rule will apply to the next.

THE NUMBER OF RAILS AND POSTS REQUIRED TO EACH TEN RODS OF POST AND RAIL STRAIGHT FENCE.

of .	of	Number of Rails for each 10 Rods.								
Length Rail	Length Pane	umber o Panels.	umber Posts.	e Rails Iigh.	Rails ligh.	n Rails Iigh.	it Rails Tigh.			
Ft.	Ft.	Z	Ź	Five	Six	Seven	Eigh			
10	8	205/8	21	103 83 69	123	144	165			
12	10	161/2	17	83	99	116 95	133			
10 12 14 161/2	12 141/ ₂	133/4	14 12	57	99 84 69	81	165 133 109 93			

HANDY MECHANICAL,

Contents of Bins and Granaries.

		ontents	01 6	ins and	Grai	iaries.		
Width and	1 Ft	. high.	2 Ft	. high.	3 Ft.	high.	4 l t.	high.
Length in feet.	Sti' k'n.	Heap.	Sti'- k'n.	Heap.	Sti'- k'n.	Неар.	Sti'- k'n.	He'p.
33 " 45 67 88 33 " 90 44 " 55 44 " 78 89 44 " 105 55 " 77 8 99 55 " 10 66 " 10	71 91 12 14 17 19 14 12 11 11 11 11 11 11 11 11 11 11 11 11	$\begin{array}{c} 577 \\ 287 \\$	14½ 19½ 29 33½ 343½ 48½ 48½ 48½ 51½ 51½ 56½ 40½ 40½ 40½ 1112½ 80½ 1112½ 1125½	11-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1	213 29 14 3 5 5 7 5 7 5 7 5 7 5 7 5 7 5 7 5 7 5 7	171 223 403 403 403 52 57 57 67 77 86 69 106 69 106 69 1127 1127 1138 1138 1148 1154 1154 1169 1173 1173 1173 1173 1173 1174 1174 1175 1175 1175 1175 1175 1175	511 641 790 1128 896 1128 1443 1641 1732 1156 1156 1156 1156 1156 1156 1156 115	411 511 72 921 447 1022 477 9022 1152 1152 121 108 1234 121 123 124 125 126 126 126 127 127 127 127 128 128 128 128 128 128 128 128 128 128

Contents of Bins and Granaries. (Continued),

Width	5 Ft	. high.	6 Ft	. high.	7 Ft.	high.	8 Ft.	high
Length in feet.	Sti' k'n.	Heap.	Sti'- k'n.	Heap.	Sti'- k'n.	Неар.	Sti'- k'n.	He'p.
5 × 5 5 · · · · · · · · · · · · · · · ·	100) 120) 120) 160) 180) 180) 180) 180) 180) 180) 191 144 181 192 225 192 225 192 235 192 235 193 35 193 35 36 36 36 36 36 36 36 36 36 36 36 36 36	961 11281 1281 1281 1281 1281 1281 1281 1	173½ 202½ 231½ 240½ 231½ 240½ 236½ 270 303½ 405 308½ 444 462½ 462½ 462½ 452½ 452½ 452½ 452½ 6694½	13834 162 18544-1 2084-1 2544-1 2541-1 189 216 243 270 297 324 2462-7 339-1 347-1 339-1 347-1 341-1 34	275 ³ 315 315 393 ³ 4331 4331 4450 445 540 495 566 ¹ 455 680 ¹ 567 ³ 680 ¹ 680 ¹ 781 481	220½ 2522 315346½ 378 288 328 328 326 432 405 445½ 405 4455 4456 450 540 540 540 540 540 540 540 540 540	4111 4623 5653 6171 5781 6361 7771 7773 7773 7773 9253	3291 3701 4152 4982 4623 5111 5653 56783 7403

This table of "Stricken and Heap" bushels is given to the nearest quarter and can be used for deeper bins, than that employed in the table:—Take the contents of half the depth and multiply by 2.

CAPACITY OF BOXES.

A box 16 inches square and 8.4 inches deep, will contain 1 bushel.

A box 16 inches by 8.4 inches wide, and 8 inches deep will contains 1/2 bushel.

A box 8 inches by 8.4 inches wide, and 8 inches deep will contain 1 peck.

A box 8 inches by 8 inches square, and 4.2 inches deep. will contain 1 gallon.

A box 7 inches by 4 inches wide, and 4.8 inches deep, will

contain 1/2 gallon.

A box 4 inches by 4 inches square and 4.2 inches deep, will contain 1 quart.

A box 24 by 16 inches square, and 28 inches deep will con-

tain a barrel (5 bushels shelled corn).

A box 24- by 16 inches square, and 14 inches deep will

contain 1/2 a barrel.

A box 26 by 161/2 inches square, and 8 inches deep, will

contain 1 bushel.

A box 4 feet by 7 inches long, 2 feet 4 inches wide, 2 feet 4 inches deep, holds 20 bushels.

CAPACITY OF A FREIGHT CAR.

A load is nominally 10 tons of 20.000 pounds. The following can be carried: whiskey, 70 bbls., salt, 70 bbls., llme, 70 bbls.; flour, 90 bbls.; eggs, 130 to 160 bbls.; flour, 200 sacks; wood 6 cords; cattle, 18 to 20 head; hogs, 50 to 60; sheep, 80 to 100; lumber, 6,000 feet; barley, 400 bushels; wheat, 340 bushels; flax seed, 360 bushels; apples, 370 bushels; corn, 400 bushels; Irish potatoes, 430 bushels; oats, 680 bushels; bran, 1.000 bushels; butter, 20.000 pounds; 400 bushels of barley; 300 bushels of sweet potatoes; 200 kegs of nails.

TO MEASURE GRAIN IN BINS.

Multiply the length of the bin in inches by the width in inches, and that by the height in inches and divide by 2150 for struck bushels, and by 2748 for heaped bushels. The quotient will be the number of bushels contained in the bins, or—

TO MEASURE GRAIN IN THE GRANARY.

Divide the cubic feet by 56, multiply by 45, and the result will be struck measure in bushels.

TO MEASURE CORN IN CRIB.

Multiply the length, breadth and height together, in feet, to obtain the cubic feet; multiply this product by 4, and strike off the right figure; and the result will be shelled bushels, nearly.

TO MEASURE CORN.

IN COB.—Two heaping bushels of corn on the cob will make 1 struck bushel of shelled corn. Some claim that 1 and ½ bushels of ear will make 1 bushel of shelled corn. Much will depend upon the kind of corn, shape of the ear, size of the cob, etc.

IN CRIB.—To measure corn in a crib, multiply the length of the crib in inches by the width in inches, and that by the height of the corn in the crib in inches and divide the product by 2,748 and the quotient will be the number of heaped bushels of ears. If the crib flares at the sides, measure the width at the top and also at the bottom, add the two sums together, and divide by 2, which will give the mean width,

MEASUREMENT OF HAY.

The only method exact of measuring hay is to weigh it, but the rules given below will be found sufficient for ordinary practical purposes:

To Find the Number of Tons of Meadow Hay in Windrows.—Multiply together the length, breadth and height, in yards, and divide the product by 25. The quotient will be the number of tons in the windrow.

To Find the Number of Tons of Hay in a Mow.--Multiply together the length, height and width, in yards, and divide by 15 if the hay be well packed. If the mow be shallow, and the hay recently placed therein, divide by 18, and by any number from 15 to 18, according as the hay is well packed.

To Find the Number of Tons of Hay in Square or Long Stacks.—Multiply the length of the base in yards by the width in yards, and that by half the height in yards, and divide by 15.

To Find the Number of Tons of Hay in a Load —Multiply together the length, width and height, in yards, and divide the product by 20.

To ascertain the value of a given number of pounds of hay, straw, or other commodity sold by the ton, at a given price per ton, multiply the number of pounds by 1/2 the price per ton, and point off three figures from the right. The result will be the price of the article.

A ton is 100 cubic feet in the mow; that is, when it has settled down and becomes solid. A truss of Hay is, new, 60 pounds, old, 50 pounds, straw, 40 pounds. A load of hay is 36 trusses. A bale of hay is 300 pounds.

TO MEASURE CISTERNS AND CASKS.

Circular Cisterns.—To ascertain the contents of circular cisterns, multiply the square of the diameter in feet by the depth in feet and that product by $\frac{373}{4000}$ for the contents in hogsheads, or by $\frac{373}{2000}$ for barrels, or 478 for the contents in gallons.

Square Cisterns.—To ascertain the contents of square cisterns multiply the width in feet by the length in feet, and that by the depth in feet, and that again by $\frac{19}{160}$ for hogsheads. or $\frac{1}{160}$ for barrels, or 7.4% for gallons. Another and simple method is to multiply together the length,

width, and depth, in inches, and divide by 231, which will give the contents in gallons.

Cask Gauging.—To measure the contents of cylindrical vessels, multiply the square of the diameter in inches by 34, and that by the height in inches, and point off four figures. The result will be the contents in, or capacity, in wine gallons and decimals of a gallon. For beer gallons multiply by 28 instead of 34. If the cask be only partially filled, multiply by the height of the liquid instead of the height of the cask to ascertain the actual contents. In ascertaining the diameter, measure the diameter at the bung and at the head, add together, and divide by 2 for the mean diameter.

TO COMPUTE THE WEIGHT OF CATTLE.

Multiply the girth in inches, immediately back of the shoulders, by the length in inches from the square of the buttock to the point of the shoulder blade, and divide the product by 144, which will give the number of superficial feet. If the animal has a girth of from 3 to 5 feet, multiply the number of superficial feet by 16, which will give the weight of the animal. If the girth is from 5 to 7 feet, multiply by 23, and if from 7 to 9 feet, multiply by 31. If less than 3 feet girth, as in the case of small calves, hogs, sheep, etc., multiply by 11. Of course many circumstances, such as the build of the animal, mode of fattening, condition, breed, etc., will influence the weight, but the above will be found approximately correct.

TO TELL THE AGE OF CATTLE.

A cows horn is generally supposed to furnish a correct indication of the age of the animal. This is not always true. However, for ordinary purposes, the following will

be found approximately correct.

At two years of age a circle of thick matter begins to form on the animal's horns, which becomes clearly defined at three years of age, when another circle or ring begins to form, and so on year after year. Its age, then, can be determined by counting the number of rings and adding two to their number. The rings on the bulls horns do not show themselves until he is five years old, so to the number of rings we must add five to arrive at his age. Unless the rings are clear and distinct this rule will not apply. Besides, dealers sometimes file off some of the rings of old cattle to make them appear younger.

AGE OF SHEEP AND GOATS.

At 1 year old they have eight front teeth of uniform size. At 2 years of age the two middle ones are supplanted by two large ones. At three a small tooth appears on each side. At four there are six large teeth. At five all the front teeth are large and at six the whole begins to get large.

WEIGHT OF A CUBIC FOOT

of various substances, from which the bulk of a load of one ton may be easily calculated:

Ibs.	ibs.
Cast Iron 450	Common Soil, compact, about 124
Water 62	Clay, about
	Brick, about125
Loose Earth, about 95	Stone, about

Legal Weights of Grain, Seed, etc., in Different States.

ARTICLES.	N. Y.	Ohio.	Penn.	Ind.	Wis.	Iowa.	1	Mich.	Conn.	Mass.	R. I.	Ky.	N. J.	Vt.	Mo.	Canada
Wheat, lb.,													60			
Rye.							54		56				56			
Corn.		56		56			56		56			56	56	56	52	56
Oats.	32	32	32		35		32		28				30			
Barley.	48	48		48			44		45			48	48	46	M	
Buckwheat.	48		48	50	42		40	42		46			50	46		
Clover seed.	60	64		60	60	60	- 2	60	-			60	64		M	60
Timothy seed.	40	62		45		45		M		M	-	45				48
Flax seed.		56		56		56		M		M		56	55		M	56
Hemp seed.	44			44		44										
Blue grass seed.	14			14		14		-								
Apples, dried.	22	25			28	24		28 28								22 22
Peaches, "		33		_	28	33		28								22
Coarse salt.		50		50		50				70		50 50			50	56
Fine salt.			83		-	50			-	70		bυ		200	50	56
Potatoes.	60	-		60		66			60		60			60		00
Peas.	60	-		00		00				60		co				60
Beans.	62			60		60	1			60		60				60
Castor beans.	46		1	46		46	İ						-0			
Onions.	57	1		57		57				DU	50		52			
Corn meal.	1	1	1	50	1		1				50			l		

The letter "M" shows the sale in that State is by measure instead of weight.

To reduce cubic feet to bushels, struck measure, divide the cubic feet by 56 and multiply by 45.

VALUE OF FOOD FOR DOMESTIC ANIMALS.

The figures below give the comparative number of pounds of each substance to equal in effect that of any standard food—as, for instance, that of hay.

Good hay, to give a certain nourishment, requires.. 100 fbs.
Good clover hay will give same effect by the use of. 95 "
Rye Straw " " " 355 "
Oat Straw " " " 220 "
Potatoes " " " 195 "

Carrots will	give same	effect by	the use of	280 1	bs.
Beets	•••	A _ 66	60	346	66
Ruta Bagas	44	66	66	262	66
Wheat	66	44	44	43	.6
Peas	44		66	44	66
Beans	66	. 66	46	46	6.6
Rye	"	44	***	49	+ 6
Barley	44	**	"	51	66
Indian Corn	66	4.6	- 66	56	66
Oats	44	4.6	44	59	66
Buckwheat	44	44	66	64	66
Oil Cake	6.6	66	44	64	66

NUTRITIVE QUALITIES OF FODDER.

The proportion of nutritive matter in 100 pounds of the following substances is as follows:

	Flesh Formers.	Fat Formers.
Clover Hayin pounds, Timothy	131/ ₂ 93/ ₄ 10	30 483/4 68
Oats	12 14	61 50
Shorts Buckwheat Bran	$^{10}_{51\!/\!2}$	56 48 21
Potatoes	1/2	14 9

The whole of these amounts may not be digestible, but they serve to give a good idea of their relative value.

CONSUMPTION OF HAY.

The hay consumed by different animals does not vary greatly from three pounds daily for each hundred pounds weight of the animals. The following table is the result of various experiments by different persons, and will be useful for farmers who wish to determine by calculation beforehand, how their hay will hold out for the winter; 500 cubic feet of timothy hay, in a full bay being about one ton.

Working Horses,	3.08 fbs	Steers.	2.84 Tbs
Working Oxen,	2.40 ''	Dry Cows,	2.42 "
Milk Cows (Boussingault's),	2.25 ''	Pigs (Estima	l-
Milk cows (Lincoln's),	2.40 "	ted),	3.00 "
Young growing cattle,	3.08 ''	Sheep,	3.00 "

All the articles enumerated in these food tables are estimated as of good quality. If the fodder he of poor quality, more must be allowed.

RELATIVE VALUE OF DIFFERENT FOODS IN STOCK RAISING.

To produce the same effect as 100 pounds of hay will require of the following articles the number of pounds opposite each:

apposite each		articios	UIIO	II WIII K	or or	pourius
opposite each:					000	
Beets, white	-				669	pounds.
Turnips					469	66
Rye straw					429	-66
Clover, red, uncured					373	"
Clover, red, dry					88	66
Carrots					371	- "
Carrot leaves					135	**
Mangolds					368.5	
Potatoes					350	
Oat straw		,			317	4.6
Lucerne					89	• 6
Buckwheat					78.5	
Corn					62.5	
Oats					59	44/
Barley					58	4.4
Rye					53.5	
Wheat					44.5	
Oilcake, linseed					43	
Peas, dry					37.5	
Beans					28	6 5

FOOD FOR POULTRY.

The table shows the percentage of nutriment in different kinds of food for poultry.

There is in Every 100 Parts by Weight of—	et vi	Warm giving Fatten Materi viz. Fat or Oil.	and ing ial	Bone-making Material, or Mineral sub- stance.	Husk, or Fibre.	Water.
Beans and Peas	25 18	2 6 6	48	2	18	15
Oatmeal	18	6	63	2 2 5	2	9
Middlings Thirds, or Fine Sharps	18	6	53		4	14
Oats	15	6	47	2	20	10
Wheat	12	3	70	2	1	12
Buckwheat	12	6	58	11/2	11	111/2
Barley	11	8	58 60 65	2 2 11/ ₂ 2 1	14	111/2 11- 10
Indian Corn	11		65	1	5	10
Hempseed	10	21	45	2	14	8
Rice	7	A trace		A trace		13
Potatoes	61/2		41	2		501/2
Milk	41/2	3	5	34		863/4

FOOD FOR SHEEP.

The table shows the number of pounds, live weight, and the number of pounds of wool and of tallow, produced by 1,000 pounds of each of the articles named, when used as food for sheep.

KIND OF FOOD.	Increase in weight, Ibs.	Wool pro-	Tallow pro-
Barley Buckwheat Corn Meal, wet Mangel-wurzel, raw Oats Peas Potatoes, raw, with salt Potatoes, raw, without salt Rye, with sait Rye, without salt Wheat	136 120 129 381/2 146 134 461/2 44 133 90 155	111/2 10 131/2 51/4 10 141/2 61/2 61/2 14	60 33 171/2 61/2 421/2 41 121/2 111/2 35 43 591/2

CORN AND HOGS.

A bushel of corn will make 101/2 pounds of pork gross. Then—

•	11011								
When corn costs				Pork costs					
				bushel.	11/2	cents	per	pound.	
	17		4.4	1.4	2			4.6	
	25	4.6	6.6	4.	3	• •	• •	14	
	35	61	4.6	4.6	4	• •	4.0	- 44	
	42	**		4.4	5	***	4.	4.6	
	50	**	4.4	4.6	6	+ 5		+6	
	60		. **	* *	7	1	16	- 44	
	65	4.4			8	**	• •	• 6	

AGES OF ANIMALS.

A. G. E	SOFAN	IMALS.		
Whales, estimated,	1.000 Yrs.	Cow,	20 Yr	s.
Elephant,	400	Deer,	20 "	
Swan,	300 "	Rhinoceros,	/20 "	
Tortoise.	100 ''	Swine.	20 "	
Eagle,	100 "	Wolf.	20 "	
Raven,	100 4	Cat	15 "	
Camel,	100 "	Fox,	15 "	e
Lion,	70 "	Dog.	10 "	
Porpoise,	30 "	Sheep,	10 "	
Horse,	20 "	Rabbit.	7 "	
Bear,	20 ''	Souirrel.	7 "	

Careful observations have shown the following to be about the average growth in twelve years, of several varieties of hard wood, when planted in groves and cultivated:

	Inches diameter.	Feet high.
White Maple.	12	30
Ash, Leaf Maple or Box Elder,	12	20
White Willow,	18	35
Lombardy Poplar,	10	40
Blue and White Ash,	10	25
Black Walnut, and Butternut.	10	20

NUTRITION IN FOOD.

The following is "Boussingault's Scale of Nutritive Equivalents," and shows how many parts of the various articles of food in common use it takes to be equal in nutrition to 100 parts of wheat flour:

100	Rye,	111
107	Rice,	177
119	Buckwheat,	108
130	Maize,	130
56	Horse Beans,	44
57	Peas.	- 67
810	Potatoes,	313
83	Carrots,	777
117.	Turnips,	1335
	107 119 130 56 57 810 83	107 Rice, 119 Buckwheat, 130 Maize, 56 Horse Beans, 57 Peas, 810 Potatoes, 88 Carrots,

WEIGHTS (MISCELLANEOUS).

2		- , -
Bbl. flour weighs	196 280	pounds.
Salt Beef	200	**
Pork	200	**
Fish	200	
Keg Powder equals	25	44
Stone of lead or Iron equals	14	• 6
Pig of " equals	21	1/2 stone.
1 bush, of Oats	32	pounds.
1 "Barley	48 56	"
1 " Corn. Rye, or flax seed	56	4.6
1 " Blue grass	14	• 5
1 " Castor Beans	46	
1 " Hemp seed	44	4.6"
1 " \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	60	46
1 " Timothy seed	45	. 6
1 " Onions	57	**
1 " Apples, or dried peaches.	28	4.6
1 " Salt	50	4.
A sack of wool	- 308	1.4
A pack " " (for a horse)	240	6.

A bale of cotton is 400 pounds, but it is put up in different states varying from 280 to 720 pounds. Sea island cotton is put up in sacks of 300 pounds.

AGES ATTAINED BY BIRDS.

AUDOI			D DI DIND		
Blackbird lives	13	yrs.	Parrot lives	65	yrs.
Blackcap lives	15	6.6	Partridge lives	15	66
Canary lives	24	"	Peacock lives	24	66
Crane lives	27	66	Pelican lives	58	66 1
Crow lives	100	"	Pheasant lives	15	66
Eagle lives	100	44	Pigeon lives	20	66
Fowl (common) li	ives 12	6.6	Raven lives	100	66
Goldfinch lives	15	66	Robin lives	12	66
Goose lives	50	"	Skylark lives	30	66
Heron lives	60	- 66	Sparrow Hawk lives	40	66
Lark lives ·	18	66	Swan lives	100	66
Linnet lives.	23	66	Thrush lives	10	6.6
Nightingale lives	18	66	Wren lives	3	6.6

FRESH WATER.

The component parts, by weight and measure, is—Oxygen 88.9 weight, and 1 by measure; hydrogen 11.1 weight, and 2 by measure. One cubic inch of distilled water at its maximum density, 39.83, the barometer 30 inches, weighs 252.7 grains. A cubic foot weighs 62.5 pounds.

AMOUNT OF OIL IN SEEDS.

Kinds of Seed. Rapeseed Sweet Almond Turnip seed White mustard Bitter Almond Hempseed Linsaed	Per cent	55 47 45 37 37 19	Oats Clover hay Wheat bran Oat-straw Meadow hay Wheat-straw	Per cent	61/2 5 4 4 31/2 3
Hempseed Linseed			Wheat flour		3
Indian corn	- 1		Barley		21/2

THE ENGLISH QUARTER, at which wheat is quoted in the English reports, is 560 pounds, or 14 of the ton gross weight of 2,240 lbs. The English legal bushel is 70 pounds, and consequently 8 of those bushels is a quarter—equal to 91/2 of our statue bushels of 60 pounds.

HOUSEHOLD WEIGHTS AND MEASURES.

1 Teaspoonful equals 1 dram.

I dessertspoonful equal 2 teaspoonfuls, or 2 drams.

1 tablespoonful equals 2 dessertspoonfuls, or 4 teaspoonfuls,

2 tablespoonfuls equal 8 teaspoonfuls, or 1 ounce.

1 common size wineglassful equal 2 ounces, or $\frac{1}{2}$ gill. A tea cup is estimated to hold 4 fluid ounces, or 1 gill.

- 1 pound of wheat is equal to about 1 quart.
- 1 pound and 2 ounces of Indian meal is equal to 1 quart.
- 1 pound of soft butter is equal to about 1 pint.
 1 pound of sugar is equal to about 1 pint.

TOWNSHIP PLAT.

T	TownshipRange							
		~	NO	RTH.	Count	y,	_	
	6	- 5	4	3	2	1	/	
-	7	8	9	10	11	12		
WEST	18	17	16*	15	14	13	EAST	
WI	19	20	21	22	23	24	E	
	30	29	28	27	26	25		
0	- 31	32	33	34	35	36		

SOUTH

*School section.

A township is 6 miles square = 36 sections. A section "1" = 640 acres. , $\frac{14}{16}$ "1 $\frac{1}{16}$ "1 $\frac{1}{16}$ "1 $\frac{1}{16}$ "1 $\frac{1}{16}$ " = 40"

Hence a township contains 23,040 acres. The smallest tract of land sold by the government is a "quarter-quarter section," which contains 40 acres. The sections are numbered from 1 to 36 commencing at the north-east corner.

Any citizen (or foreigner who has declared his intention to become one), who has actually settled upon an unappropriated quarter section (160 acres), and has erected a dwelling-house thereon, acquires the right of "pre-emption," that is, the right to purchase that 160 acre plot at the *minimum price*, though he had not located the tract before his settlement. He is permitted to take up, without payment of any price, except certain fees, 160 acres of \$1.25 land, or 80 acres of \$2.50 land, as a homestead. But the patent or deed will not be issued until he has resided on it for five years. The "patent" or deed is issued by the U. S. Land Commisioner.

THE CENTER OF POPULATION.

The centre of population of the United States is stedily moving westward, at the rate of fifty miles every ten years. The following is the centre point at each census:

miles east of Baltimore. "west of Baltimore. 1790 221800 18 1810 40 north-west of Wasnington. north of Woodstock, Va west by south-west Moorefield, W. Va. 1820 16 1830 66 19 66 1840 16

1840 16 "west of Clarksburg W. Va. 1850 23 "south-east Parkersburg, W. Va. 1860 20 "south of Chillicothe, O.

1870 48 " east by north of Cincinnati. 1880 8 " west by south of Cincinnati.

POWER OF AN ORDINARY MAN.

1 man can raise 10 pounds, 10 feet, in a second, 10 hours a day.

1 man can raise 100 pounds 1 foot.

1 man can draw on a level 640 pounds.

A man can press with hands equal to 110 pounds.

A man's force, drawing horizontally, 110 pounds. A man can lift with both hands 236 pounds.

A man can support on his shoulders 330 pounds.

5 men working 10 hours a day are equal to 1 horse working 8 hours.

3 men carrying 100 pounds each will ascend a hill quicker than 1 horse carrying 300 pounds.

A man's strength is a sater in rasing a weight when his own weight is to that of his load as four is to three.

POWER OF A HORSE.

1 horse can raise 150 pounds 220 feet high in a minute: 8 hours a day.
1 horse-power is reckoned at from 30.000 to 36,000 pounds,

raised 1 foot high per minute.

horse's force drawing horizontally is estimated at

770 pounds. 1 horse can draw on a level 4480 pounds,—2 tons—equal to 7 men.

FORCE REQUISITE TO MOVE A BODY.

A stone along a rough chiseled floor require's $\frac{2}{3}$ of its weight. The same on rollers, 1-32.

A stone along a wooden floor, 3-5 of its weight. The

same on rollers 1-40.

DISTANCE IN FEET GONE BY IN A SECOND.

A man walking, 4; a horse, harnessed, 12; a ship, 14; a steamship, 18; a reindeer on ice, 26; a race horse, 43; a hare, 88; a locomotive engine, 117; a 24 pound cannon ball, 1,300; the moon, 3,300; the earth, 99,733; an eagle, 117; a hawk, 50; a crow, 36.

The electric telegraph, 1.520.640.000, or more than eleven

times around the world.

9

A swift bird would be 3 weeks in flying round the world. Light travels about 192.000 miles in a second.

Light could pass round the earth in the 18th of a second.

SOUND.

Sound	passes	through air along water	in	a	second		1.130 4.900	
66	66	Cast-Iron					11.090	
66	44	Steel					17.000	• •
66	66	Glass					18.000	• 6
66	66	Wood				4636 to	17.000	6.5

Cold air conducts sound better than warm.

MEASURES OF ROCK AND FARTH

		141-7	CONTEO OF HOOK AND EARTH.		
25	cubic	feet c	of sand equal	1 to	on.
18	44	66	Earth	1 '	٠.
17	66	66	Clay	1 '	6
13	6.6	66	Quartz, unbroken in lode	1 .	6
18	6.	- 66	Gravel or earth before digging	alama	27

18 " " Gravel or earth before digging equals 25 cubic feet when dug.

20 cubic feet of quartz, broken (of ordinary fineness from the lode), equals one ton, contract measurement.

RAILWAY SIGNAL CODE.

One whistle signifies "down brakes," Two whistles signify "off brakes," Three whistles signify "back up," Continued whistles signify "danger." Rapid short whistles "a cattle alarm." A sweeping parting of the hands on the level with the eyes, signifies "go ahead." Downward motion of the hands with extended arms, signifies "back." Red flag waved up the track, signifies "danger." Red flag stuck up by the roadside, signifies "danger ahead." Red flag carried on a locomotive, signifies "an engine following." Red flag hoisted at a station, is a signal to "stop." Lanterns art." Lanterns swung at right angles across the track, means "stop." Lanterns swung in a circle, signifies "back the train."

REMARKS ON USING FILES.

A new file should always be used with a light pressure on the work till the needle-like points of the teeth are worn away; after this, a much heavier pressure may be used with much less danger of breaking off the teeth at their base. Many new files are violently diminished half their efficiency by a few careless strokes when first applied to the work.

Do not use a new file on the chilled and gritty skin of castings, or on a weld where borax or any vitreous fluxes have been employed—no file can endure such usage.

Every filer should keep a worn file with which first to attack the rough, gritty or oxy dized surface of iron work, and thereby pave the way for a more efficient work whis sharp files. A piece of gritty or chilled casting that would rapidly destroy the cutting qualities of a new file, would produce scarcely any damaging effect to a worn one.

In filing steel, better results can generally be obtained by using files of a grade not coarser than "2d cut;" finer grades being employed according to the finish and delicacy

of the work under manipulation.

Parties using files should always seek to discover the fitness or adaptibility of cut and form of files especially suited to their work. No one should expect the best results from a file on brass or spelter which was intended for use on iron or steel.

SHRINKAGE OF CASTINGS.

Iron, Small cylinders. "Pipes	=	1-16 in. 1/8 "	per foot.
" Girders, Beams, etc.	=	1/8 "	in 15 Ins.
" Large cylinder the contract	tion	,0	
" of diameter at top	=	1-16 "	per foot.
" Ditto at bottom	=	1/2 "	** **
" in length	= 0.	1/8 "	in 16 Ins.
Brass, thin	=	1/8 "	in 9 "
" thick	=	- 1/8 "	in 10 "
Zine	= ,	5-16 "	in a foot.
Lead	= '	5-16 "	in " "
Copper	=	3-16 "	in " "
Bismuth	=	5-32 "	in " "

SPEED OF SAWS.

To ascertain the proper number of revolutions per minute of any size saw, divide 36.000 by the diameter of the saw in inches, thus -36.000+60=600, the number of revolutions a 60 inch saw should make.

WEIGHT OF GRINDSTONES.—RULE:—Square the diameter (in Inches) multiply by thickness (in Inches); then by the decimal .06363; the product will be the weight of the stone in pounds.

TO ASCERTAIN THE DEGREE OF HEAT OF STEEL.

Steel becomes a very		r). 430°
	Straw color	450
	Full yellow	470
	Brown	490
/	Brown with purple spots	510
	Purple	530
	Blue	550
	Full blue	560
	Dark blue verging on black	600

AVERAGE OF THE LINEAL EXPANSION OF A FEW METALS FROM 32° TO 212°.

	ncreas	ed len-			ised leng at 212°	gth
Zinc sheet			-		part in	812
" cast	- 66	322		Antimony	*	923
Lead	66	351	1	Palladium	**	1000
Tin pure	66	403		Platinum	44	1167
" impure	**	516		Glass	"	1160
Silver	**	• 524		Marble	66	2833
Copper	41	581		Iron soft	44	818
Brass	66	584	1	Iron east	66	900
Gold	66	682		Steel tempere	d. "	806
Bismuth	- 46	719		Steel	"	926

Quantity of water that will flow through a pipe 500 feet long in 24 hours, with a fall of 10 feet.

3/8 1/2	inches	bore	576 1,150	gallons.
5/8	66	46	2,040	46
34	6.6		3,200	44
1	46 0	66	6.624	"
71/4	66	+6	10,000	46

METAL IN THEIR PROBABLE ORDER OF THEIR HARDNESS.

Mercury, Sodium, Potassium, Lead, Zinc, Tin, Antimony, Gold, Silver, Cadmium, Bismuth, Tellurium, Copper, Coper and Zinc, (Brass) Platinum, Copper and Tin, (gumetal) Palladium, Iron, Cobalt, Nickel, Crude Iron, (grey) Steel, (soft) Steel, (hardened) Manganese, Titanium, Crude Iron, (white) Chromium, Rhodium, Iridium, Osminum, Hardest steel varying from white iron to top of list.

The following Table Represents the pressure in pounds on the square inch at a given depth of water.

20	Feet	81/2	Ibs.	70	Feet	301/2	tbs.	120	Feet	521/41	bs.
30	66	1234	4+	80	66	3434	66	130	"	561/2	
40	44	1714	a6 6	90	"	• 39	"	140	"	0004	"
50	66	2134	46	100	66	431/2	*6	150	-4.6	651/4	"
60	4.6	2614	46	110	66	4734	+ 6				

14

SOLDERS.

For lead, one of tin and one and one-half of lead. For tin, one of tin and two of lead.

For pewter, two of tin and one of lead.

For brazing (hardest), three of copper and one of zinc.

For brazing (hard), one of copper and one of zinc. For brazing (soft), one of tin, four of copper, and three of

zinc; or, two of tin and one of antimony.

For silver (hardest), four of fine silver, and one of copper. For silver (hard), three of silver one part brass wire. For silver (softest), two of silver and one of brass wire. For gold (hardest), four of copper seven of silver and

eighty-nine of gold.

For gold (hard), sixty-six of copper and thirty-four of zinc.

For gold (soft), sixty-six of tin and thirty-four of lead. For iron, sixty-six of copper, 33 of zinc and one of antimony.

For copper, fifty-three of copper and forty-seven of tin. For steel, thirteen of copper, five of zinc and eighty-two of silver.

For brass, forty-seven of copper forty-seven of zinc.

FLUXES FOR SOLDERING OR WELDING.

For iron or steel, borax or sal-ammoniac,

For tinned iron, resin or chloride of zinc. For copper and brass, sal-ammoniac or chloride of zinc.

For zinc, chloride of zinc.

For lead, tallow or resin.

For lead and tin pipes, resin and sweet oil.

ACTUAL HORSE-POWER OF ENGINES.

RULE:—Multiply the area of the piston by the pressure per square inch; the product by the speed of the piston per minute, equals the force in pounds; this last divided by 33.000 equals the actual horse-power, including the friction.

SIMPLE RULE TO ASCERTAIN HORSE-POWER OF STEAM ENGINE.—Area of cylinder in inches multiply by pounds of steam in boiler, less 20 per cent off, the remainder by speed of piston in feet per minute; divide the product by 33.000

Thus: engine 20-inch cylinder (area 314 inches), boiler pressure 80 pounds, less 20 per cent off=64 pounds, speed of piston 250 feet per minute.

Then: $314 \times 64 \times 250 \div 33.000 = 152 \text{ H. P.}$

EASY RULE FOR FINDING THE AREA OF A CIRCLE.

A short and easy method of finding the area of a circle, is to multiply the square of the diameter by 7 and divide by 9, and you will have the area (nearly). This rule does

not give it exact; it falls a little short, but is near enough for all ordinary purposes.

To find the circumference when the diameter is given.—Multiply the diameter by 22 and divide by 7, and you will have the circumference (nearly).

EFFECTS OF HEAT.

		Degrees Fahr
Fine-Gold	Melts	2590
" Silver	**	1860
Copper	34	2548
Wrought Iron	66	3980
Cast	6.6	3479
Glass	6.6	2377
Brass	6.	1900
Antimony	66	951
Bismuth.	44	476
Cadmium	44	600
Steel	66	250
Lead	66	600
Tin	66	424
Mercury boils	6.6	600
" volatilizes		806
Platinum	6.	4561
Zinc	6.6	766
Mercury	66	39
Bronze (100 copper 10 tin)	6	1652
Sodium	44	190
Potassium		
Nicke!	66	136
Tellerium	46	3950
Indium	66	850
Indidin		349

BLASTING.

In small blasts 1 pound of powder will loosen about 41/2 tons.

In large blasts 1 pound of powder will loosen about 234 tons.

Inclosing 50 or 60 pounds of powder, in a resisting bag hung or propped up against a gate or barrier, will demolish any ordinary construction.

One man can bore, with a bit 1 inch in diameter, from 50 to 100 inches, per day of 10 hours in granite, or 300 to 400 inches, per day in lime stone,

Two strikers and a holder can bore with a bit 2 inches in diameter 10 feet in a day in rock of medium hardness.

COLORS FOR DRAWING.

MATERIAL.	COLOR.
Brass.	Gamboge.
Brick.	Carmine.
Cast-Iron.	Neutral tint.
Clay.	Burnt umber.
Concrete.	Sepia with dark spots.
Earth.	Burnt umber light.
Copper.	Lake and burnt sienna.
Granite.	Indian Ink light.
Lead,	" Ink & Prussian blue
Steel.	Light blue and lake.
Water.	Cobalt or Verdigris.
Wooda	(Burnt Sienna, deep and light for dark
Woods.	and light wood.
Wrought-Iron.	Prussian blúe, light.

STRENGTH OF ICE.

Ice two inches thick will bear men on foot; four inches, men on horse back; six inches thick will bear cattle and teams with light loads; eight inches thick, teams with heavy loads. Ten inches will sustain a pressure of 1.000 pounds per square foot. The above is on the supposition that the ice is sound, and not "snow-ice."

COMPARATIVE VALUE OF WOOD FOR FUEL.

Taking shell-bark hickory as the highest standard, and calling that 100, other trees will compare with it for burning purposes, as follows: shell-bark hickory, 100; pignut hickory, 95; white oak, 84; white ash, 77; dogwood, 75; scrub oak, 73; white hazel, 72; apple tree, 70; white beach 65; black birch, 65; hard maple, 65; black walnut, 62; yellow oak, 60; white elm, 58; red oak, 56; red cedar, 56; wild cherry, 55; yellow pine, 54; chestnut, 52; yellow poplar, 51; butternut, 43; white birch, 43; white pine, 30.

THE SIZES OF SKATES.

COMPARE WITH SIZES OF SHOES AS FOLLOWS.

Skates, Ins.	7	71/2	8	81/2	9	91/2	10	101/2	11 111/2
Shoes, No.	91/2	11	121/2	1	21/2	4	51/2	71/2	9 101/2

FLY WHEELS.

A fly-wheel should always have high velocity.

The diameter should be from 3 to 4 times that of the stroke of the driving engine.

The weight of the rim should be about 85 to 95 poundsper actual horse-power, the momentum of the wheel being 4½ times that of the piston.

When the engine to which a fly-wheel is to be attached is single-acting, it is customery to make the weight of the wheel 5 times greater than when it is to be attached to a double-acting engine. The weight of a fly-wheel in engines that are subjected to irregular motions, as in a cotton-press, rolling-mill, etc., must be greater than in the others where so sudden a check is not experienced.

PILING.

Piles may be loaded to 1000 pounds per square inch of head, if driven to firm bottom.

In sandy soil, the greatest force of a pile-driver will not drive a pile over 15 feet.

MASONRY.

Concrete or Beton should be thrown, or let fall from a height of at least 10 feet, or well beaten down. The average weight of brick-work in mortar is about 102 pounds per cubic foot.

A FOOT SOLDIER TRAVELS IN ONE MINUTE.

70 yards. Common time. 90 steps equals In quick time, 110 86 66 In double quick time 140 110

He occupies in the ranks a front of 20 inches, and a depth of 13, without a knapsack; the interval between the ranks is 13 inches. Average weight of men, 150 pounds each. Five men can stand in a space of 1 square yard.

Table of Proportions of the Circle and its Equal,

The diameter of any circle × 3.1416=the circumference. The circumference of a circle $\times (\frac{1}{3.1416} = 0.31831) =$ the diameter.

The square of the diameter \times (3:1416=0.7854)=the area. The square of the circumference $\times \left(\frac{0.7854}{3.1416^2} = 0.07958\right) =$

the area. The diameter of a circle \times ($\sqrt{0.7854} = 0.8862$) = side of equal square.

The circumference of a circle \times ($\sqrt{0.07958}$ =0.2821) = side of equal square.

The side of any square \times ($\pi_{2871}=3.545$)=circumference of equal circle.

The side of any square $\times (\frac{1}{0.8862} = 1.1284) = \text{diameter of}$

Square of side $\times (\frac{1}{0.7854} = 1.27324366) = \text{square of diameter}$ of equal circle equal so called round inches.

Round inches \times ($^{97954}_{444} = 0.0546$) = square feet. Square of diameter of equal circle \times 0.7854 = square side.

MENSURATION OF SURFACES.

Area of any parallelogram = base \times perpendicular height.

Area of any triangle = base $\times 1/2$ perpendicular height. Area of section of circle = are $\times 1/2$ radius.

Area of segment of circle=area of sector of equal radius, less area of triangle.

Area of parabola = base $\times \frac{2}{3}$ height.

Area of ellipse=longest diameter \times shortest diameter \times .7854.

Area of any regular polygon=sum of its sides× perpendicular from its centre to one of its sides, divided by 2.

Surface of cylinder = area of both ends + height \times circumference.

Surface of segment = height of segment \times whole circumference of sphere of which it is a part.

Cubic contents of a cylinder=area of one end × length.

MENSURATION OF SOLIDS.

Cylinder = area of one end \times length,

Sphere = cube of diameter \times .5236.

Segment of sphere = square root of the height added to three times the square of radius of base \times by height and by .5236.

Cone of pyramid = area of base $\times 1/3$ perpendicular height.

Frustrum of a cone=product of diameter of both ends+sum of their squares, \times perpendicular height \times .2618.

Frustrum of a pyramid=sum of the areas of the two ends + square root of their product, \times by 1/3 of the perpendicular height.

Solidity of a wedge = area of base $\times \frac{1}{2}$ perpendicular height.

Frustrum of a wedge=1/2 perpendicular height \times sum of the areas of the two ends.

Solidity of a ring=thickness + inner diameter,× square of thickness, \times 2.4674.

TO FIND THE DIAMETER AND THE BREAKING STRAIN OF A BOLT.

Multiply the area of $1 \ \Box$ inch by 20, of $2 \ \Box$ inch by 19, of $3 \ \Box$ inch by 18, of $4 \ \Box$ inch by 17, of $5 \ \Box$ inch by 16, of $6 \ \Box$ inch by 15, etc., for Upset Bolts; but with 12.6 for $1 \ \Box$ inch, 12.54 for $2 \ \Box$ inch, 12.50 for $3 \ \Box$ inch, 12.31 for $4 \ \Box$ inch, 11.90 for $5 \ \Box$ inch, and 11.34 for $6 \ \Box$ inch, for common, not Upset Bolts. The result will be the net breaking weight, which is to be divided by the required factor of safety.

EXAMPLE:—What weight can a 2 inch bolt carry before breaking with a factor of 3?

Area of 2=3.1416 $\times \frac{19}{3}$ = 19.9 tons if upset, or $\frac{3.1416}{3}$ ×

12.54 = 13.13 if not upset.

What size of Bolt is required to carry 19.9 tons?

 $19.9 \times \frac{1}{19} = 3.142 = 2$ inch round bolt upset. $19.9 \times \frac{1}{12} = 4.76 = 2.45$ inch round, not upset.

RULES FOR WEIGHTS OF CASTINGS.

		Cast-Iron,	
Multiply the weight of the pattern by	13 "	Brass,	and the product
of the nettown by	19 "	Lead,	is the weight of
of the pattern by	12.2"	Tin,	the casting.
	11.4"	Zinc,	

SHRINKAGE IN CASTINGS.

	Cast-Iron,	3-16	of an inch lon-
PATTERN MAKERS RULE.		1/8 }	ger per lineal
RULE.	Tin,		foot.
	Zinc.	3-16	

REDUCTION FOR ROUND CORES AND CORE PRINTS.

RULE:—Multiply the square of the diameter by the length of the core in inches, and the product by 0.017 is the weight of the Pine Core to be deducted from the weight of the pattern.

SHIPPING ADMEASUREMENT.

REGISTER TON.—For Register tonnage or for measurement of the entire internal capacity of a vessel: 100 cubic feet = 1 Registered Ton.

This number is arbitrarily assumed to facilitate com-

putation.

Shipping Ton for the Measurement of Cargo:

HOW WINES AND LIQUORS ARE PUT UP AND THE NUMBER OF GALLONS THEY CONTAIN.

Dutt of Sherry	100	gamons
Pipe of Port	115	"
Pipe of Teneriffe	100	6
Butt of Malaga	105	44
Puncheon of Scotch Whiskey	110 to 130	-44
" Brandy	110 to 120	66
" Rum	100 to 110	66

Hogshead of Brandy Pipe of Madelra Hogshead of Claret

55 to 60 gallons. 92 46

A hogshead is one-half, a quarter cask is one-fourth, an octave is one-eighth of a pipe, butt, or puncheon.

Proportion of Alcohol in 100 parts of the following Liquors, (Brande).

		(-
Small Beer	1.08	Bordeaux	15.1
Cider	9.8	Shiraz	15.5
Porter	5.3	Malmsey	16.4
Brown Stout	6.8	Sherry	17.2
Ale	10.	" old	23.9
Perry	7.3	Alba Flora	17.3
Rhenish	7.6	Constantia, red	18.9
Moselle	8.7	Port	23.
Johannisberger	8.71	Colares	19.7
Elder Wine	8.8	Lisbon	18.9
Claret	8.9	Malaga	17.2
Tokay	9.4	Cape Muscat	18.3
Rudesheimer	10.7	Tenneriffe	19.8
Marcobrunner	11.6	Lachryma	19.7
Gooseberry Wine	11.8	Currant Wine	20.6
Frontignac	12.9	Maderia	22.3
Hockheimer	12,1	" Sercial	27.4
Vin de Grave	12.8	Marsala	25.1
Champagne	12.7	Raisin Wine	25.2
" Burgundy	14.6	Cape Madeira	29.5
Hermitage, red	12.3	Gin	51.6
" white	17.4	Brandy	53.4
Amontillado	12.6	Rum	53.7
Barsac	13.9	Irish Whiskey	53.9
Santerne	14.2	Scotch "	54.4
White Port	15.		

COMMON NAMES OF CHEMICAL SUBSTANCES.

COMMON NAMES.

Aqua Fortis

Aqua Regia Blue Vitriol Cream of Tartar Calomel Chalk Caustic Potassa Chloroform Common Salt Copperas, or Green Vitriol Corrosive Sublimate Diamond

CHEMICAL NAMES.

Nitric Acid. Nitro-Muriatic Acid. Sulphate of Copper. Bitartrate of Potassium. Chloride of Mercury. Carbonate Calcium Hydrate Potassium. Chloride of Gormyle. " of Sodium.

Sulphate of Iron. Bi-Chloride of Mercury.

Pure Carbon.

COMMON NAMES, Dry Alum

Epsom Salts Ettnops Mineral Fire Damp Galena Glauber's Salt Glucose **Goulard Waters** Iron Pyrites Jewelers Putty Kings Yellow Laughing Gas

Lime Lunar Caustic Mosaic Gold Muriate of Lime Nitre or Saltpetre Oil of Vitriol Potash Realgar Red Lead. Rust of Iron Sal-Ammoniac

Salt of Tartar

Slacked Lime

Soda Spirits of Hartshorn Spirits of Salt Stucco or Plaster of Paris Sugar of Lead

Verdigris Vermilion Vinegar Volatile Alkali Water

White Precipitate White Vitriol

CHEMICAL NAMES.

Sulphate Aluminum and Potassium.

Sulphate of Magnesia. Black Sulphide of Mercury. Light Carbureted Hydrogen. Sulphide of Lead. Sulphate of Sodium.

Grape Sugar. Basic Acetate of Lead. Bi-Sulphide Iron. Oxide of Tin.

Sulphide of Arsenic. Protoxide of Nitrogen. Oxide of Calcium. Nitrate of Silver. Bi-Sulphide of Tin. Chloride of Calcium. Nitrate of Potash. Sulphuric Acid. Oxide of Potassium.

Sulphide of Arsenic. Oxide of Lead. Oxide of Iron. Muriate of Ammonia. Carbonate of Potassa. Hydrate Calcium. Oxide of Sodium.

Ammonia. Hydro-Chloric or Mur'ic Acid.

Sulphate of Lime. Acetate of Lead. Acetate of Copper. Sulphide of Mercury. Acetic Acid. (Diluted). Ammonia.

Oxide of Hydrogen. Ammoniated Mercury. Sulphate of Zinc.

WATER AT DIFFERENT TEMPERATURES.

There are four notable temperatures for pure water,

- 1. Freezing point at sea level, 32° F. weight per cubic foot 62,418 pounds; per cubic inch, .03612 pounds.
- 2. Point of maximum density, 39. 1° F. weight per cubic foot 62.425 pounds; per cubic inch, .036125 pounds.
- 3. British standard for specific gravity 62° F. weight per cubic foot 62,355 pounds; per cubic inch .03608 pounds.

4. Boiling point at sea level, 212° F, weight per cubic foot 59.760 pounds; per cubic inch .03458 pounds.

Sea water, (average), has a specific gravity of 1.028, boils at 213.2° F., and weighs 64 pounds, per cubic foot at 62° F.

A British Thermal Unit (or heat unit), is that quantity of heat which will raise one pound of water at or about the freezing point, 1° Fahrenheit. A French "Caloric" is the heat required to raise one kilogramme of water 1° Centigrade, and is equal to 3.96832 British thermal units.

HERSCHEL'S TABLE FOR FORETELLING THE WEATHER.

This table and the accompanying remarks, originally formed by Dr. Herschel, and approved with some alterations, by the experienced Dr. Adam Clarke, are the result of many years' close observation, the whole being on a due consideration of the sun and moon in their several positions respecting the earth. They show what kind of weather will most probably follow the entrance of the moon into any of its quarters; so probably, indeed, that it has been seldom found to fail. If the new moon, first quarter, full moon or last quarter happens—

BETWEEN	IN SUMMER.
12 and 2, morning,	Fair
2 and 4 "	Cold, with frequent showers.
4 and 6 "	Rain.
6 and 8 "	Wind and rain.
8 and 10 ''	Changeable.
10 and 12 "	Frequent showers.
12 and 2, afternoon,	Very rainy.
2 and 4 "	Changeable.
4 and 6 "	Fair.
6 and 8 "	(Fair if wind N. W.: rainy
8 and 10 "	if winds S. or S. W.
10 and midnight,	Fair.
BETWEEN	IN WINTER.
12 and 2, morning,	Hard frost, unless wind be S. or W.
2 and 4 "	Snow and stormy.
4 and 6 '	Rain
6 and 8 "	Stormy.
8 and 10 "	Cold rain if wind be W.; snow if E.
10 and 12 "	Cold and high wind.
12 and 2, afternoon.	Snow or rain.
2 and 4' "	Fair and mild.
4 and 6 "	Fair.
6 and 8 "	Fair and frosty if wind N. or N. E.
8 and 10 _"	rain or snow if S. or S. W.
10 and midnight,	Fair and frosty.

OBSERVATIONS .- 1. The nearer the time of the moon's change, first quarter, full or last quarter is to midnight, the fairer will the weather be during the seven days following. 2. The space for this calculation occupies from 10 at night till 2 next morning.

3. The nearer to midday, or noon, the phases of the

moon happen, the more foul or wet weather may be expected during the next seven days.

4. The space of this calculation occupies from 10 o'clock

in the morning to 2 in the afternoon.

ALPHABETS OF DIFFERENT LANGUAGES.

The English alphabet contains 26 letters; the French, 25; Hebrew, Chaldee, and Syriac, 22; Greek, 24; Latin. 25; Spanish, 27; Italian, 20; Arabic, 28; Persian, 31; Turkish, 33; Georgian. 36; Coptic, 32; Muscovite, 43; Sclavonic. 27; Dutch, 26; Ethiopic, 222; Tartarian, 222; Bengal India, 21; Brachman, 19; Sanscrit, 28.

FACTS IN LAW.

Ignorance of the law excuses no one.

It is a fraud to conceal a fraud.

The law compels no one to do impossibilities.

An agreement without consideration is void. Signatures made with a lead pencil are good in law.

A receipt for money paid is not legally conclusive. The acts of one partner bind all the others.

Contracts made on Sunday cannot be enforced.

A contract made with a lunatic is void.

Contracts for advertisements in Sunday newspapers are invalid.

Principals are responsible for the acts of their agents.

Agents are responsible to their principals for errors.

Each individual in a partnership is responsible for the whole amount of the debts of the firm.

Notes bear interest only when so stated.

It is not legally necessary to say on a note "for value received."

Part payment of a debt which has passed the time of

statutory limitation revives the whole debt.

An oral agreement must be proved by evidence. A written agreement proves itself. The law prefers written to oral evidence because of its precision.

RELATING TONOTES.

Demand Notes are payable on presentation without grace, and bear legal interest, after a demand has been made, if not so written. An endorser on a demand note is holden for a limited time. variable in different States.

A Negotiable Note must be made payable either to bearer, or be properly endorsed by the person to whose

order it is made. If the endorser wishes to avoid responsibility, he can endorse "without recourse."

^{*}A Joint Note is one signed by two or more persons, who each become liable for the whole amount.

Three Days Grace are allowed on all time notes, after the time for payment expires; if not then paid, the endorser, if any, should be legally notified, to be holden.

Notes Falling Due Sunday, or on a legal holiday, must be paid the day previous.

Notes Dated Sunday are void.

Altering a Note in any manner by the holder, makes it void.

Notes Given by Minors or Lunatics are void.

The Maker of a Note that is lost or stolen is not released from payment if the amount and consideration can be proven.

Notes Obtained by Fraud, or given by an intoxicated person, cannot be collected

An Endorser has a right of action against all whose names were previously on a note endorsed by him.

Deposits of Money in a Bank placed to the credit of depositors, are always subject to their check for full amount due.

If The Letter Containing a Protest of non-payment be put into the post-office, any miscarriage does not affect the party giving notice.

READY RECKONING AND DISCOUNTS.

TO FIND NET COST OF A SINGLE ARTICLE AT VARIOUS DISCOUNTS.

15 20	per "cent.	off,	multiply divide	price	per	dozen	by	.07 1-12 .15
20	and 5	66	multiply	66	66	66	6.	.061/3
20	" 10	66	44	6.6	6.6	4.6	66	.06
	per cent.	4.6	6.	66	66	66	66	.061/4
331	/2 "	6.6	64	4.6	66	44	66	1-18
331,	66	6.6	44	66"	66	6.6	66	.05 5-12
40	"	66	44.		66	66	66	.05

4 0 4 0	and 5 per		ıt. off, mu	ltir 	oly by .43/4
45	per cent.	off.	multiply	by	.04 7-12
50	44	66	"		.04 1-6
60	66	4.4	44		.031/3

TABLE FOR MARKING EACH ARTICLE AT A GIVEN PER CENT. ADVANCE, WHEN BOUGHT BY THE DOZEN.

To gain		r cent.,	remove po					
- /	25	••	arre	r moving	g point,	aaa	1-24	
66	26	66	**		**	66	1-20	
66	28	1 66	44	66	66	66	1-15	
6.6	30	6.6	66	44	66	66	1-12	
46	32	. 66	- 66	44	61	4.6	1-10	
66	331/3	4.6	- 66	66	4.6	66	1-9	
+ 6.6	35	60	4.6	66	66	- 66	1/8	
6.6	40	66	. 46	46	66	66	1-6	
- 441	44	66	66	66	- 16	4 4	1-5	
4.6	50	44	66	66	44	6.6	1/4	
44	60	44	66	46	44	4.6	1/9	
66	80	46 .	44	1 66	66	66	1/2	

EXAMPLE 1.—If goods cost \$20.00 per dozen, what is the price each, at 20 per cent, profit?

\$2.00 Answer.

EXAMPLE 2.-At 35 per cent. 8)2.00

.25

\$2.25 Answer.

TO FIND OUT THE DIFFERENCE BETWEEN PER-CENTAGE ON AND DISCOUNT OFF A PRICE.

60 per cent. on a price, i. e. \$1.00, is \$1.60. This is 371/2 per cent. from a price, \$1.60=\$1.00.

50 per cent. on a price, i. e. \$1.00, is \$1.50. This is 331/3 per cent. or $\frac{1}{3}$ from a price, \$1.50=\$1.00.

40 per cent. on a price, i. e. \$1.00, is \$1.40. 281/2 per cent. from a Price, \$1.40=\$1.01. This is about

33 per cent. on a price, i. e. \$1.00, is \$1.331/3. This is 25 per cent. from a price, \$1.331/3=\$1.00.

25 per cent. on a price, i. e. \$1.00 is \$1.25 This is 20 per

cent. or 1-5 from a price, \$1.25=\$1.00. 20 per cent. on a price, i. e. \$1.00, is \$1.20. This is 162/3 per cent. or 1-6 from a price, \$1.29=\$1.00. 162/3 per cent.on a price, i. e. \$1.00 is \$1.162/3. This is about

12½ per cent. or ¼ from a price, \$1.1623=\$1.02. 12½ per cent. on a price i e. \$1.00, is \$1.12½.

about 1034 per cent. from a price, \$1.121/2=\$1.01. 10 per cent on a price, i. e. \$1.00, is \$1.10. This 91/8 per cent. from a price, \$1.10=\$1.00. This is about

To Find out the Price for Single Pieces when Gross Price is Known (this is very convenient in buying or selling articles by the piece when list price is by the gross).

Multiply gross price by 7, and point off 3 figures from the right; those remaining are cents if gross price is dollars

and will give the price very near, i. e. \$10.00 \times 7=7.000 or nearly 7¢ each, or 84¢ per dozen=\$10.08 per gross.

To Make a List Price from which a Percentage can be Taken and Find Net Cost or Leave a Profit.

For cost 60 per cent. off, multiply by 10 and divide by 4.

EXAMPLE. $-\$1.00\times10=\$10.00\div4=\$2.50$; this less 60 per cent. i. e. \$1.50=\$1.00.

For profit 60 per cent, off add the profit you intend to make and proceed as above.

For 50 per cent, profit on:

EXAMPLE. $-\$1.00+50=\$1.50\times10=15.00\div4=\3.75 ; less 60 per cent., i. e. \$2.25=\$1.50.

If you want to make cost price 60 per cent. and wish to sell at 40 per cent, for retail for 50 per cent, profit on or 331/3 per cent. off of sales:

EXAMPLE. -\$2.50 list less 40 per cent. -\$2.50 - \$1.00 = \$1.50the amount of sale.

If you wish to sell at wholesale at 50 per cent, and for 25 per cent, profit on or 20 per cent, off:

Example.—\$2.50 list less 50 per cent.=\$1.25, amount of sale.

For cost	50	per cent.	off,	multiply	by	10,	divide	by 5
66	40	- 44	66	66		10	66 .	6
66	30	66	6.6	66		10	66	7
66	25	66	66	44		10	66	71/9
44	20	44	66	"		10	- "	8

The Following Suggestions are Given for Readily Obtaining the Cost of Goods Sold at a Discount From List Prices.

To deduct 21/2 per cent., subtract 1-40 from amount.

To deduct 5 per cent., subtract 1-20 from amount.

To deduct 5 and $2\frac{1}{2}$ per cent., subtract 1-20 from the amount; then 1-40 from remainder.

To deduct 71/2 per cent., subtract 11/2 times 5 per cent.

To deduct 10 per cent., subtract 1-10 from amount. To deduct 10 and 5 per cent., subtract 1-10 from amount; then 1-20 from remainder.

To deduct 121/2 per cent., subtract 1/2 from the amount.

To deduct 15 per cent., subtract 1½ times 10 per cent.
To deduct 15 and 5 per cent., subtract 1½ times 10 per cent. from amount, and 1-20 from remainder. To deduct 20 per cent., subtract 1-5 from the amount.

To deduct 20 and 5 per cent., subtract 1-5 from the amount; then 1-20 from remainder.

To deduct 25 per cent., subtract 14 from amount.

To deduct 25 and 5 per cent., subtract 1/4 from the amount; then 1-20 from remainder.

To deduct 331/3 per cent., subtract 1/3 from amount.

To deduct 35 per cent., add 30 per cent. to 1/2 the amount.

To deduct 40 per cent., subtract 14 from the amount; then subtract 1-5 from remainder.

To deduct 40 and 5 per cent., subtract 14; then subtract 1-5 from remainder; then 1-20. Or, subtract 4-10, and 1-20 from remainder.

To deduct 45 per cent., divide by 2 and add 10 per cent.

To deduct 45 and 5 per cent., divide by 2, add 1-10 and subtract 1-20.

Cost of Articles by the Piece, from I to I Dozen.

Price			,	C	ost 1	er ()uan	tity			
Dozen.	11	10	9	8	7	6	5	4	3	2	- 1
\$1.00	1\$.92	\$.83	\$.75	\$.67		\$.50					\$.081/3
1.25	1.15			.83	.73	.63	.52	.42	.31	.21	.101/2
1.50				1.00	.88	.75	.63	.50	.38	.25	.121/2
1.75	1.60						.73	.56	.44	.29	.145/8
2.00	1.83	1.67	1.50	1.33	1.17	1.00	.83	.67	.50	.33	.162/3
2.25				1.50			.94	.75	56	.38	.183/4
2.50	2.29	2:08	1.88	1.67	1.46	1.25	1.04	.83	.63	.42	.211/8
2.75	2.52	2.29	2.06	1.83	1.60	1.38	1.15	.92	.69	.46	.23
3.00	2.75	2.50	2.25	2.00	1.75	1,50	1.25	1.00	.75	.50	.25
3.50	3.21	2.92	2.63	2.33	2.04	1.75	1.46	1.17	.88	.58	.291/4
3.75	3.44	3.13	2.81	2.50	2.19	1.88	1.56	1.25	.94	.63	.311/4
4.00	3.67	3.33	3.00	2.67	2.33	2.00	1.67	1.33	1.00	.67	.331/3
4.25	3.89	3.54	3.19	2.83	2.48	2.13	1.77	1.42	1.06	.71	.351/2
4.50	4.13	3.75	3.38	3.00	2.63	2.25	1.88	1.50	1.13	.75	.371/2
4.75	4.23	3.96	3.56	3.17	2.77	2.34	1.98	1.58	1.19	.79	.395/8
5.00	4:58	4.17	3.75	3.33	2.92	2.50	2.08	1.67	1.25	.83	.412/3
5.25	4.81	4.38	3.94	3.50	3.06	2.63	2.19	1.75	1.31	.88	.4334
5.50	5.04	4.58	4.13	3.67	3.21	2.75	2.29	1.83	1.38	.92	.46
5.75	5.27	4.79	4.31	3.83	3.35	2.87	2.40	1.92	1.44	.96	.48
6.00	5.50	5.00	4.50	4.00	3.50	3.00	2.50	2.00	1.50	1.00	.50
6.25	5.73	5.21	4.69	4.17	3.65	3.13	2.60	2.08	1.56	1.94	
6.50						3.25					
6.75	6.19	5.63	5.06	4.50	3.94	3.38	2.81	2:25	1.69	1.13	.5614
7.00	6.42	5.83	5.25	4.67	4.08	3.50	2.92	2.33	1.75	1.17	.581/3
7.25				4.93	4.23	3.63	3.02	2.42	1.81	1.21	.601/2
7.50	6.88	6 25	5.63	5.00	4.38	3.75	3.13	2.50	1.88	1.25	
7.75	7 11	6.46	5.81	5.17	4.59	3.88	3.23	2.58	1.94	1.29	.645/8
8.00	7.33	6 67	30.3	5 22	1 65	1 00	3 23	2 67	2 00	1 33	.662/3

HOW TO MARK GOODS.

Suppose an article is bought by the dozen, and the merchant wants to make 20 per cent. All he has to do is remove the decimal point one place to the left. Suppose brooms are \$2.50 a dozen; then 25 cents each is the cost with 20 per cent. added. To make 25 per cent. remove the point one place to the left and add 1-24.

To	make	30	per	cent.	add	1-12	itself.
46	+6	331/ ₃ 35	46	46	66	1-9 1/8	66
46	4.6	40	66	44	4.6	1-6	44
1.	4.6	44	6.6	6.6	46	1-5	••
44	4.4	50	66	6.6	46	1/4	**
4.6	44	60	66	4.6	- 46	1/2	
4.6	66	80	4.6	4.6	66	1/2	46

Always remove the decimal point one place to the left before making the additions and the sum will be the selling price of the single article,

In calculating the per cent, on a single article if you wish to make

10 per cent. divide by 10, multiply by 11 66 20 10 12 46 "multiply "10 divide "divide "10 multiply " 258 66 30 331/3** " add 1/3 of itself.
" divide by 3 multiply by 66 add 1/2 of itself. 50

ANTIDOTE FOR POISONS.

In cases where the other articles to be used as antidotes are not in the house, give two tablespoonfuls made mustard in a pint of warm water. Also give large draughts of warm milk or water mixed with oil, butter, or lard. If possible, give as follows:

Poisons.

Antidotes.

BED-BUG POISON,
BLUE VITRIOL,
CORROSIVE SUBLIMATE,
LEAD WATER,
SALTPETRE.
SUGAR OF LEAD,
SULPHATE OF ZINC.
RED PRECIPITATE.
VERMILION,
BISMUTH,
VERDIGRIS,

Give Milk or White of Eggs, in large quantities.

Poisons.

Antidote.

Fowler's Solution, White Precipitate, Arsenic, Give prompt Emetic of Mustard and Salt, tablespoonful of each; follow with Sweet Oil, Butter, or Milk.

ANTIMONIAL WINE, TARTAR EMETIC, Drink warm water to encourage vomiting. If vomiting does not stop, give a grain of Opjum in water.

OIL VITRIOL, AQUA FORTIS, BI-CARBONATE POTASS, MURIATIC ACID, OXALIC ACID,

Magnesia or Soap, dissolved in water, every two minutés.

CAUSTIC SODA, CAUSTIC POTASH, VOLATILE ALKALI, Drink freely of water with Vinegar or Lemon Juice in it.

CARBOLIC ACID, IODINE, IODIDE OF POTASS,

Give Flour and Water or Glutinous drinks.

Pour cold water over the head

CHLORAL HYDRATE, CHLOROFORM,

and face, with artificial respiration, Galvanic Battery.

Prompt Emetics; Soap or Mucil-

CARBONATE OF SODA, COPPERAS, COBALT,

Strong Coffee followed by Ground Mustard or Grease in warm water to produce vomiting. Ke ep in motion.

aginous drinks.

NITRATE OF SILVER, STRYCHNINE, TINCT. NUX VOMICA, \Give common Salt in water.

Emetic of Mustard or Sulphate of Zinc, aided by warm water.

PHOSPHORUS,

LAUDANUM, MORPHINE,

OPIUM.

Magnesia with water and copious draughts mucilaginous drinks.

In all cases of poisoning, the first step is to evacuate the stomach. This should be effected by an emetic which is quickly obtained. Mustard or salt (tablesponful) mixed in a tumblerful of water, or ½ teaspoonful powdered Ipecac every 10 to 15 minutes. When vomiting has already taken place, copious draughts of warm water should be given to keep up the effect till the poisonous substance has been thoroughly evacuated. If vomiting can not be produced the stomach-pump must be used.

TABLE OF UNITED STATES AND FOREIGN MONEY.

TABLE OF UNITED ST	A LES AND FUNEIGN	IVIC	NET.
Argentine Republic.	Peso.	G	\$.965
Austria.	Florin.	Ğ	.336
Belgium	Franc.	G	.193
Bolivia.	Boliviano.	S	.68
Brazil.	Milreis.	G	.546
British Possessions, N. A.	Dollar.		1.00
Chili.	Peso.		.912
Cuba.	Peso.	G	.926
Denmark.	Crown.	Ĝ	.268
Ecudor.	Sucre.	Ğ	.68
Egypt.	Pound (100 piastres).	G	4.943
France.	Franc.	Ğ	.193
German Empire.	Mark.	Ğ	.238
Great Britain.	Pound sterling.	G	4.8665
Greece.	Drachma.	Ğ	.193
Guatemala.	Peso.	S	.68
Hayti.	Gourde.	Š	.965
Honduras.	Peso.	S	.68
India.	Rupee.	GGGGGGGGMMG	.323
Italy.	Lira.	Ğ	.193
		G	.997
Japan.	Yen. {	S	.734
Liberia.	Dollar.		1.00
Mexico.	Dollar.	G	.739
Netherlands.	Florin.		.402
Nicaragua.	Peso.	Ĭš	.68
Norway.	Crown.	Ğ	.268
Peru.	Sol.	G S G S	.68
Portugal.	Milreis.	Ğ	1.08
Russia.	Rouble.	G	.544
Spain.	Peseta.	Ğ	.193
-Sweden.	Crown.	Ğ	.268
Switzerland.	Franc.	Ğ	.193
Tripoli	Mahbub.	-	.614
Turkey	Piastre.	G	
United States Colombia.	Peso.	G	
Venezuela.	Bolivar.	Ğ	.136
, carcada and	12702210021		

UNITED STATES.

10 mills (m)	make		1	cent	¢. d.
10 cents 10 dimes	"		1	dollar	\$.
10 dollars	6	-	1	eagle	E_{\bullet}

FRANCE.

U. S.	Value.	\$.	¢.	m.
			-	11 8

10 Centimes equal	1 Decime.	.01.8
10 Decime	1 Franc.	.18.7
20 Franc "	1 Napoleon (or Louis).	3.72.0
40 "	1 Double Napoleon and (Louis).	7.44.0
5 " niece "		.93.0

GREAT BRITAIN AND IRELAND.

GREAT BRITAIN AND IRELAND.	
. U. S. Value, \$	¢. m,
4 Farthings equal 1 Penny	, ,
12 Pence " 1 Shilling.	.22,2
20 Shillings " 1 Pound Sterling.	4.44,4
2 " " 1 Florin.	.44,4
10 Florins " 1 pound.	4.44,4
1 Crown " 5 Shillings.	1.08,0
1 Sovereign " 20 "	4.86,
1 Guinea " 21 "	5.07,5
a = 1 = = -	
SPAIN.	
34 Maravedis equal 1 Real.	.11,0
8 Reals " 1 Dollar or Plate.	.88,0
275 Maravedis " 1 Ducat of Exchange.	2.21,0
4 Dollars of Plate " 1 Pistole of "	3.88,4
•	
AMSTERDAM.	
16 Pfennings equal 1 Stiver.	.02,0
20 Stivers " 1 Florinour Guilder.	
12 Grotes, or Pence Flemish, or § 1 Shilling.	•
6 Stivers. Flemish.	.12,0
20 Shillings, or " (1 Downd	2.40.0
6 Florins,	2.40,0
2½ Florins, or " {1 Rix Dollar.	.96,0
50 Stivers,	.50,0
W . W D W D G	
HAMBURG.	
12 Pfennings equal 1 Schilling or Sol.	
16 Schillings " 1 Mark.	.28,5
3 Marks " 1 Rix Dollar.	.85,5
Control of the contro	
PRUSSIA.	
12 Pfennings equal 1 Silver Groschen.	.02,3
30 Groschen " 1 Dollar.	.69.0
DENMARK.	
12 Pfennings equal 1 Skilling.	,
16 Skillings 1 Mark	.08.7
6 Marks Danish " 1 Rix dollar	.52.5
RUSSIA.	
10 Kopecks equal 1 Grieve	.07,5
10 Grieves " 1 Ruble	.75,0
1 10000	,0
A USTRIA.	
4 Pfenning equal 1 Kreutzer	
60 Kreutzers ". 1 Florin	.48,5
11/2 Florins " 1 Rix dollar	.72.7
1 ma dollar	. 14, 1

PORTUGAL.

	t to at a t	A 21 A2 .	
1000 Rees 400 Rees 480 Rees "	1 Cru	U. S. Value. dree. usado of Exchange. w Crusado,	\$. ¢. m. 1.24,0 .49,6 .59,5
	ROM	E.	
2 Mezzi Quattrini 5 Quattrini 10 Baiocchi 10 Paoli	equal "	1 Quattrino. 1 Baioccho. 1 Paolo. 1 Scudo.	.01,0 .10,0 1.00,6
B E N G	AL and	CALCUTTA.	
12 Pice 16 Anna	equal	1 Anna. 1 Rupee.	$.03.3 \\ .50,0$
	GREE	CE.	
100 Lepta	equal	1 Drachma.	.16,6
	TURK	EY.	
3 Aspers 40 Paras	equal	1 Para. 1 Piastre.	.01,0 $.40,0$

PORTRAITS ON AMERICAN CURRENCY.

\$1, Washington; \$2, Jefferson; \$5, Jackson; \$10, Webster, \$20. Hamilton; \$50, Franklin; \$100, Lincoln; \$500, General Mansfield; \$1000, De Witt Clinton; \$5000, Madison; \$10-000, Jackson. On silver certificates—\$1, Martha Washington; \$2, Gen. Hancock; \$10, Robert Morris, Thos. A. Hen; dricks; \$20, Commodore Decatur; \$50, Edward Everett. \$100, James Monroe; \$500, Charles Sumner, and \$1000, W. L. Marcy. On gold notes—\$20, Garfield; \$50, Silas Wright; \$100, Thomas H. Benton; \$500, A. Lincoln; \$1000, Alexander Hamilton; \$5000, James Madison; \$10,000, Andrew Jackson.

HOW BIRDS AND ANIMALS ARE GROUPED.

A table showing in a concise manner how various birds and animals are classed:—A covy of Partridges. A wide of Pheasants. A wisp of Snipe. A bevy of Quall. A flight of Doves or Swallows. A muster of Peacocks. A siege of Herons. A building of Rooks. A brood of Grouse. A plump of Wild Fowl. A stand of Plovers. A watch of Nightingales. A flock of Geese. A cast of Hawks. A trip of Dottrell. A swarm of Bees. A school of Whales. A shoal of Herrings. A herd of Swine. A skulk of Foxes. A pack of Wolves. A drove of Oxen. A sounder of Hogs. A troop of Monkeys. A pride of Lions. A sleuth of Bears.

Interest on \$1 from 2% to 9% to thousandths of a cent, for any number of days. or months, and for 1 year.

- TT:	1 0 1	1 0 7	1 42				0 /	0.4
Time.	2%	3%	1 4%.	5%	6%	7%	8%	9%
1 da.	.00005	.00008	,00011	.00014	.00017	.00019	.00022	.00025
- 2 3	.00011	.00017	.00022	.00028	.00033	.00039	.00044	.0005
3	1.00016	.00025	.00033	.00042	.0005	.00058	.00067	.00075
5	.00022	.00034	.00044	.00056	.00067	.00078	.00089	.001
5	,00028	.00042	.00056	.00069	.00083	.00097	.00111	.00125
6	.00033	.0005	.00067	.00083	.001 .00117	.00117	.00133	.0015
7 8	.00039	.00058	.00078	. 00097	.00117	.00136	.00156	.00175
8		.00066	.00089	.00111	.00133	.00156	.00178	
9	.0005	.00075	.001	.00125	.0015	.00175		.00225
10	.00056	.00083	.00111	.00139	.00167	.00194	.00222	.0025
11					.00183	.00214	-00244	,00275
12	.00067	.001	.00133	.00167	.002	.00233	.00267	.003
13	,00072	.60108	.00144	.00181	00217 00233	.00253	0.00289	.00325
14	.00078	.00116	.00156	.00194	.00233	.00272	.00311	.0035
15	.00084	.00125	.00167	.00208	.0025	00292	.00333	.00375
16	.00089	.00133	.00178	.00222	.00267	.00311	.00356	.004
17	.00095	.00141	.00189	.00236	. 00283	.00331	1.00378	.00425
18	.001	.0015	.002	.0025	. 003	.0035	.004	.0045
19	.00106	.00158	.00211	.00264	.00317	.00369	.00422	.00475
20	.00111	.00166	.00222	.00278	.00333 .0035	.00389	.00444	.005
21	.00117	0.00175	.00233	.00292	.0035	.00408	.00467	.00525
22	.00122	.00183	.00244	.00306	.00367	.00428	.00489	.0055
23	.00128	.00191	0.00256	.00319	.00383 .004	.00447	.00511	.00575
24	.00134	.002	.00267	.00333	.004	.00467	.00533	.006
25	.00139	.00208	.00278	.00347	.00417	.00486	.00556	.00625
26		.00216	.00289	.00361	.00423	.00506	.00578	.0065
27	.0015	.00225		.00375	.0045	.00525	.006	.00675
28		.00233			.00467			.007
29	0.00161	.00241	.00322	.00403	.00483			
	.00167		.00333	.00417	.005		.00667	
2 3 4	.00334		.00667	.00833	.01		.01333	
3	.005	.0075	.01	.0125	.015	.0175	.02	.0225
4	.00667	.01	.01333	.01667	.02	.02333	.02667	.03
5		.0125	.01667	.02083		.02917	.03333	.0375
6	.01	.015	.02	.025	.03	.035	.04	.045
7	.01167	.0175	.02333	.02917		.04083		.0525
8	.01334		.02667	.03333	.04	.04667	.05333	.06
9	.015	.0225	.03	.0375	.045	.0525	.06	.0675
10		.025	.03333	.04167		.05833		.075
11.	.01834			.04583			.07333	
1 Yr.	1.02	1.03	1.01	1.05	.06	.07	1.08	.09

EXAMPLE:—What is the Interest on \$50.00 for 1 year; 3 months and 16 days at 8 per cent?

Interest on \$1.00 for 1 year is . .08000

"" 1.00 "3 mo." . .02000

"" 1.00 "16 days" . .00356

Interest on \$1.00, for 1 yr., 3 mo., 16 da.. . .10356 Then $$50.00 \times .10356 = 5.178 interest at 8%.

Showing the Amount of \$1 Improved at Compound Interest for any number of years not exceeding 50.

		or an			of ye	ears n	ot exc	eea in	g 50.	
Yrs.	1%	11%	2%	21%	3%	31%	4%	41%	5%	6%
1	\$1.01	\$1.02	\$1.02	\$1.03	\$1.03	\$1.04	\$1.04	\$1.05	\$1.05	\$1.00
2	1.02	1.03	1.04	1.05	1.06	1.07	1.08	1.09	1.10	1.12
3	1.03	1.05	1.06	1.08	1.09	1.11	1.12	1.14	1.16	1.19
4 5 6	1.04	1.06	1.08	1.10	1.13 1.16 1.19 1.23 1.27 1.30 1.34 1.38 1.43	1.11	1.12 1.17 1.22 1.27 1.32 1.37	1.19 1.25 1.30 1.36	1.22 1.28 1.34	1.20
5	1.05	1.08	1.10	1.13	1.16	1.19	1.22	1.25	1.28	1.34
6	1.06	1.09	1.13	1.16	1.19	1.23 1.27	1.27	1.30	1.34	1.4
7	1.07	1.09 1.11 1.13 1.14 1.16 1.18 1.20	1.15	1.19	1.23	1.27	1.32	1.36	1.41	1.5
8	1.08	1.13	1.17 1.20 1.22	$\frac{1.22}{1.25}$	1.27	1 32 1.36	1.37	1.42 1.49 1.55 1.62 1.70	1.48 1.55	1.5
ğ	1.09	1.14	1.20	1.25	1.30	1.36	1.44	1.49	1.55	16
10	1.10	1.16	1.22	1.28 1.31 1.34	1.34	1.41	1.48 1.54	1.55	1.63 1.71 1.80 1.89 1.98	1.7
11	1.12	1.18	1.24 1.27 1.29 1.32	1.31	1.38	1.46	1.54	1.62	1.71	1.9
12 13	1.13	1.20	1.27	1 34	1 43	1.51	1.60	1.70	1.80	1.9 2.0
13	1.14	1.21	1.29	1.38	1 47	1.56	1 67	1.77 1.85	1.89	2.1
14	1.15	1.21 1.23	1 33	1.41	1 51	1.62	1.67 1.73	1 85	1 98	2.2
15	1.16	1 25	1.35	1 45	1.47 1.51 1.56	1.68	1 80	1.94	2.08	2.4
14 15 16	1 17	1.25 1.27 1.29 1.31 1.33	$\frac{1.35}{1.37}$	1.48 1.52 1.56	1 1 60	1 73	1.80 1.87	2.02	2.08 2.18 2.29 2,41 2.53 2.65 2.79	2.4 2.5 2.6 2.8
17	1 18	1 20	1.40	1.59	1 65	1 79	1 95	2.11	2 29	2.6
18	1.20	1 31	1.43	1.56	1.70	1 86	2.03	2 21	2.41	9.8
19	1 21	1 39	1.46	1 60	1 1 75	1.92	2.00	2.21	2,53	3.0
20	1 22	1 35	1.40	1.64	1 81	1.99	2 10	2.41	2.65	3.2
21	1 22	1.35 1.37	$\frac{1.49}{1.52}$	1.69	1 96	2.06	2.10	2.59	2.70	3.4
99	1.23	1.39	1.52	1.00	1.00	9 13	9.20	9 69	2.13	3.6
$\frac{\overline{22}}{23}$	1.24	1.41	1.50	1.74	1.92	2.13	9.46	9.75	2.93 3.07	96
23	1.20	1.43	1.00	1.70	2.09	0.00	9.56	0.00	9.07	4.0
24 25	1.17 1.18 1.20 1.21 1.22 1.23 1.24 1.26 1.27 1.28 1.30	1.45	1.55 1.58 1.61 1.64	1.64 1.68 1.72 1.76 1.81 1,85	1.92 1.97 2.03 2.09	2.13 2.21 2.28 2.36	1.95 2.03 2.11 2.19 2.287 2.46 2.56 2.67 2.77 2.88 3.00 3.12 3.24 3.37 3.51 3.65 3.79 4.10	1.94 2.02 2.11 2.21 2.31 2.41 2.52 2.63 2.75 2.88 3.01	3.23 3.39 3.56 3.73 3.92 4.12	4.0
26	1.20	1.45	1.67	1,00	2.16	2.45	2.07	3.14 3.28 3.43 3.58 3.75	0.00	4.2
27 27	1.50	1.40	1.07	1.90	9.00	0.40	0.00	0.14	9.70	4.8
28	1.51	1.49	1.71	1.99	2.22 2.29 2.36 2.43	2.53 2.62 2.71 2.81	2.00	9.49	3.10	5.1
29	1.04	1.54	1.79	2.00	9.49	2.04	9.00	9.50	0.04	5.4
29	1.55	1.54	1.75	2.00	2.50	2.71	5.14	3.90	4.14	5.7
30	1.31 1.32 1.33 1.35 1.36 1.37 1.39	1.49 1.52 1.54 1.56 1.59	1.01	1.95 2.00 2.05 2.10 2.15	2.43	2.01	0.29	0.70	4.32 4.54	6.0
31	1.50	1.09	1.80	2.10	2.50	2.91	3.37	3.91 4.09	4.76	0.0
32	1.37	1.61 1.63	1.88	2.20	2.98	3.01	3.51	4.09	4.70	6.4
33	1.59	1.00	1.92	2.20	2.00	3.11	5.00	4.46	5.00	0.0
34	1.40 1.42	1.66	1.71 1.74 1.78 1.81 1.85 1.88 1.92 1.96 2.00	2.52	2.75	3.22 3.33	3.79	4.27 4.47 4.67 4.88	5 25 5.52	6.8 7.2 7.6
35	1.42	1.68 1.71	2.00	2,57	2.81	3.33	3.90	4.07	5.54	8.1
36	1.43	1.71	2.04	2.20 2.26 2.32 2,37 2.43 2.49 2.56 2.62	2.50 2.58 2.65 2.73 2.81 2.90	3.45	4.10	4.00	5.79	0.1
37	1.45	1.73 1.76	2.08	2.49	2.99	3.57	4.27 4.44	5.10	6.08	8.6 9.1 9.7
38	1.46	1.76	2.12	2.56	3.07	3.70	4.44	5.53	6.39	9.1
39	1.47 1.49	1.79 1.81 1.84	2.04 2.08 2.12 2.16 2.21 2.25 2.30	2.62	2.99 3.07 3.17 3.26 3.36 3.46	3.83 3.96	4.62	5.10 5.33 5.57 5.82 6.08	6.70	19.
40	1.49	1.81	2.21	2.69	3.26	3.96	4.80	5.82	7.04	10.2
41	1.50	1.84	2.25	2.75	3.36	4.10	4.99 5.19	6.08	7.39	10.5
42	1.52	1.87	2.30	2.82	3.46	4.24	5.19	0.35	7.76	11.0
43	1.53	1.90	2.34	2.69 2.75 2.82 2.89	0.500	11 4.09	5.40	6.64	7.04 7.39 7.76 8.15	12.2
44	1.55	1.93 1.95	2.39	2.96 3.04	3.67 3.78	4.54 4.70	5.62 5.84	6.94	8.56	12.9 13.7
45	1.56	1.95	2.39 2.44 2.49	3.04	3.78	4.70	5.84	6.94 7.25 7.57 7.92	8.99	13.7
46	1.58	1.98	2.49	3.11	3.90	4.87 5.04	6.08	7.57	9.43	14.5
47	1,60		2.54	3.19	4.01	5.04	6.32	7.92	9.91	15.4
48	1.61	2.04	2.59	3.27	4.19	5.21	6.57	8.27	10.40	16.
49	1.63	2.07 2.11	2.64	3.35	4.26	5.40	6.88	8.64	10.92	17.3
50	1.64	2.11	2.6	3.44	4.38	5.58	7.11	1 9.03	11.47	118.4

Table showing the net amount of earnings of ONE CENT to FIFTY DOLLARS per day for FIVE YEARS of 313 working days, without interest and with interest at 5, 6, 7, and 8, per cent., improved each six months.

Savings per day.	Without interest.	With interest at 5%	With interest at 6%	With interest at 7 %	With interest at 8%
1	\$15 65	\$17 53	\$17 94	\$18 36	\$18 79
2	31 30	35 07	35 88	36 72	37 58
3	46 95	52 60	53 82	55 08	56 37
4	62 60	70 13	71 76	73 44	75 16
5	78 25	87 67	89 70	91 80	93 95
6	93 90	105 20	107 65	110 16	112 74
7	109 55	122 73	125 59	128 52	131 53
8	125 20	140 27	143 53	146 88	150 32
9	140 85	157 80	161 47	165 24	169 11
10	156 50	. 175 33	179 41	183 60	187 90
15	234 75	263 00	267 11	275 39	281 84
20	313 00	350 00	358 82	367 19	375 79
25	391 25	438 33	448 52	458 99	469 74
30 1	469 50	526 00 701 33	538 23	550 79	563 69
40	626 00 782 50	876 66	717 64 897 03	734 39	751 58
50 60	939 00	1,052 00	1.076 46	917 98 1,101 58	939 48 1,127 37
70	1,095 50	1,227 33	1,255 87	1,285 17	1,315 27
80	1,202 00	1,402 66	1,435 28	1,468 77	1,503 16
90	1,403 50	1,578 00	1,614 69	1,652 37	1,691 06
\$1 00	1,565 00	1,753 33	1,794 10	1,835 96	1,878 96
2 00	-3,130 00	3,506 66	3,588 19	3,671 93	3,757 91
3 00	4,695 00	5,259 99	5,382 29	5,507 89	5,636 87
4 00	6,260 00	7,013 32	7,176 39	7,343 85	7,515 82
5 00	7,825 00	8,766 65	8,970 49	9,179 82	9,394 78
6 00	9,390 00	10,519 98	10,764 58	11,015 78	11,273 73
7 00	10,955 00	12,273 30	12,558 68	12.851 74	13,132 69
8 00	12,520 00	14,027 63	14,352 78	14,688 70	15,031 65
9 00	14,085 00	15,779 93	16,146 87	16,523 67	16,910 60
10 00	15,650 00	17,533 29	17,940 96	18,359 63	18,789 56
15 00	23,475 00	26,299 94	26.711 46	27,539 45	28,184 34
20 00	31.300 00	35,066 58	35,881 94	36,719 26	37,579 12
25 00	39,125 00	43,833 23	44,852 43	45,899 08	46,973 89
30 00	46,950 00	52,599 88	53,822 91	55,078 89	56,368 67
35 00	54,775 00	61,366 52	62,793 40	64,258 71	65,763 45
40 00	62,600 00	70,133 17	71,763 88	73,438 52	75,158 23
45 00	70,425 00	78,899 82	80,734 37	82.618 34	84,533 01
50 00	78,250 00	87,666 46	89,704 86	91,798 15	93,947 79

TIME AT WHICH MONEY DOUBLES AT COMPOUND INTEREST.

At 10 per cent interest, in 7 years 3½ months; at 9 per cent., in 8 years ½ month; at 8 per cent., in 9 years at 7 per cent., in 10 years 3 months; at 6 per cent., in 11 years 11 months; at 5 per cent., in 14 years 2½ months; at 4 per cent., in 17 years 8 months; at 3 per cent., in 23 years 5½ months; at 2 per cent., in 35 years.

HANDY INTEREST RULES.

For finding the interest on any principal for any number of days, multiply in each case the dollars by the number of days, and for ascertaining at the rate of—

3	per cent.,	Divide by		9 r	er cent.,	Divide b	
4	" "	44	90	10	"	1.6	36
5	66	4.6	72	12	44	"	30
6	6.6	46	60	15	46	6.	24
7		- 44	52	18	4.6	66	20
8	• 6	66	45	20	- "	"	18

Then by cutting off the two right hand figures, you have the interest in dollars and cents.

Example:—Interest on \$50 for 30 days at 4 per cent., \$0.50 equals 15.00, which divided by 90 equals 1643, the required result.

CALCULATING INTEREST.

To find the interest on any given amount for a given time:

For 1 per cent., multiply the amount by the number of days and divide by 36,000.

For 2 per cent., multiply the amount by the number of days and divide by 18,000.

For 3 per cent., multiply the amount by the number of

days and divide by 12.000.

For 4 per cent., multiply the amount by the number of days and divide by 9.000.

For 5 per cent., multiply the amount by the number of days and divide by 7.200.

For 6 per cent., multiply the amount by the number of

days and divde by 6,000.

For 7 per cent., multiply the amount by the number of days and divide by 6,000 and add \(\frac{1}{6}\).

For 8 per cent., multiply the amount by the number of days and divide by 4,500.

For 9 per cent., multiply the amount by the number of days and divide by 4,000.

For 10 per cent., multiply the amount by the number of days and divide by 3,600.

For 11 per cent., multiply the amount by the number of days and divide by 3,600 and add $\frac{1}{10}$.

For 12 per cent., multiply the amount by the number of days and divide by 3,000.

For 13 per cent., multiply the amount by the number of

days and divide by 3,000 and add 12.

For 14 per cent., multiply the amount by the number of days and divide by 3,000 and add \(\frac{1}{6} \).

For 15 per cent., multiply the amount by the number of days and divide by 2,400.

The formula is as follows:

Principal
$$\times$$
 number of days $\div \frac{36,000}{\text{Rate } \%} = \text{interest.}$

Table showing the number of days from any given day in one month to any given day in another month.

Mo.	Ja.	Fe.	M.	Ap.	Ma.	Ju.	J'y.	Au.	Se.	Oc.	No.	De.
Jan.	365	31	59	90	120	151			243	273	304	334
Feb.	334	365	28	59	89			181	212	242	273	303
Mar.	306	337	365	31	61	92	122	153	184		245	275
Apr.	275	306	334	365	30	61	91		153		214	244
May.	245	276	304	335	365	31	61		123	153	184	214
Jun.	214	245	273	304	334	365	30	61	92	122	153	183
Jul	184	215	243	274	304	335	365	31	62	92	123	153
Aug.	153	184	212	243	273	304	334	365	31	61	92	122
Sep.		153	181	212	242	273	303	334	365	30	61	91
Oct.	92	123	151	182	212	243	273	304	335	365	31	61
Nov.	-61	92	120		181	212	242	273	304	334	365	30
Dec.	31	62	90	121	151	182	212	243	274	304	335	365

RULE:—Find the first given month in the left hand column, and the second given month in the line at the top of the table, and to the number of days found at the intersection of the two lines, add the difference between the days mentioned in the two given months.

When the number of days given in the first mentioned month is greater than the given number of days in the second month, then the difference of the days must be subtracted.

EXAMPLE: How many days from March 21st to the 23rd of next September.

184, the number of days at intersection of the lines, and 23-21=2, the difference of the days in the two given months. Hence 184+2=186 days.

When February has 29 days, proper allowance must be made.

INTEREST LAWS OF DIFFERENT STATES.

In the subjoined table the figures under the head "Legal" show the legal rate per cent.; those under "Special" show the highest rate allowed under special contract;

-	e*	
Penalty of Usury.	Loss of interest. None. None. None. None. None. Porfeiture of all interest. Forfeiture of contract. Forfeiture of contract. Forfeiture of all interest. None. \$300. or impisonment 6 months, or both. Forfeiture of all the interest. Forfeiture of all the interest. Forfeiture of all the interest. Forfeiture of access over 12 per cent. Forfeiture of access over 12 per cent. Forfeiture of access over 12 per cent. Forfeiture of all the interest. Forfeiture of interest.	Forfeithe of excess.
Legal. Special.	++++++++******************************	+9
Legal.	80°2	9
STATE.	Alabana. Arizona Arizona Arizona Arkansas California Colorado Connecticut Dakota. Dalaware. District of Columbia Florida Georgia Habo Illinois Indiana Indiana Iowa. Kentucky Kentucky Kentucky Mainasa.	Maryland

INTEREST LAWS OF DIFFERENT STATES (CONTINUED).

ı	- 4																									
	None (6 per cent. on judgments).	Forfeiture of excess over 7 per cent.	None.	Forteiture of all interest.	Forfeiture of all interest and costs.	None.	Forfeiture of three times the interest received.	Forfeiture of all interest.	None.	of	ot	Forfeiture of excess.	Forfeiture of interest, principal and costs.	Forfeiture of excess, Act May 28, 1858.	Forfeiture, unless a greater rate is contracted.	None.	Forfeiture of excess over 6 per cent. and \$100 fine.	None.	None,	Forfeiture of excess.	Forfeiture of contract.	None.	Forfeiture of excess.	Forfeiture of all the interest.	None.	*Rate on judgments unless otherwise expressed. † On railroad bonds only. ‡ No limit.
2	++0	22	++0	2	.12	++	91	~	175	9	x	x	15	9	++	++	2	++-	++	4	12	+4-	9	10	++	otherw
	9 9	-	9	9	22	10	91	_	9	9	9	9	2	9	9*	<u>_</u>	9	ဘ	2	ဗ	9	10	9	7	10	nless
	Massachusetts	Minnesota	Mississippi	Missouri	Nebraska	Nevada	New Hampshire		New Mexico	New York	North Carolina	Ohio	Oregon	Pennsylvania	Rhode Island	South Carolina	Tennessee	Texas	Utah	Vermont	Virginia	Washington Territory.	West Virginia	Wisconsin	Wyoming	*Rate on judgments

Statutes of Limitations—State Laws with reference to Limitation of Action, the limit of years to bring Action,

tution of Action, the time of years to orth	ty Act	
STATES Assault. Open Notes J	Judg-	Sealed &
unu hepieu- gainta hoces.	ments.	witnes'd
TERRITORIES. In etc.		Instr'ts.
Alabama 1 3 6	20	10
Arkansas	10	10
California	5	5
Colorado	3	3
Connecticut	6	17
Colorado 1 2 2 Connecticut 1 6 6 Dakota. 2 6 6 Delaware. 1 3 6 District of Columbia. 1 3 3 Florida 2 5 5	20	20
Delaware. 1 3 6 District of Columbia. 1 3 3	20	20
District of Columbia 1 3 3	12	12
Florida	20	20
Georgia 1 4 6	7	20
Idaho 3 2 4	5	5
Illinois	20	10
Indiana 2 6 20	20	20
Indiana	20	10
Kansas 1 3 5	5	15
Kentucky 1 5 5	15	15
Louisiana 1 3 5	10	20
Maine	20	20
Maryland 3 3 3	12	12
Massachu setts	20	20
Maine. 2 6 20 Maryland 3 3 3 Massachu setts, 2 6 20 Michigan 2 6 6 Minnesota 2 6 6	10	10
Minnesota 2 6 6	10	20
Mississippi. 1 3 6 Missouri. 1 4 20 Montana 2 2 4	7	7
Missouri 1 4 20	5	10
Montana	5	4
Nebraska	20	10
Nevada 2,6 6 20	20	20
New Hampshire 1	10	10
New Jersey 2 6 6	20	20
New Mexico	10	10
New York	15	15
North Carolina 1 3 10	10	10
Ohio 1 6 15	15	15
Ontario (U. Canada) 1 5 5	30	30
Oregon 2 1 6	10.	20
Pennsylvania 1 6 6	20	20
Quebec (L. Canada) 1.2 5 5	30	30
Rhode Island 1 6 6	20	20
South Carolina 2 6 6	20	20
Tennessee 1 6 6	20	
Texas 1 2 4	10	10
Utah 1 2 4	5	7
Vermont	8	/ 8
Virginia 5 5 5	10	20
Washington Territory. 2 3 6	9	20
Washington Territory. 2 3 6 West Virginia 5 5 6	10	10
Wisconsin 2 6 6	20	20
Wyoming 1 6 15	10	21

EXEMPTION LAWS OF UNITED STATES.

STATES.	Personal	Acres	Value
- i	Property.		Homestead
Alabama	\$1,000	160	\$2,000
Arizona	900		5,000
Arkansas	500	160	2,500
California	900		5,000
Colorado	1,000	S	2,000
Connecticut	500		*
Dakota	1.500	160	*
Delaware	200		*
District of Columbia	300		*
Florida	1.000	160	
Georgia	300	50	1.600
Idaho	300		5,000
Illinois.	300		1,000
Indiana	600		*
Iowa	200	40	- 11
Kansas	800	160	
Kentucky	200	100	1,000
Louisiana	-t-	160	
Maine	300	100	500
Maryland	100		*
Massachusetts,	450		800
	400	40	
		40	1,500
Minnesota	860	80	0.000
Mississippi	550	80	2,000
Missouri	300	160	1.500
Montana	900	100	5,000
Nebraska	******	160	2,000
Nevada	900		5,000
New Hampshire	450		500
New Jersey	200		1,000
New Mexico	900		5,000
New York	250		1,000
North Carolina	500		1,000
Ohio	100		1.000
Oregon	175		*
Pennsylvania	300		*
Rhode Island	500		*
South Carolina	500		1,000
Tennessee	1.200		1,000
Texas		200	5,000
Utah			1,000
Vermont	200		500
Virginia			
Washington	İ	1	İ
West Virginia	200	1	1.000
Wisconsin	450	40	2,000
Wyoming	900		5,000

^{*}No Homestead Law. †The homestead, land and personal property not to exceed \$2,000. ‡Similar to California. §Any number. || No limit.

RULES OF PARLIAMENTARY PROCEDURE.

Trace each motion to its respective references on the next page, and you master at a glance the intricacies of Parliamentary usages, comprising some three hundred points of order:

Motion to adjourn	1a * B a J x
Motion to determine time to which to ad-	
journ	2atAaJx
Motion to amend	3atAaJx
Motion to amend an amendment	$3a * A \alpha J x$
Motion to amend the rules	3a + A·b J x
Motion to appeal from Speaker's decision	
re indecorum	latAaJn
Motion to appeal from Speaker's decision	
generally	3a*AaJn
Call to order	1a*AaSn
Motion to close debate on question	1atAbJx
Motion to commit	3b † AaJx
Motion to commit	1,00
tion	latAaJx
tion Leave to continue speaking after inde-	
corum	1a*AaJx
Motion that do lie on the table	1a * CaJx
Motion to limit debate on question	latAbJx
Objection to consideration of question	1a*AbSn
Motion for the orders of the day	1a * AaSn
Motion to postpone to a definite time	4atAaJx
Motion to postpone indefinitely	3b*AaJx
Motion for previous question	1a*AbJx
Questions touching priority of business	latAaJx
Questions of privilege	3atAaJx
Reading papers	1a * A a J x
Motion to reconsider a debatable question.	3b*BaJz
Motion to reconsider an undebatable ques-	
tion	la*BaJz
Motion to refer a question	3btAaJx
Motion that committee do not rise	1a * BaJx
Question whether subject shall be discussed	1a*AbSn
Motion to make subject a special order	3a+AbJx
To substitute in the nature of an amend-	
ment	3atAaJx
Motion to suspend the rules	1a * B b J x
Motion to take from the table	la*CaJx
To take up question out of its proper order	la*AbJx
Motion to withdraw a motion	1a * AaJx
Questions of precedence of questions	567891012
Forms in which questions may be put131	14 15 16 17 18 19

RULES OF PARLIAMENTARY PROCEDURE-Condensed.

1. Question undebatable: sometimes remarks tacitly allowed.

2. Undebatable if another question is before the assembly.

3. Debatable question.

4. Limited debate only on propriety of postponement.

a. Does not allow reference to main question.

b. Opens the main question to debate.

*. Cannot be amended.

May be amended.
 Can be reconsidered.

B. Cannot be reconsidered.

C. An affirmative vote on this question cannot be reconsidered.

b. Requires two-third vote unless special rules have been enacted.

a. Simple majority suffices to determine the question.

J. Motion must be seconded.

Does not require to be seconded.

x. Not in order when another has the floor. Always in order though another may have the floor.

z. May be moved and entered on the record when another has the floor, but the business then before the assemby may not be put aside. The motion must be made by one who voted with the prevailing side, and on the same day the original vote was taken.

5. Fixing the time to which an adjournment may be

made; ranks first.

6. To adjourn wihout limitation; second.

7. Motion for the Orders of the Day; third. 8. Motion that .. do lie on the table; fourth. 9. Motion for the previous question; fifth.

10. Motion to postpone definitely; sixth.
12. Motion to commit; seventh.

13. Motion to amend; eighth.

14. Motion to postpone indefinitely; ninth.

15. On motion to strike out words, "Shall the words stand part of the motion?" unless a majority sustains the words they are struck out.

16. On motion for previous question the form to be observed is, "Shall the main question be now put?" This,

if carried, ends debate.

17. On an appeal from the Chair's decision, "Shall the decision be sustained as the ruling of the house?" chair is generally sustainded.

18. On motion for Orders of the Day, "Will the house now proceed to the Orders of the Day?" This, if carried,

supersedes intervening motions.

19. When an objection is raised to considering question, "Shall the question be considered?" objection may be made by any member before debate has commenced, but not subsequently.

Law of Grace on Sight Drafts, and Damages on Protested Bills of Exchange.

Frotesteu	bills of Exchange.
STATES.	ON SIGHT DRAFTS.
Alabama	Grace is allowed.
Arizona	Grace allowed.
Arkansas	No statute.
California	No grace.
Colorado	No grace.
Connecticut	No grace.
Dakota	Allowed by statute of 1873.
Delaware	No grace.
District of Columbia	No grace.
Florida	No grace by custom.
Georgia	No grace. Act Feb. 8, 1850.
Idaho	No grace.
Illinois,	No grace.
Indiana	Grace allowed.
Iowa	Grace allowed.
Kansas	Grace allowed.
Kentucky	Grace allowed.
Louisiana	Grace not allowed by custom.
Maine	Grace allowed. Rev. St'ts., p. 264.
Maryland	Grace not allowed.
Massachusetts,	Grace allowed.
Michigan	Grace allowed by custom.
Minnesota	Grace allowed by custom.
Mississippi	Grace allowed by custom.
Missouri	Grace not allowed by custom.
Montana	Grace allowed by custom,
Nebraska	Grace allowed by statute.
Nevada	Grace not allowed.
New Hampshire	Grace allowed by Rev. St'ts p 389.
New Jersey	Grace allowed by statute.
New Mexico	Grace allowed.
New York	Grace not allowed. Act Ap'l, 1857.
North Carolina	Grace allowed. Act Jan'y, 1849.
Ohio	Grace not allowed. Act Feb. 1861.
Oregon	Grace allowed by statute.
PennsylvaniaRhode Island	Grace not allowed. Act May 1857. Grace not allowed. Act May 1857.
South Carolina	Grace allowed. Act May 1897.
Tennessee	Grace not allowed by statute.
	Grace not allowed by statute.
TexasUtah	Grace allowed by custom.
Vermont	Grace not all'ed. St'te Jan. 1873.
Virginia	Grace not allowed by statute 1873.
Washington	No Grace.
West Virginia	No grace by custom.
Wisconsin	Grace all'ed. Rev. statutes, 1849.
Wyoming	Grace allowed by custom.
Canada	Grace allowed by custom.

The damages on a domestic Bill of Exchange or note, consist of Notaries' fees, postage, &c., and range from \$1.25 to \$2.50, according to the Statute of the State where it goes to protest. Foreign Bills, that is, drafts drawn by a person out of the United States upon another within the same, or the reverse, and protested for non-paymeut, are subject to a total expense for protest, &c., of from \$1.50 upwards.

WEIGHTS AND MEASURES.

AVOIRDUPOIS WEIGHT.

16 drachms	equal	1 ounce.
16 ounces	-66	1 pound.
25 pounds	• 6	1 quarter.
4 quarters	6.	1 hundred.
20 hundred	"	1 ton

The English quarter is 28 fbs. Hundred weight 112 fbs. Ton 2240 pounds.

TROY WEIGHT.

24 grains	equal	1 pennyweight.
20 pennyweight	• 6	1 ounce.
12 ounces	44	1 pound.

Weighing Diamonds 31/3 grains equal one carat.

The standard unit of weight (the Troy fb.) is equal to 22.794422 inches of distilled water, at the temperature of 39.83°, the barometer being at 30 inches. This is the unit measure of weight, (in the U. S. Mint).

7000 Troy	grains	equal	1 fb.	avoirdupois
175 "	pounds	-66	144 Tb.	46
175 "	ounces	44	192 oz.	**
4371/2 "	grains	44	1 oz.	44

APOTHECARIES WEIGHT.

20 grains (gr)	equal	1 scruple, or o
3 scruples	- 44	1 dram, or 3
8 drams	66	1 ounce, or 3
12 ounces	"	1 pound, lb or Ib.

APOTHECARIES FLUID MEASURE.

60 minims (or drops) 8 fluid drams	equal	1 fluid dram fl 3. 1 " ounce fl 3.
16 " ounces 8 pints	44	1 pint. 1 gallon.

45 drops, or a common teaspoonful, make about 1 fluid dram; 2 teaspoonfuls about 1 fluid-ounce; a wineglassful about 1½ fluid-ounces; and a teacupful about 4 fluid-ounces.

LIQUID OF WINE MEASURE.

TI COID	T IIIII DAT	allo Citili.
4 gills	equal	1 pint.
2 pints	• •	1 quart.
4 quarts	44	1 gallon.
311/2 gallons	, 44	1 barrel.
42 gallons	66	. 1 tierce.
63 gallons	6.6	1 hogshead,
2 tierces	6.6	1 puncheon.
2 hogsheads	66	1 pipe or butt,
2 pipes	66	1 tun.

The following cylinders contain some of these measures very closely.

	Dia	meter.	Не	ight	t.		Dia	meter.	Hei	ght.
Gill	13/4	inches.		ins.	1	Gallon	7 i	nches.	6	ins.
1/2 Pint	$21\sqrt{4}$	4.	35	8 "	2	4.	7	44	12	- 66
Pint	$31/_{2}$	4.6	3	"	8	4.6	14	66	12	4+
Quart	31/2	- 66	6	4.6	10	+ 6	14	**	15	6.6

The Standard Unit of Liquid Measure adopted by the U.S. Government is the Winchester Wine Gallon, which contains 231 cubic inches, and holds 8.339 fbs. Avoirdupois of distilled water, at its maximum density weighed in air, the barometer being at 30 inches.

The *Imperial Gallon* adopted by Great Britain contains 277.274 cubic inches, containing 10 lbs. Avoirdupois of distilled water, weighed in air, at a temperature of 62°, the barometer at 30 inches and equals 1.20032 U. S. gallons.

To convert Imperial gallons to U. S. gallons multiply by 1.20032. And to convert U. S. gallons to Imperial gal-

lons multiply by .83311.

UNITED STATES AND BRITISH LINEAL MEASURE.

The Standard Unit of the U. S. and British linear measure is the yard. It was intended to be exactly the same for both countries, but in reality the U. S. yard exceeds the British Standard by .00087 inch. The actual Standard of length of the U. S. is a brass scale 82 inches long prepared for the Coast Survey and deposited in the office of Weights and Measures at the U. S. Treasury Department Washington. The yard is between the 27th and 63rd inches of this scale. The temperature at which it is used in the U. S. Coast Survey, is 62° Fahrenheit.

The Imperial (British) standard yard is referred to a natural standard, which is the length of a pendulum vi-

brating seconds in vacuo in London, at the level of the sea; measured on a brass rod, at a temperature of 62°.

LONG MEASURE.

12 inches	equal	1 foot.
3 feet	-60	1 yard.
51/2 y'ds or 161/2 ft	66	1 rod.
40 rods	66	1 furlong.
8 furlongs	66	1 mile

One yard is .000568 of a mile. One inch is .0000158 of a mile.

SQUARE MEASURE.

144 square inches	equal	1 sq. foot.
9 " feet	- "	1 sq. yard.
3014 " yards	66	1 sq. rod.
40 " rods	66	1 rood.
4 roods	661	1 acre.
640 acres	66	1 sq. mile.

An acre is 63.5701 yards square; or 208.710321 feet square; 220 feet by 198 feet square equal 1 acre.

SURVEYOR'S MEASURE.

7.92 inches	equal	1 link.
25 links	-6.	1 rod.
4 rods	66	1 chain (66 ft).
80 chains	66	1 mile.

A Nautical mile contains 6080 feet. A Statute mile 5280 feet. Three Nautical miles 1 league; 20 leagues 1 degree; 6 feet 1 fathom. One knot or geographical mile is 1-60 of a degree; 3 knots make 1 marine league; 60 knots or 69.19 statute miles equal 1 degree. A hair's breadth is 1-48 part of an inch. A ship's cable is a chain usually about 120 (720 ft.) fathoms long.

DRY MEASURE.

2 pints	equal	1 quart.
4 quarts	66	1 gallon.
2 gallons	46	1 peck.
4 pecks	"	1 bushel.

The standard bushel is the Winchester, containing 2150,42 cubic inches, or 77.627 avoirdupois pounds of distilled water at its maximum density. Its diameter (cylinder) inside is 181/2 inches, outside 191/2 inches, its depth is 8 inches.

The Imperial (English) bushel equals 2218,192 cubic inches, equals 1.03152 U. S. bushels.

36 U. S. bushels equals 1 chaldron equals 58.658 cubic feet and weighs 3,136 pounds.

Heaped bushel, 19½ inches in diameter, cone 6 inches equals 2815,4872 cubic inches.

32 British or Imperial bushels are equal to 38 U. S. bushels. The English quarter equals 814 (nearly) U. S. bushels and contains 10.2694 cubic feet. Four quarts or 1/2 peck equals 282 cubic inches.

SOLID OR CURIC MEASURE.

1728	cubic	inches	equal	1 cubic foot.
27	44	feet	-66	1 "yard.
128	4.4	feet	66	1 cord.

8 feet long, 4 feet wide, 4 feet high, equal 128 cubic feet or 1 cord of wood. 2434 cubic feet equal 1 perch of stone, or masonry. One cubic foot of water weighs 62142 pounds. A cubic foot contains 2200 cylindrical inches, 3300 spherical inches, or 6600 conical inches.

CLOTH MEASURE.

21/4 in	nches		equal	1 nail.
. 4 n	ails			1 quarter.
4 a	uarters		44	1 vard.
3	6.6	100	66	1 ell Flemish.
5	4.6		66	1 ell English.
6	6.6		66	1 ell French.
4 2-15	"		"	1 ell Scotch.

METRIC, OR FRENCH LIQUID AND DRY MEASURE.

	Litres.						
Millilitre ed	qual .001	equal	.061	= {	Liquid Dry	.00845 $.0018$	gill.
Centilitre							
Decilitre	equal .1	equal	6.1	= {	Liquid Dry	.845 .18	gill. pint.
Litre equa	al 1. eq	ual 6	1.02	= {	Liquid Dry	2.113 1.8	pints.
Decalitre e	equal 10. e	equal 6	10.16	=	Liquid Dry	2.641 2.27	galls.
		U. S.	Cu.	Ft.			
				(Liquid	96 414	malle

 $\begin{array}{c} \textit{U. S. Cu. Ft.} \\ \textit{Hectolitre equal 100. equal 3.531} = \left\{ \begin{array}{c} \textit{Liquid 26.414 galls.} \\ \textit{Dry} & 2.837 \textit{ bush.} \end{array} \right. \\ \textit{Kilolitre equal 1000. equal 35.31} = \left\{ \begin{array}{c} \textit{Liquid 264.141 gals.} \\ \textit{Dry} & 28.374 \textit{ bush.} \end{array} \right. \\ \textit{Myrialitre equal 10000. equal 353.1} = \left\{ \begin{array}{c} \textit{Liquid 2641.4 gals.} \\ \textit{Dry} & 283.7 \textit{ bush.} \end{array} \right. \\ \end{aligned}$

METRIC, OR FRENCH LINEAL MEASURE.

		Metres.		U. S. Me	easure.
Mynametre	equal	10,000.	equal	6.2137	miles.
Kilometre	**	1,600.	**	.62137	66
Hectometre	4.6	100.	66	328.1	feet.
Decametre	+6	10.	66	393 7	inches.
Metre	66	1.	66	39.37	**
Decimetre	66	′ .1	4.	3.937	
Centimetre	4.6	.01	66	.3937	- 66
Millimetre	66	.001	6.6	.03937	"

METRIC, OR FRENCH SQUARE MEASURE.

	S	q. Met	res.	U. S.	Sq.	Measure.
Sq. Centimetre	equal	.01	equal	.155	sq.	inches.
Sq. Decimetre	744	.1	**	1.55	sq.	6.6
Centiare	6.6	1.	**	10.763	sq. i	eet.
Are	66	10.	66	119.6	sq. y	ards.
Hectare	66	100.	66	2,47	Acre	
Sq. Kilometre	equal	.38607	sq. mile	s equa	ıl 24'	acres.

Sq. Mynametre equal 38.607 sq. miles equal 247 acres.

METRIC, OR FRENCH CUBIC OR SOLID MEASURE.

	Cu	ı. Metres		U. S. (Cu. Measure
Cubic Centimetre	equal	.0001	equal	6.10165	cu. inches.
" Decimetre	-66	.001	-66	61.0165	cu. "
Centistere	66	.01	4.6	.353105	cu. feet.
Decistere	4.6	.1	. 66	3.53105	cu. "
Stere	66	1.	6.6	1.3078	cu. yards.
Decastere	6.6	10.	6.6	13.078	cu. "
Hectostere	66 :	100.	" 1	30.78	C11. "

METRIC, OR FRENCH WEIGHTS.

		Grammes.		Avoi	r.
Millegramme	=	.001	=	.00003528	ounce.
Centigramme	=	.01	=	.0003528	
Decigramme	=	.1	=	.003528	**
Gramme	= ^	1.	=	.03528	44
Decagramme	=	10.	=	.3528	• 6
Hectogramme	=	100.	=	3.52758	4.6
Kilogramme	=	1.000.	=	35.2758	66
Myriogramme	- =	10,000.	=	22.04737	pounds.
Quintal	=	100,000.	=	220.4737	**
Tonneau	=1	,000,000.	=	2204.737	4.6

THE FRENCH METRE.

The French metre is intended to be the one ten-millionth part of the distance from either pole of the earth to the equator; but after it had been introduced into use, errors were discovered in the calculations employed for ascertaining that distance; so that the French metre, like the British standard yard, is not what it was intended to By the British standard, the length of the metre is, approximately, 1.03633 yard; or 3.280899 feet; or 39.37079 inches. By the U. S. standard it is, very approximately, 1.035697 yard; or 3.280709 feet; or 39.368505 inches.

The unit of Length is the Metre. The unit of Weight is the Gram. The unit of Capacity is the Liter. The unit of

Area is the Are. A Cubic Metre is called Stere.

The higher denominations are expressed by prefixing to the unit, the Greek words: Deca (10), Hecto (100), and Kilo (1000). Thus, a decametre = 10 Metres; a hectoliter = 100 Liters; a kilogram = 1000 Grammes.

The lower denominations are expressed by prefixing the Latin words: Deci (10), Centi (100), Milli (1000). Thus, a decigram is the 10th part of a Gram; a centimetre is the

100th part of a Metre, etc.

COMMON MEASURES AND WEIGHTS, WITH THEIR METRIC

EQUIV	/ALENTS.
Common Measure.	Equivalents.
An inch	2.54 Centimetres.
A foot	.3048 Metres.
A yard	.9144 "
A rod	5.029 "
A mile	1.6093 Kilometres.
A square inch	6.452 Sq. Centimetres
A square foot	.0929 Sq. Metres.
A square yard	.8361 Sq. "
A square rod	25.29 Sq. "
An acre	.4047 Hectare.
A Square mile	259,008 Hectares.
A cubic inch	16.39 Cu. Centimetres
A cubic foot	.02832 Cu. Metre.
A cubic yard	.7646 Cu. ''
A cord	3.624 Steres.
A liquid quart	.9465 Liter.
A gallon	3.786 Liters.
A dry quart	1.101
A peck	8.811 "
A bushel	35.24 "
An ounce Avoir.	28.35 Grams.
A pound "	.4536 Kilogram.
A ton "	.9072 Tonneau.
A grain Troy	.0648 Gram.
An oz; "	31.104 Grams.
A 1b., "	.3732 Kilogram.

WAGES TABLE-YEARLY, MONTHLY, WEEKLY AND DAILY-TEN HOURS TO THE DAY.

WAGES PER YEAR.	WAGES PER MONTH.	WAGES PER WEEK.	WAGES PER DAY.	WAGES PER YEAR.	WAGES PER MONTH.	WAGES PER WREE.	WAGES PER DAY.
\$1000 is	\$83,33	\$19.23	\$2.74	\$295 is	\$24.58	\$5.67	81c.
975	81 25	18.75	2 67	290 -	24.17	5.58	79
950	79.17	18.27	2.60	285	23 75	5.48	78
925	77.08	17.79	2.53	280	23.33	5.38	77
000	75 00	17.31	2.47	275	22.92	5.29	75
875	72.93	16.83	2.40	270	22.50	5.19	74
850	70.83	16 35	2.33	260	21.67	5.00	71
825	68.75	15.87	2.26	250	20.80	4.81	69
>00	66.67	15.39	2.19	240	20.00	4.62	66
775	64.58	14.90	2.12	235	19 58	4.52	64
750	62.50	14.42	2.05	230	19.17	4.42	63
725	60.42	13.94	1 99	225	18.75	4 33	62
700	58.33	13.46	1.92	220	18.33	4.23	60
675	56.25	12.99	1.85	215	17.92	4 13	59
650	54.17	12.50	1.78	210	17.50	4.04	58
625	52.08	12.02	1.71	205	17.08	3 94	56
600	50.00	11.54	1.64	200	16.67	3 85	55
675	47.92	11.06	1.58	195	16.25	3.75	53
550	45.83	10 58	1.54	190	15.83	3.64	52
525	43.75	10.10	1.44	185	15.42	3.56	51
500	41.67	9.62	1.37	180	15.00	3 46	49
475	39.58	9.13	1.30	175	14.58	3.37	48
450	37.50	8.66	1.23	170	14.17	3.27	47
425	85.42	8.17	1.16	165	13.75	3 17	45
400	33.33	7.69	1.10	160	13.33	3.08	44
390	32.50	7.50	1.07	155	12.92	2.98	42
330	31.67	7.31	1.04	150	12.50	2.88	41
375	31.25	7.21	1.03	145	12.08	2.79	404
370	30.83	7.12	1.01	140	11.67	2 69	38
360	30.00	6.92	.99	135	11.25	2.60	37
350	29.17	6.73	.96	130	10.83	2 50	30
31)	28.33	6.54	.93	125	10 42	2.40	34
330	27.50	6.35	.90	120	10.00	2 31	33
325	27 08	6.25	89	115	9.58	2.21	31
320	26 67	6.15	.88	110	9.17	2.11	30
310	25.83	5.96	85	105	8.75	2.02	20
309	25.00	5.77	.85 .82	100	8.33	1.92	: 27

TABLE OF BOARD OR RENT, BY THE WEEK, SHOW-ING IT FOR DAYS.

. 25	.50	.75	SI	82				Days.					\$11		
.02 .04 .07	.07 .14	.20	.14 .29 .43	.29 .57 .86	1 29	.29 .57 1.14 1.71 2.29	2.14	3	1.71	$\frac{2.29}{3.43}$	2.57 3.86	2.86 4.29	79 1.57 3.14 4.71 6.29	3.43 5.14	6.43
.18 .21 .25	.36 .43 .50	.54	.71	1.43	2.14	2.25 2.86 3.43 4.00	3.57	5	4 29	5 71	6 43	7 14	7.86 9.43 11.00	8 57	10 21

TABLE OF WAGES

For One Week, Two Weeks, Three Weeks, or Four Weeks.

EK.	DAYS.	\$1 00	\$1 50	\$2 00	\$2 50	\$3.00	\$3.50	\$4.00	\$4.50	\$5.00	\$5.50	\$6.00
FIRST WERE.	123456	.16% .331/3 .50 .66% .831/8	.25 .50 .75 1.00 A.25 1.50	.33½ .66½ 1.00 1.33⅓ 1.66¾ 2.00	.41% .831% 1.25 1.66% 2.081% 2.50	,50 1.00 1.50 2.00 2.50 3.00	.58½ 1.16% 1.75 2.83¼ 2.91½ 3.50		.75 1.50 2.25 3.00 3.75 4.50	.83½ 1.66% 2.50 3.33½ 4.16% 5.00		1.00 2.00 3.00 4.00 5.00 6.00
2KD WEEK.	7 8 10 11 12	1.16% 1.33% 1.50 1.66% 1.83% 2.00	2.25	2.33½ 2 66% 3.00 3.33¼ 3 66% 4.00	2.91% 3.33% 3.75 4.16% 4.58% 5.00	3.50 4.00 4.50 5.00 5.50 6.00	4.08½ 4.66⅔ 5.25 5.83⅓ 6.41⅔ 7.00	4.66 ² / ₃ 5 33 ¹ / ₈ 6.00 6.66 ² / ₄ 7.33 ¹ / ₃ 8.00	5,25 6,00 6 75 7,50 8,25 9,00	5.83½ 6.66% 7.50 8.33½ 9.16% 10.00	6.41% 7.331% 8.25 9.16% 10.081% 11.00	7.00 8.00 9.00 10.00 11.00 12.00
SRD WEIR.	13 14 15 16 17 18	2.16% 2.331% 2.50 2.66% 2.831% 3.00	3.25 3.50 3.75 4.00 4.25 4.50	4.33\% 4.66\% 5.00 5.33\% 5.66\% 6.00	5.41% 5.831% 6.25 6.66% 7.081% 7.50	6.50 7.00 7.50 8.00 8.50 9.00	7.581/3 8.162/3 8.75 9.331/3 9.912/3 10.50	10 662/4	12.00	12.50 13.331/3 14.162/3	11.91% 12.831% 13.75 14.66% 15.581% 16.50	13.00 14 00 15.00 16 00 17.00 18.00
dra Week.	19 20 21 22 23 24	3.16% 3.331/s 3.50 3.66% 3.831/s 4.00	4.75 5.00 5.25 5.50 5.75 6.00	6.331/4 6.662/3 7.00 7.331/4 7.662/4 8.00	7.91% 8.33% 8.75 9.16% 9.58%	10.00 10.50 11.00 11.50	11.60% 12.25 12.831/3 13.41%	14.662/6 15.331/6	15.00 15.75 16.50 17.25	16.66% 17.50 18.331% 19.16%	18.831/3	19.00 20.00 21.00 22.00 23.00 24.00
												24.00
X.	DAYS.	\$6.50	\$7.00	\$7.50		\$9.00	\$10	\$11	\$12	\$13	\$14	\$15
FIRST WEEK.	12034	\$6.50 1.0814 2.16% 3.35 4.3314	\$7.00 1.16 ² / ₃ 2.33 ¹ / ₃ 3.50 4.66 ² / ₃ 5.83 ¹ / ₃ 7.00	\$7.50 1.25 2.50 3.75 5.00 6.25 7.50		\$9.00 1.50 3.00 4.50 6.00 7.50		\$11 1.831/5 3.669/8	\$12 2.00 4.00 6.00 8.00 10.00	\$13 2 16% 4.331% 6.50		\$15 2.50 5.00 7.50
2ND WEEK. FIRST WEEK.	1223456 7890011	\$6.50 1.0814 2.1673 3.35 4.3314 5.4173 6.50 8.6673	1.16 ² / ₃ 2.331/ ₃ 3.50 4.66 ² / ₃ 5.831/ ₃ 7.00 8.16 ² / ₃ 9.331/ ₃	1.25 2.50 3.75 5.00 6.25 7.50 8.75 10.00	\$8.00 1.3314 2.6658 4.00 5.3314 6.6658 8.00 9.3314 10.6668	1.50 3.00 4.50 6.00 7.50 9.00 10.50 12.00 13.50 16.50	\$10 1.66% 3.33% 5.00 6.66% 8.33%	\$11 1.8314 3.6654 5.50 7.3314 9.1656 11.00 12.8314 14.6624 16.50	\$12 2.00 4.00 6.00 8.00 10.00 12.00 14.00 16.00 18.00 20.00 22.00	\$13 2 16% 4.331% 6.50 10.831% 13.00 15.16% 17.331% 19.50	2.331/4 4.662/4 7.00 9.331/4 14.00 16.331/4 18.662/4 18.662/4	\$15 2.50 5.00 7.50 10.00 12.50 15.00 17.50 20.00 22.50
WEEK.	123456 78990112 341567	\$6.50 1.0814 2.1673 2.357 4.3314 5.4173 6.50 9.75 10.8313 10.8313 11.9173 13.00 1 14.0314 15.1676	1.16 ³ / ₄ 2.331/ ₃ 3.50 4.66 ³ / ₄ 5.831/ ₃ 7.00 8.16 ³ / ₂ 9.331/ ₃ 10.50 11.66 ³ / ₂ 12.831/ ₃	1.25 2.50 3.75 5.00 6.25 7.50 8.75 10.00 11.25 12.50 13.75 15.00	\$8.00 1.331/4 2.66% 4.00 5.331/4 8.00 9.331/2 10.66% 12.00 13.331/4 14.66% 16.00 17.331/4 18.66%	\$9.00 1.50 3.00 4.50 6.00 7.50 9.00 10.50 13.50 15.00 15.00 17.50 21.00 22.50 22.50 22.50 25.50	\$10 1.66% 3.33½ 5.00 6.65% 8.33½ 10.00 11.66% 15.00 16.65% 15.00 16.66% 20.00 21.66% 23.33½ 20.00	\$11 1.83½ 3.66½ 5.50 7.33½ 9.16½ 11.00 12.83¼ 16.50 18.33¼ 20.16½ 22.00 23.63½ 25.66½	\$12 2.00 4.00 6.00 8.00 10.00 12.00 14.00 16.00 20.00 21.00 22.00 24.00 28.00 38.00 3	\$13 2 16% 4 .331/4 6 .50 8 .66% 10 .831/4 13 .00 15 .16% 21 .66% 22 .831/4 26 .00 28 .16% 30 .331/4 32 .50	2. 3314 4. 66% 7. 00 9. 3314 11. 66% 14. 00 16. 3314 18. 66% 21. 00 23. 3314 25. 66% 28. 00	\$15 2.500 5.000 7.50 10.00 12.50 15.00 17.50 22.50 22.50 22.50 23.50 33.00 37.50 40.00

TABLE OF WAGES BY THE WEEK, FROM \$2 TO \$20.

\$2	\$21/2	\$3	\$31/6	\$4	\$41/6	\$5	Days	\$7	88	\$9	\$10	\$12	\$15	\$20
.29	.36	.43	.50	.57	.64	.71			1.14	1.29	1.43	1.71	2.14	2.86
.08		~.13		.17		.21		.29	.33		.42	.50	.63	.83
.17		.25		,33		.42	1 1/6	.58		.75		1.00		1.67
.25	.31	.38		.50		.63			1.00					2.50
.33	.42	.50							1.33					3.33
,50		.75			1/13				2.00		2.50			5.00
.67	.83	1.00			1.50				2.67		3.33			
.83	1.04				1.88				3,33		4.17			
					2.25				4.00		5.00			10.00
					2.63				4.67					11.67
					3.00				5.33				10.00	
					3.38				6.00				11.25	
					3.75				6.67				12.50	
					4.18				7.33				13.75	
2.00	2.50	3,00	[3.50]	4.00	4.50	5.00	6	7.00	8.00	9.00	11).00	12.00	15.00	20.00

EXPLANATIONS.—The rate per week will be found in the top lines, and the time, in the middle columns. For example, at \$7 per week, the wages for four-and-a-half days will amount to \$5.5.

TABLE OF WAGES BY THE DAY .- The 10 Hour System.

\$1	\$11/4	\$11/2	\$134	\$2	\$21/4	\$21/2	Hours.	\$23/4	\$3	\$31/4	\$31/2	\$1	\$11/2	\$5(
.10			.18	.20			1	.28	.30	.33	.35	.40	.45	. 50
.20								.55	.eo					1.00
.30		.45		.60		.75 1.00		1 10	.90				$\frac{1.35}{1.80}$	
.50		.75			1.13			1.38					2.25	
.60	.75	.90	1.05	1.20	1.35	1.50	6	1.65	1.80	1.95	2.10	2.40	2,70	3.00
.70			1.23										3.15 3.60	
			1.58				å	2 48	2 70	2 93	3 15	3 60	4.05	4.50
			1.75										4.50	

TABLE OF WAGES BY THE DAY .- The 8 Hour System.

\$1	\$11/4	\$11/2	\$134	\$2	\$21/4	\$21/2	Lours.	\$23⁄4	\$3	\$31/4	\$31/2	\$1	\$11/2	\$3
.13	.16	.19	.22	.25	.28	.31	1	.34	.38	41	44	.50	.56	.63
.25		.38	.44	.50				.69	.75	.81	.88	1.00	1.13	1.25
.38					.84									1.88
.50	.63		1.09			1.25								2.50
.95			1.31				6	2.06	2 25	2.05	2 63	3 00	3 38	3.13.
			1,53											4.38
1.00	1.25	1.50	1.75	2 00	2.25	2 50	8	2.75	3 00	3.25	3 50	4.00	4.50	5 00

TABLE OF WAGES BY THE WEEK. Ten Hours Rer Day.

Per Week.	5 Days.	4 Days.	3 Days.	2 Days.	Day.	Day.	Day.	/1 Hour.
2.00	1.66%	1.331/6	1.00	.66%	.331/3	.16.66	. 8 33	3.56
2.50	2.0813	1.65%	1.25	.8046	212/3	.20 08	.10 1/2	4 1
3.50	2.91%	2.3314	1.75	1 16%	.581/3	. 29 ֆ	.10 1/2	5.08
4.00	3.331/6	2.66%	2.00	1.331/3	.66%	.33 33	.16.66	6 66
4.50	3.75	3.00	2.25	1.50	.66% 75 .831⁄s	.37 1/2	.18 3/4	7 14
j.00	4.16%	3.3316	2.50 2.75	1.66%	.831/6	.41.66	.20.08	8.33
5.50	4.16%	3.66%	2.75	1.831/3	91%	.45.08	.22.23	9 1
6.00	5,4123	4.3313	3.25	2.16%	1.081/8	.54 }	.27.12	10.08
7.00	5,831/3	4.66%	3.50	2.3613	1.16%	.58.33	.29 1	11.66
7.50	6.25	5.00	3.75	2.50	1.25	.62 1/2	.31 1/4	12 1/4
8.00	6.66%	5.331/3	4.00	2 662/8	1.331/3	.66.66	.33.33	13,33
9.00	7.50	6.00	4.50	3.00	1.50	.75	.37 1/2	15 .
10.00	8.3314	6.66%	5.00	3.331/3	1.66%	.83.33	.41.66	16.66
11.00	9.16%	7.331/4	5.50	3.66%	1.831/3	.91.66	.45,08	18.33
13.00	10.831/6	8.66%	6.50	4.331/3	2.16%	1.08.33	.54 4	21.66
14.00	11.66%	9.331	7.00	4.66%	2.331/6	1.10.66	.58.66	23.33
16.00	13.331	10.66%	8.00	5.361/3	2.66%	1.33.33	.66.66	26.66
17.00	14 16%	11.3314	8.58	5.66%	2.831/4	1.41.66	.70.08	28.33
19 00	15.831	12.6624	9.50	6.331/3	3.16%	1,58.33	.70 3	31.66
20.00	16 66%	13 3313	10.00	6.66%	3 331/4	1.66.66	.83.33	31,66 33,33
21.00	17.50	14.00	10.50	7.00	3.50	1.75	.87 1/4	35
22.00	18.331/4	14.66%	11.00	7.331/4	3 66%	1,83,33	.91.66	36.46
23.00	19.16%	15.331/9	11.50	7.66%	3.431/3	1.91.66	.95.08	38.33
25.00	20.8313	16,66%	12.50	8.331/3	1 16%	2.08.33	1.01 4	41.00

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